

Electrospray from Magneto-electrostatic Instabilities

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MichiganTech

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THE UNIVERSITY OF
SYDNEY

Brian Hawkett, Nirmesh Jain

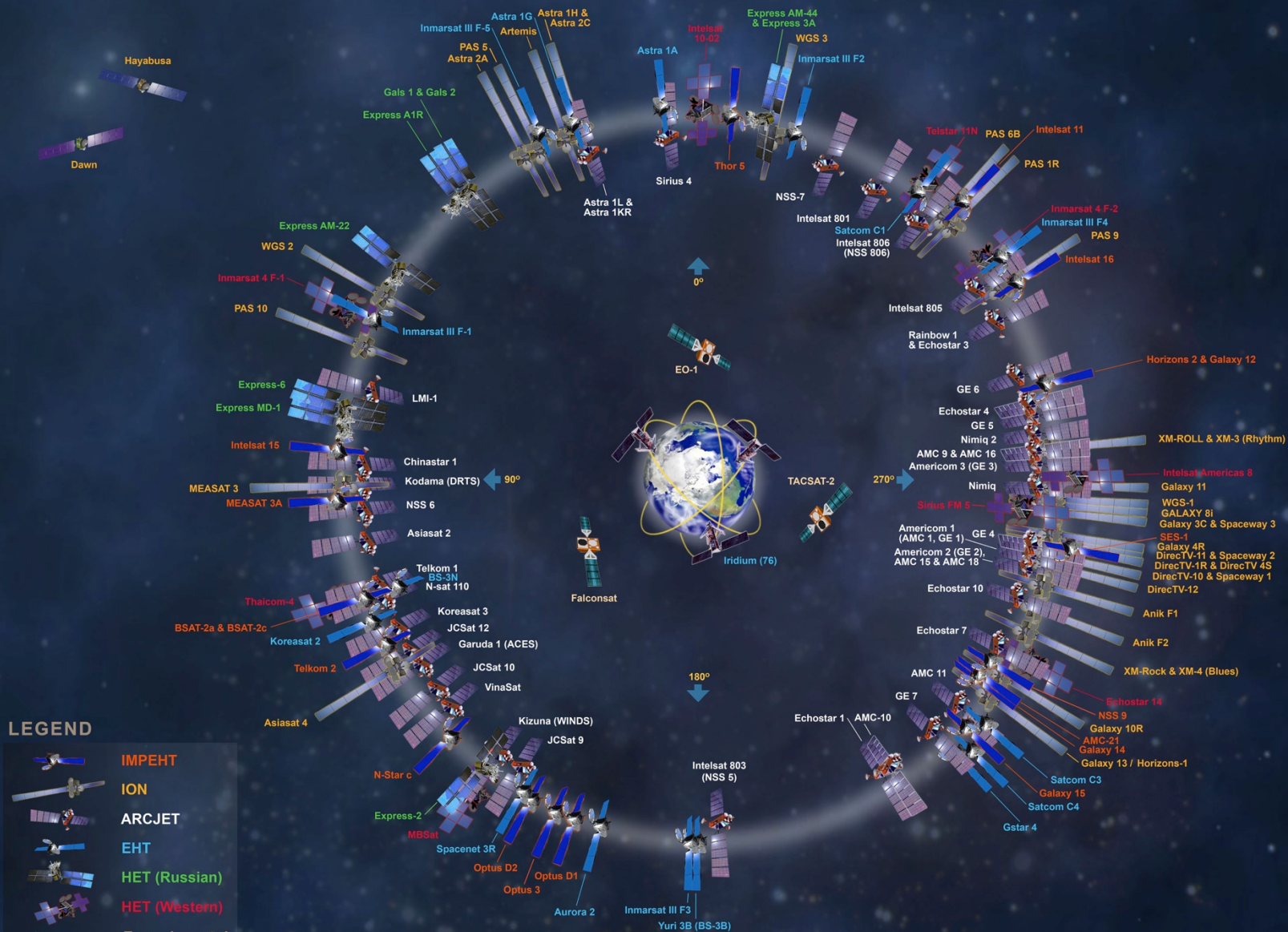
Yale

Juan Fernandez de la Mora, Aaron Madden, Javier Cubas



Deborah Levin, Neil Mehta

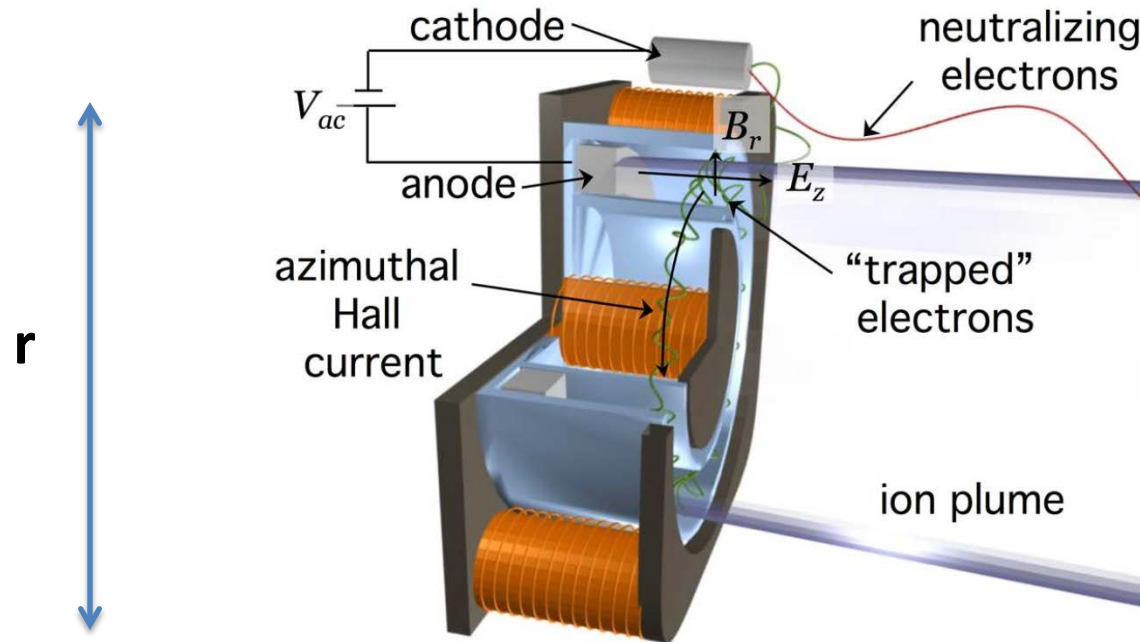
Operational Satellites with Electric Propulsion



All Spacecraft Employing EP = 236
Spacecraft Employing Aerojet EP = 158





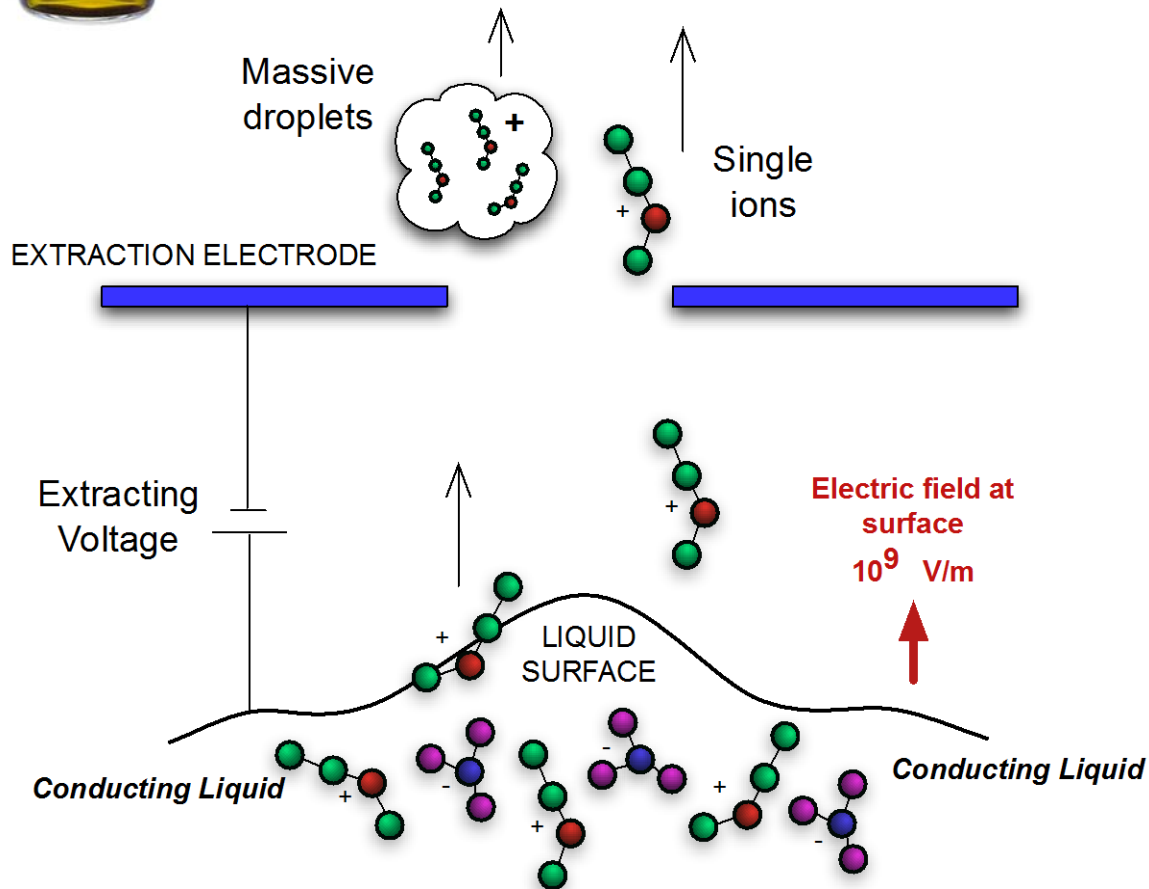


Gas density: $\lambda = \frac{1}{n\sigma} \Rightarrow n \propto \frac{1}{r}$

$$\frac{\text{Amount of erosion}}{\text{Amount of material}} \propto \frac{\text{Area}}{\text{Volume}} = \frac{r^2}{r^3} = \frac{1}{r}$$

Magnetic field: $r_L = \frac{mv_{\perp}}{|q|B} \Rightarrow B \propto \frac{1}{r}$

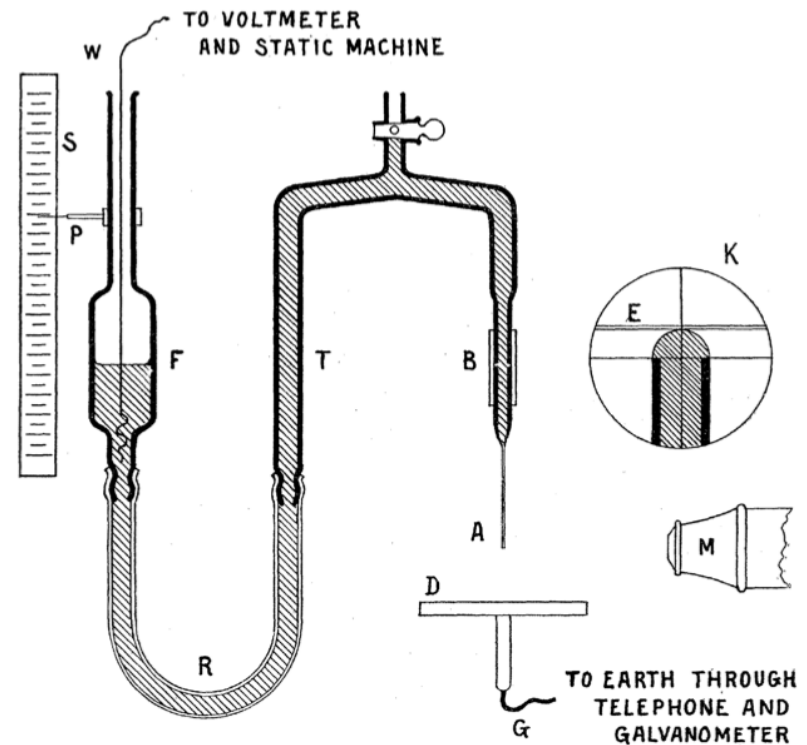
Electrospray: plasma in a bottle



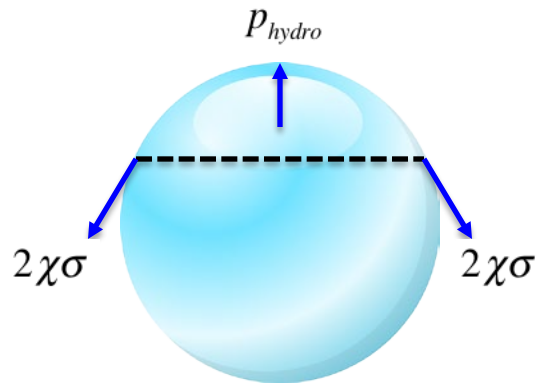
Jean-Antoine Nollet – 1750:

“a person, electrified by connection to a high-voltage generator, would not bleed normally if he were to cut himself; blood would spray from the wound.”

Zeleny, J., "The electrical discharge from liquid points, and a hydrostatic method of measuring the electric intensity at their surfaces," *Physical Review*, **3**(2), 1914, 69-91.

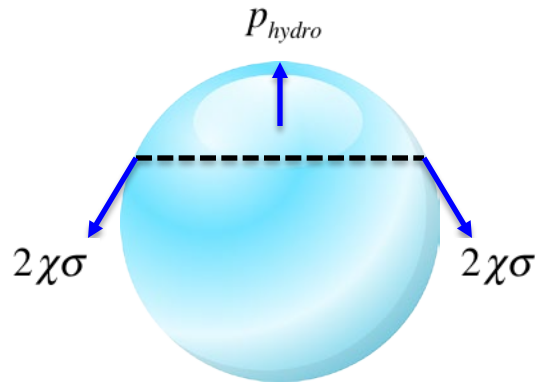


Neutral Fluid



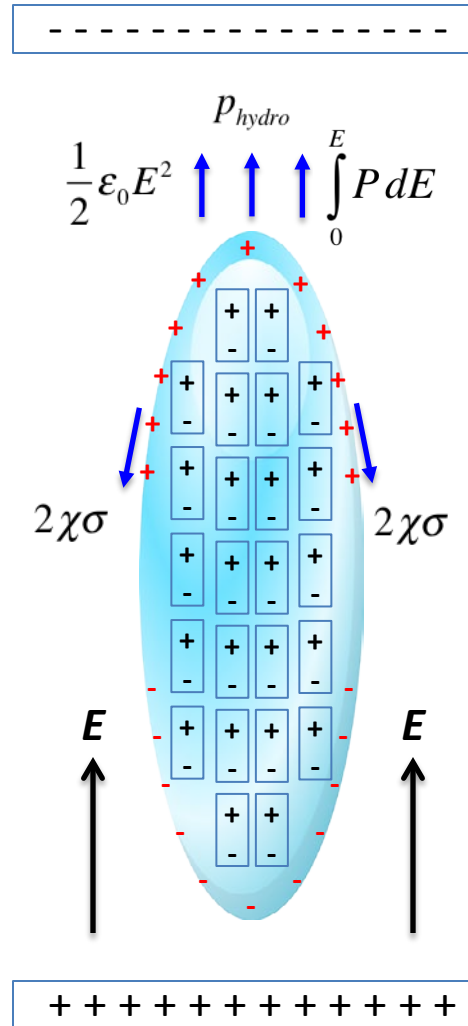
*Surface tension is balanced by
fluid pressure*

Neutral Fluid

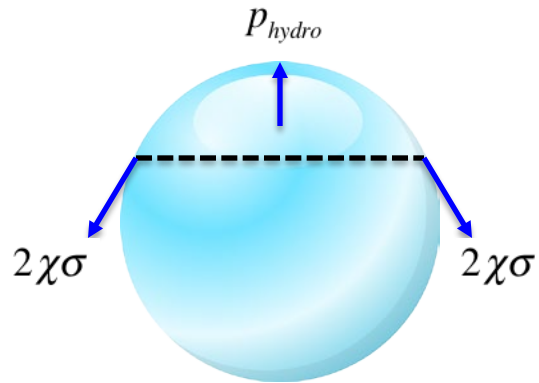


Surface tension is balanced by fluid pressure

Electrohydrodynamic Stress

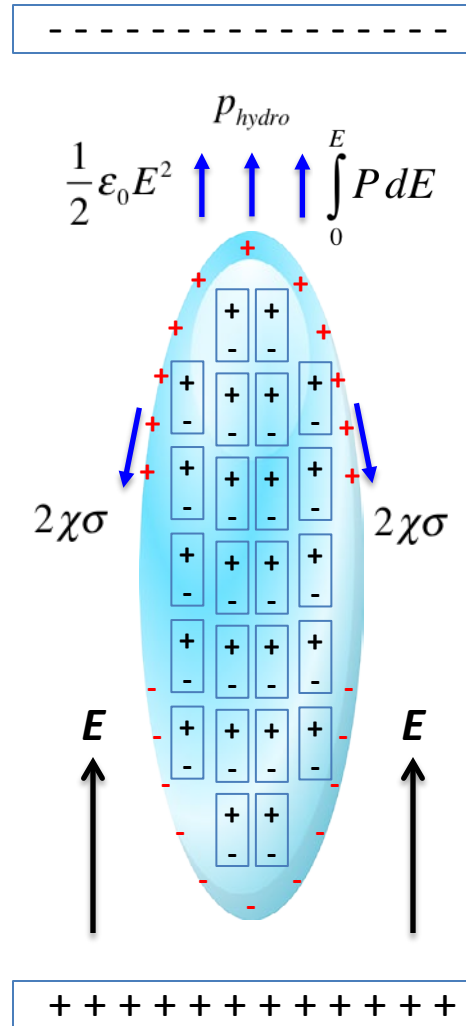


Neutral Fluid

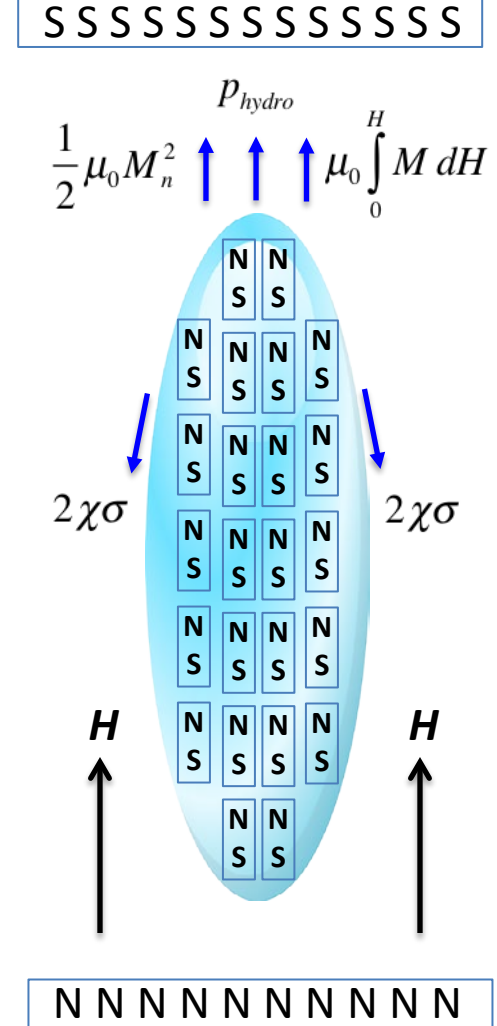


Surface tension is balanced by fluid pressure

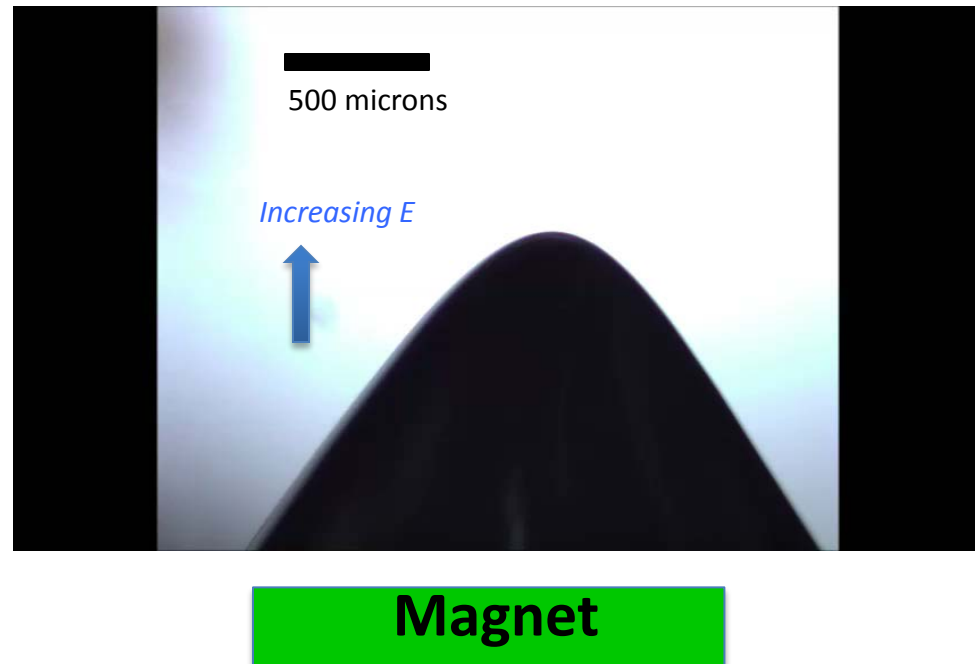
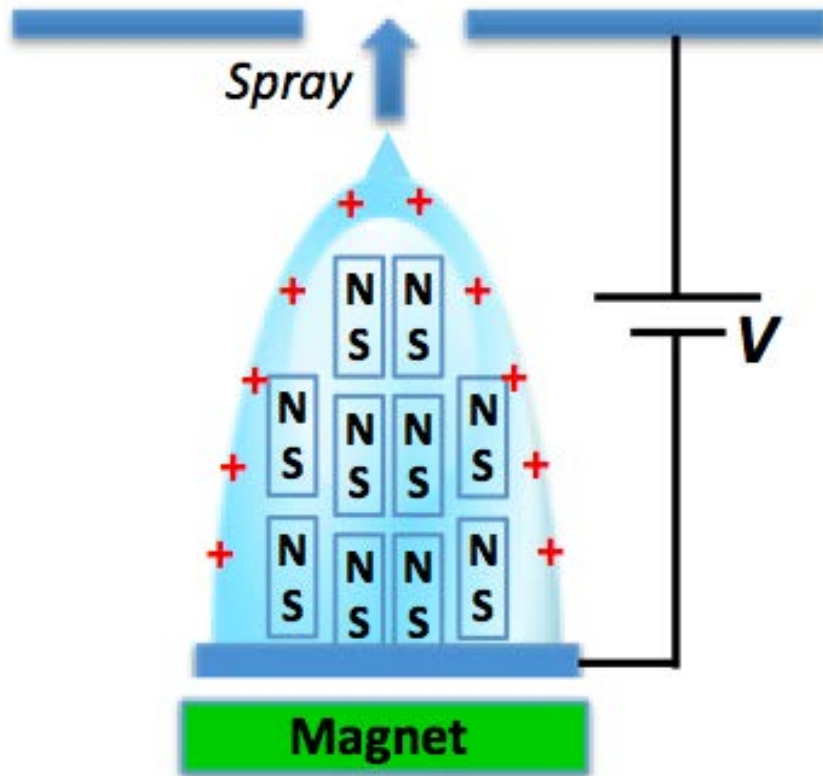
Electrohydrodynamic Stress



Ferrohydrodynamic Stress



Explore new fluid mechanics of combined ferro- and electrohydrodynamic spray emission



New material: Ionic liquid ferrofluid

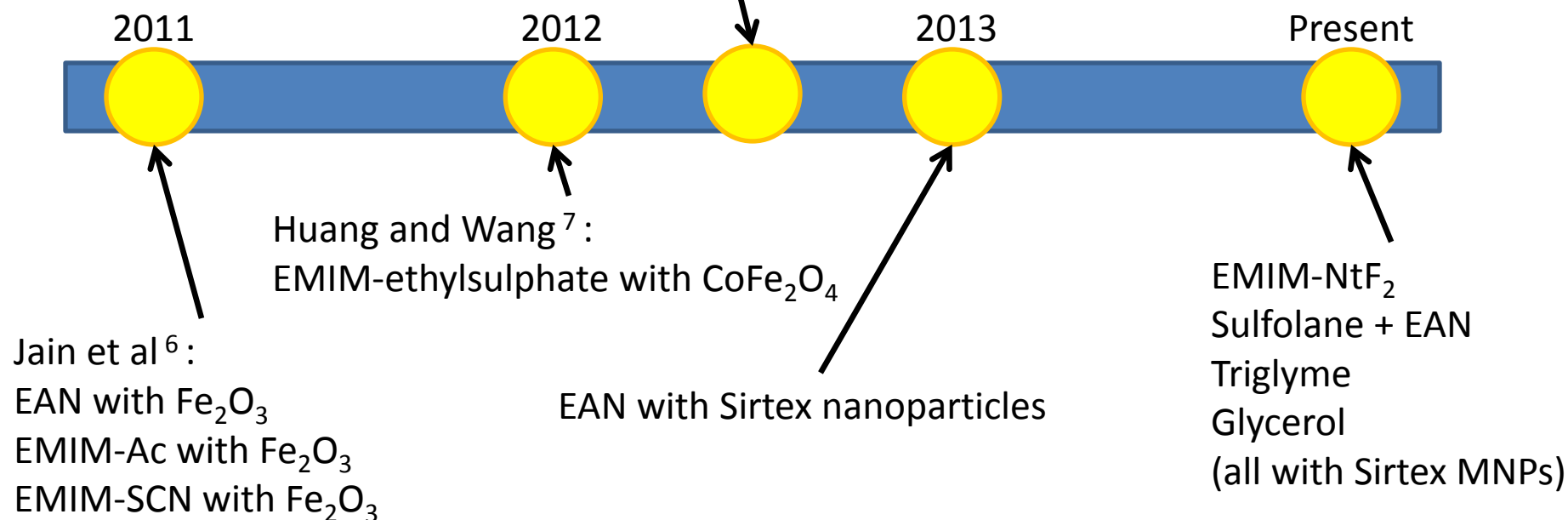
Collaboration between

MichiganTech

and



THE UNIVERSITY OF
SYDNEY



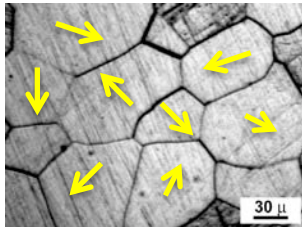
⁶ Jain, N. et al., Stable and Water-Tolerant Ionic Liquid Ferrofluid. Applied Materials and Interfaces 2011 (3): p. 662-667

⁷ Huang, W. and Wang, X., Study on the properties and stability of ionic liquid-based ferrofluids. Colloid Polym Sci, 2012 290: p. 1695-1702

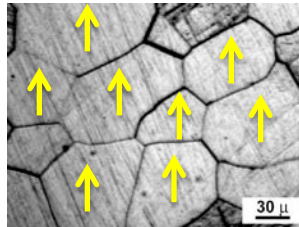
How to make a Ferrofluid

Melting a
Ferromagnetic
Substance Doesn't
Work:

$T \sim \text{Room Temp}$
No applied field
 $M_{\text{net}} = 0$

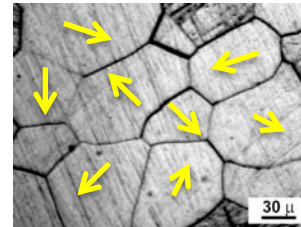


$T \sim \text{Room Temp}$
Applied Field
 $M_{\text{net}} > 0$



$\uparrow H$

$T > \text{Curie Temp}$
Applied Field
 $M_{\text{net}} \sim 0$



$\uparrow H$

$T > T_{\text{liquid}}$
 $M_{\text{net}} = 0$

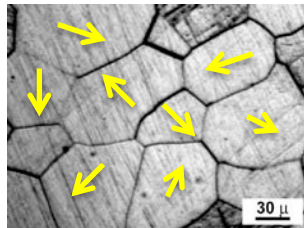


$\uparrow H$

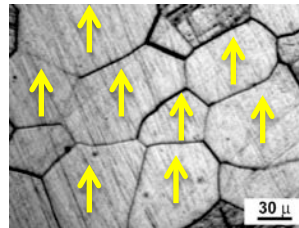
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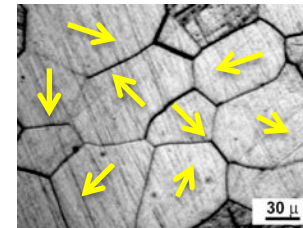


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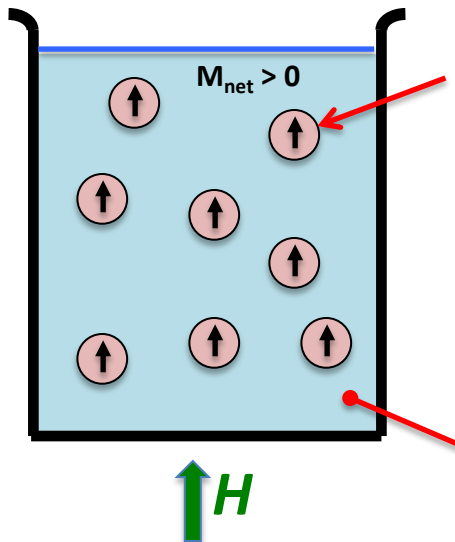
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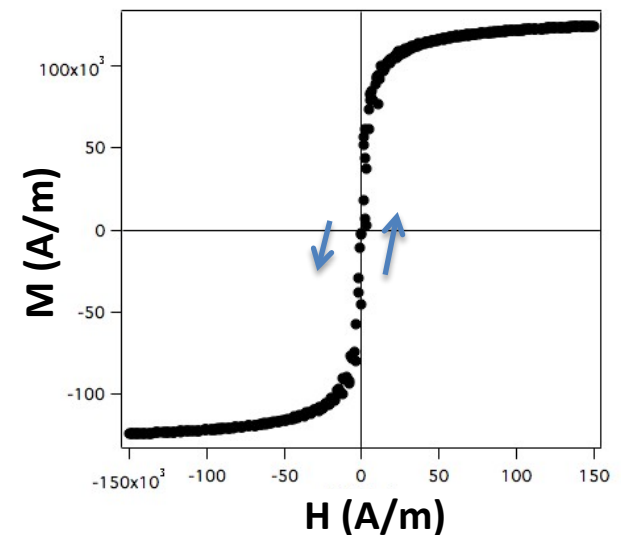
A Ferrofluid is a
Superparamagnetic
Colloid:



Solid-state
ferromagnetic
particles
small enough to
contain only
a single magnetic
domain (10s of nm)

Carrier liquid

Because the particles are free to rotate
The M-H curve does not display hysteresis



Ionic liquid ferrofluid: a truly magnetized plasma

Magnetohydrodynamics

$$\rho \frac{\partial \mathbf{v}}{\partial t} = \mathbf{j} \times \mathbf{B} - \nabla p$$

Lorentz Force

Electrohydrodynamics

$$\rho \frac{\partial \mathbf{v}}{\partial t} = q\mathbf{E} - \frac{1}{2}E^2 \nabla \epsilon - \nabla p$$

Coulomb Force

Ferrohydrodynamics

$$\rho \frac{\partial \mathbf{v}}{\partial t} = \mu_0 M \nabla H - \nabla p$$

Kelvin Force

Momentum:

$$\rho \frac{\partial \mathbf{v}}{\partial t} = \mathbf{j} \times \mathbf{B} + q\mathbf{E} - \frac{1}{2}E^2 \nabla \epsilon + \mu_0 M \nabla H - \nabla p$$

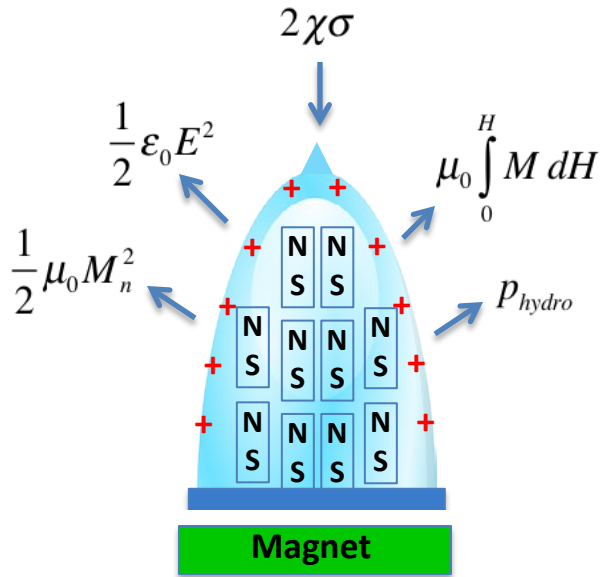
Quasi-static Maxwell:

$$\nabla \times \mathbf{H} = \mathbf{0} \quad \nabla \cdot \mu \mathbf{H} = 0 \quad \nabla \times \mathbf{E} = \mathbf{0} \quad \nabla \cdot \epsilon \mathbf{E} = 0$$

Young-Laplace:

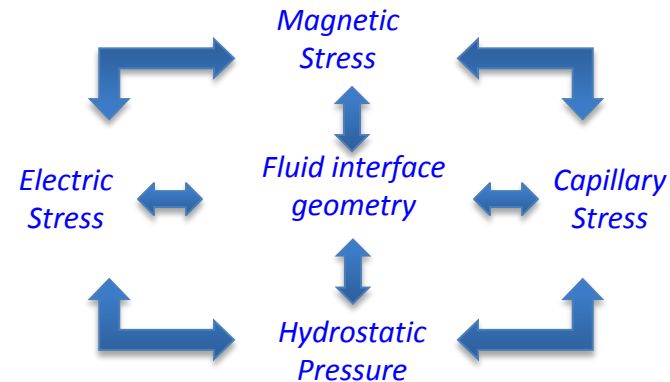
$$p_{hydro} + \mu_0 \int_0^H M dH + \frac{1}{2} \epsilon_0 E^2 + \frac{1}{2} \mu_0 M_n^2 = 2 \chi \sigma$$

Determine Critical Fields for Spray Onset



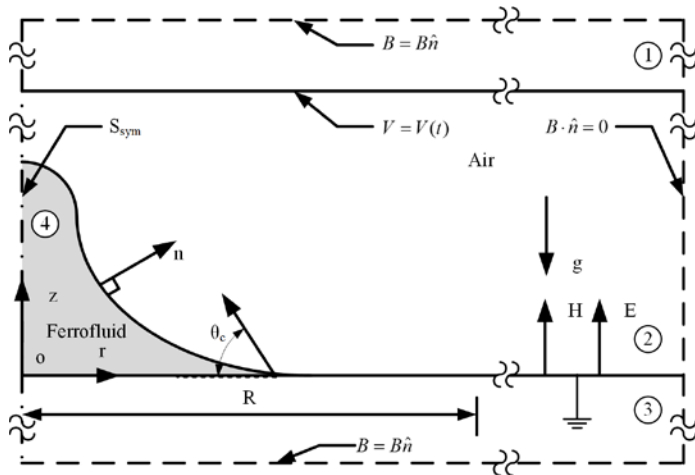
Fluid meniscus geometry is non-linear equilibrium

$$p_{hydro} + \mu_0 \int_0^H M dH + \frac{1}{2} \epsilon_0 E^2 + \frac{1}{2} \mu_0 M_n^2 = 2\chi\sigma$$



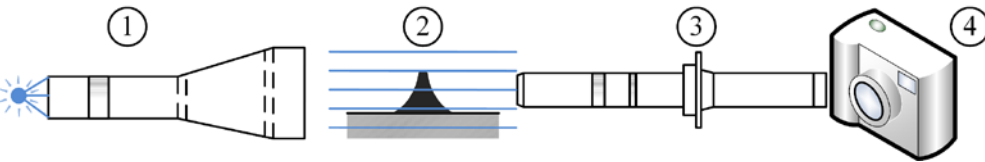
Numerical Simulation of Ferrofluid Droplet

- COMSOL Microfluidics with electromagnetic stress
- Two-phase transient flow with moving mesh (ALE)
- Experimentally determined M-H characteristic for fluid
- Experimentally determined fluid-solid contact angle

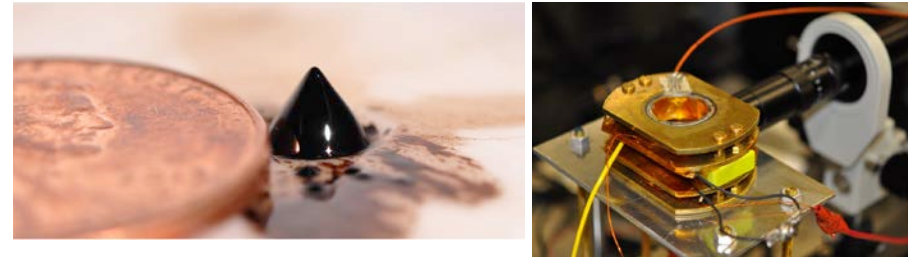


Numerical Model Validation

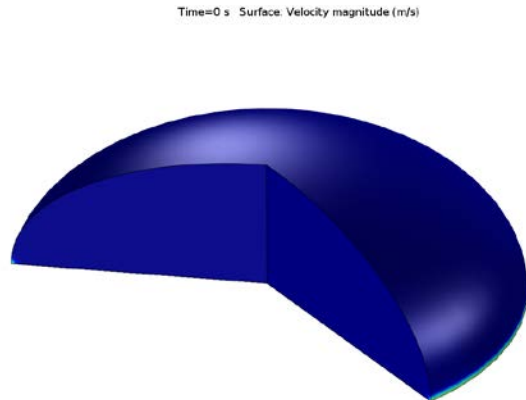
Collimated Backlight Imager



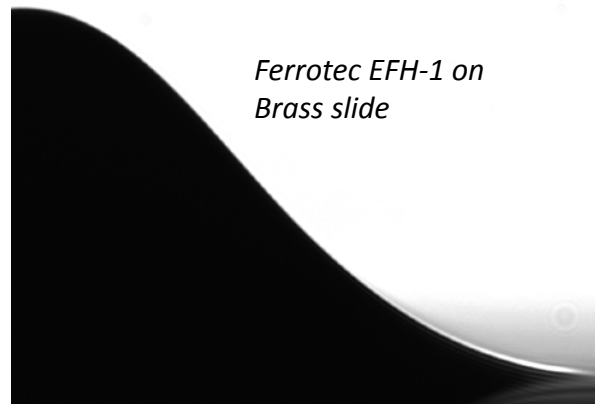
Droplet on Flat Plate in Helmholtz Coil



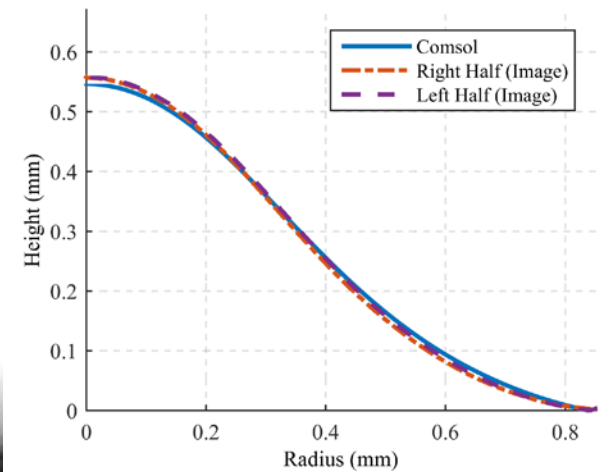
Transient Droplet Dynamics



Silhouette Image



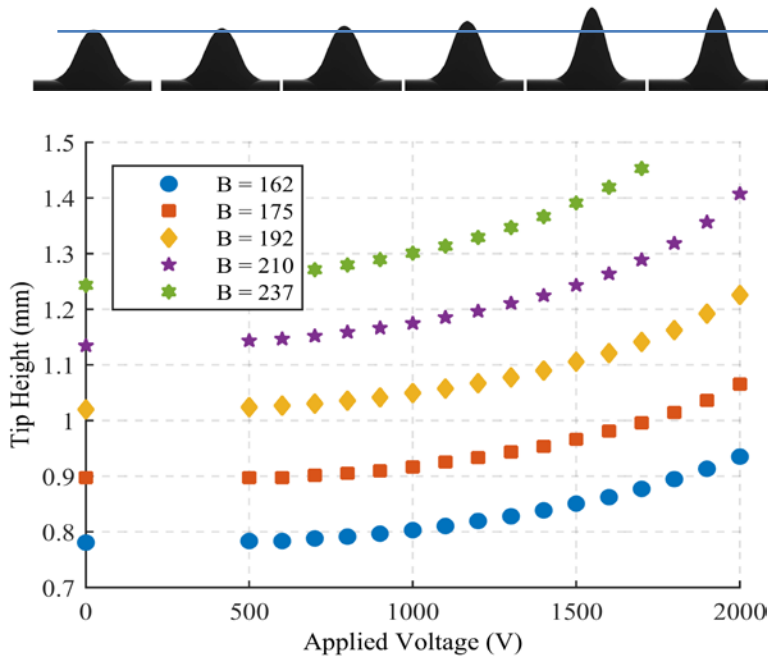
Model Validation



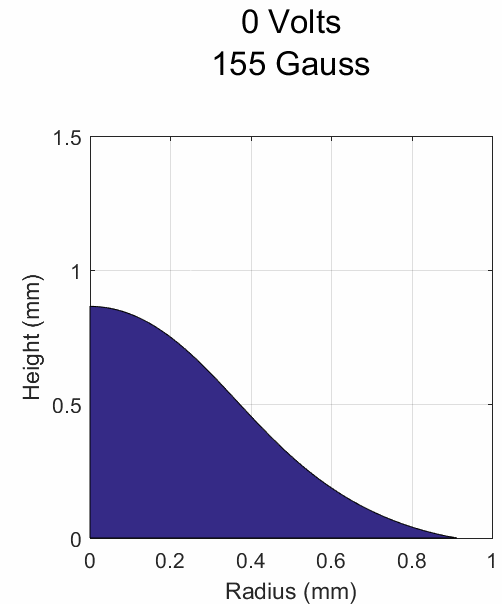
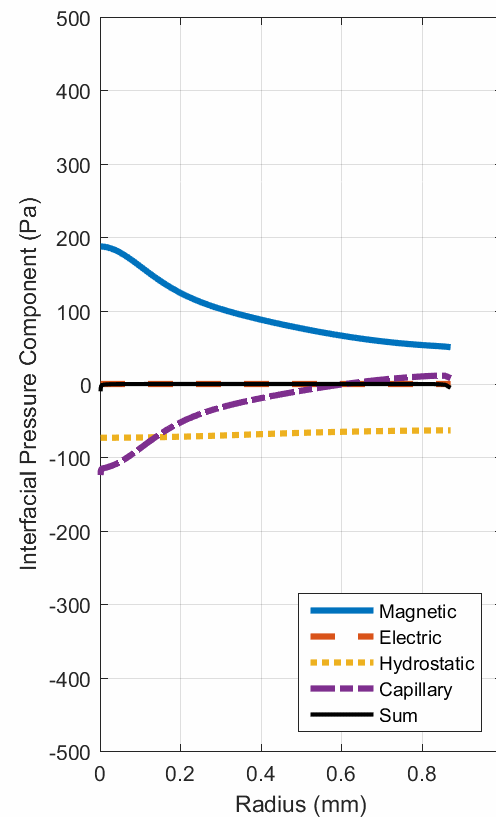
Interfacial Magneto-electrostatic Stress

$$p_{hydro} + \mu_0 \int_0^H M dH + \frac{1}{2} \epsilon_0 E^2 + \frac{1}{2} \mu_0 M_n^2 = 2 \chi \sigma$$

Experimental Silhouette Images

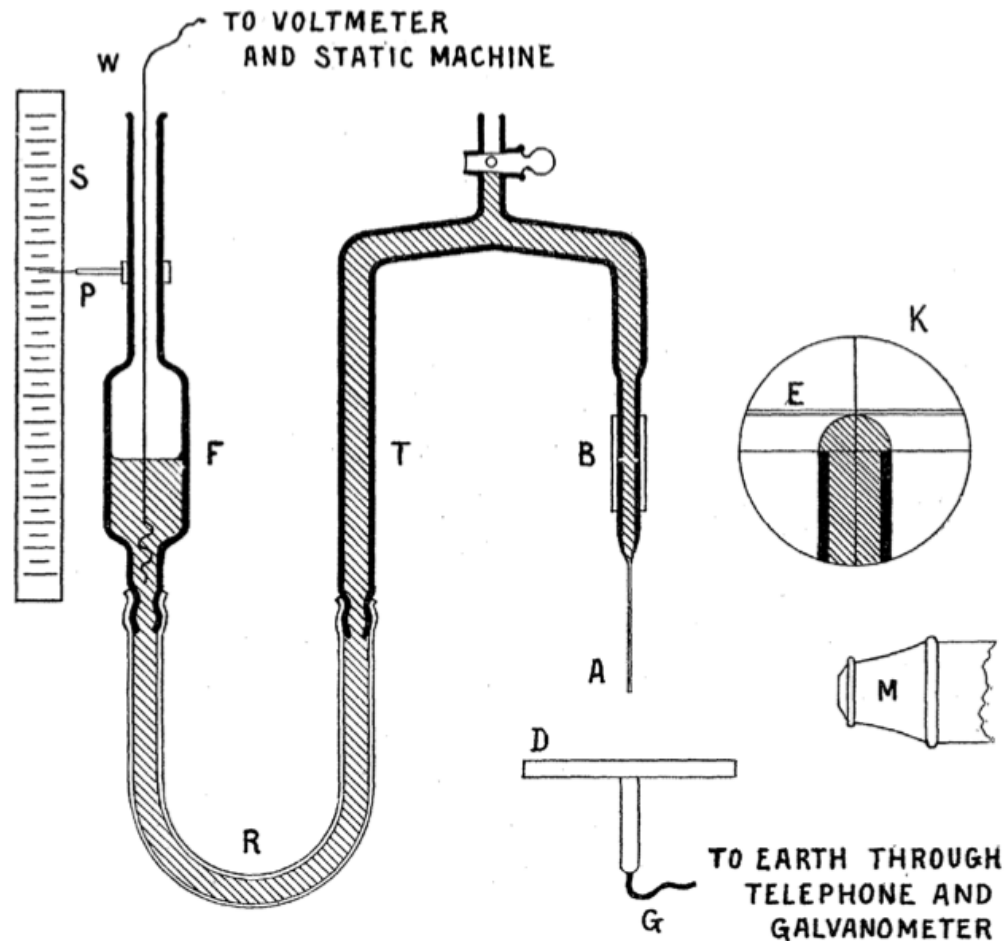


Numerical Simulation



Compare with Established Theory: Capillary Electrospray

Zeleny, J., "The electrical discharge from liquid points, and a hydrostatic method of measuring the electric intensity at their surfaces," *Physical Review*, 3(2), 1914, 69-91.



Capillary Studies: Motivation and Approach

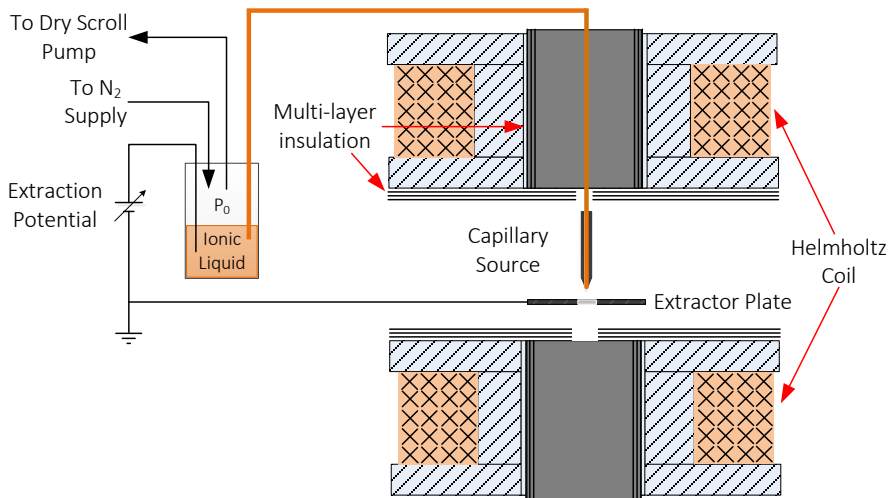
Existing Electrospray Theory (over 400 citations):

Fernandez de la Mora, J., and Loscertales, I.G., "The current emitted by highly conducting Taylor cones," *J. Fluid Mech.* 260, 155-184, 1994.

Surface tension $\rightarrow$ γ $\rightarrow$ Flow rate

Spray current $\rightarrow I \sim \sqrt{\frac{\gamma Q K}{\epsilon}}$ $\rightarrow$ Conductivity

ϵ $\leftarrow$ Permittivity



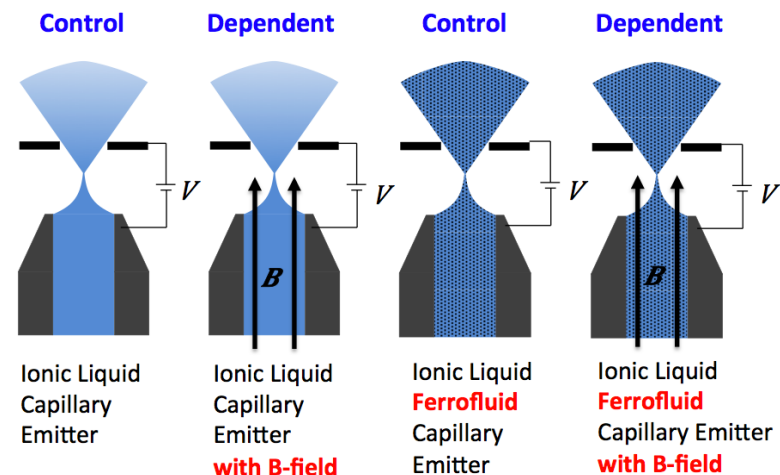
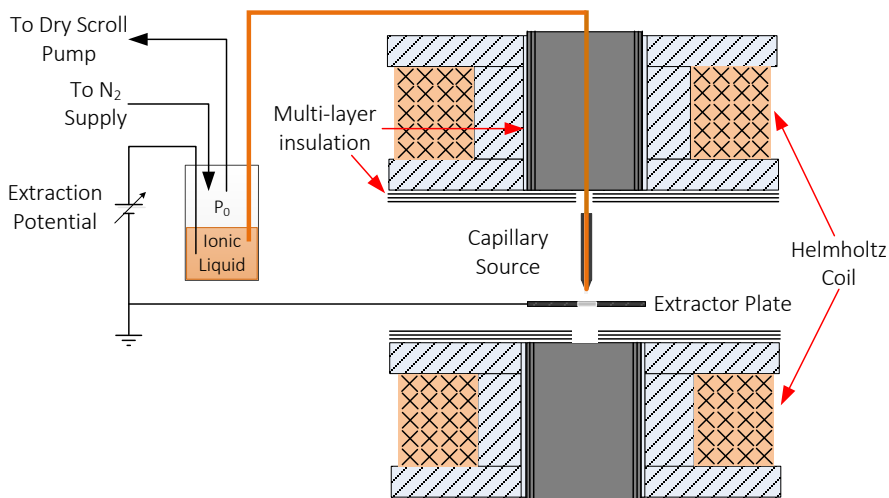
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$$I \sim \sqrt{\frac{\gamma Q K}{\epsilon}}$$

Surface tension $\rightarrow \gamma$
 Flow rate $\rightarrow Q$
 Conductivity $\rightarrow K$
 Spray current $\rightarrow I$
 Permittivity $\rightarrow \epsilon$



Sprayed in atmosphere

Sprayed in vacuum

Ferrofluid base	Sulfolane + 0.1% EAN	Sulfolane + 1% EAN	Sulfolane + 10% EAN	EMIM-NTf2
Conductivity (S/m)	0.012	0.033	0.324	0.57

Ferrofluids synthesized by University of Sydney Key Centre for Polymers and Colloids (Hawket and Jain) by stabilizing ~ 50-nm-diameter maghemite particles supplied by Sirtex Medical, Ltd.

Capillary Spray Results

Existing Electrospray Theory (over 400 citations):

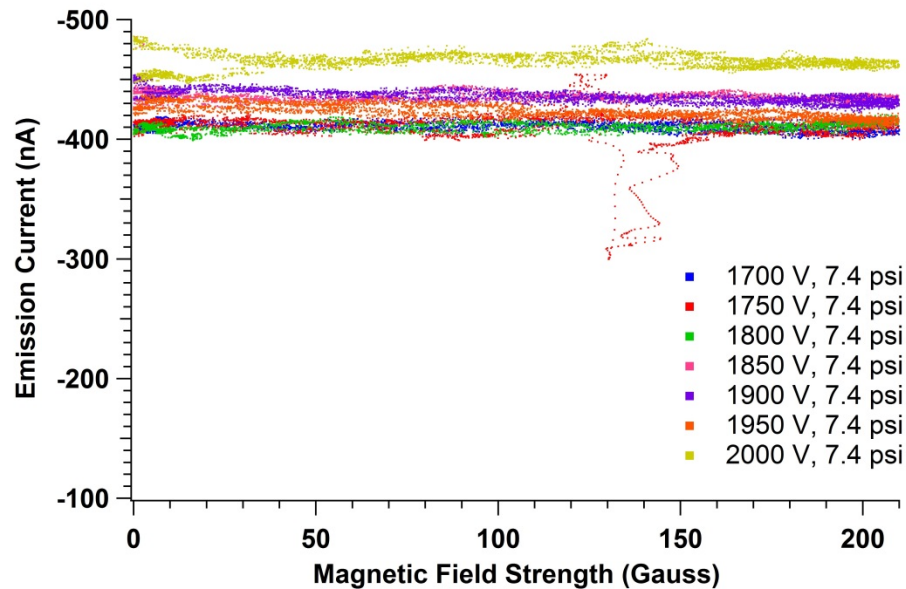
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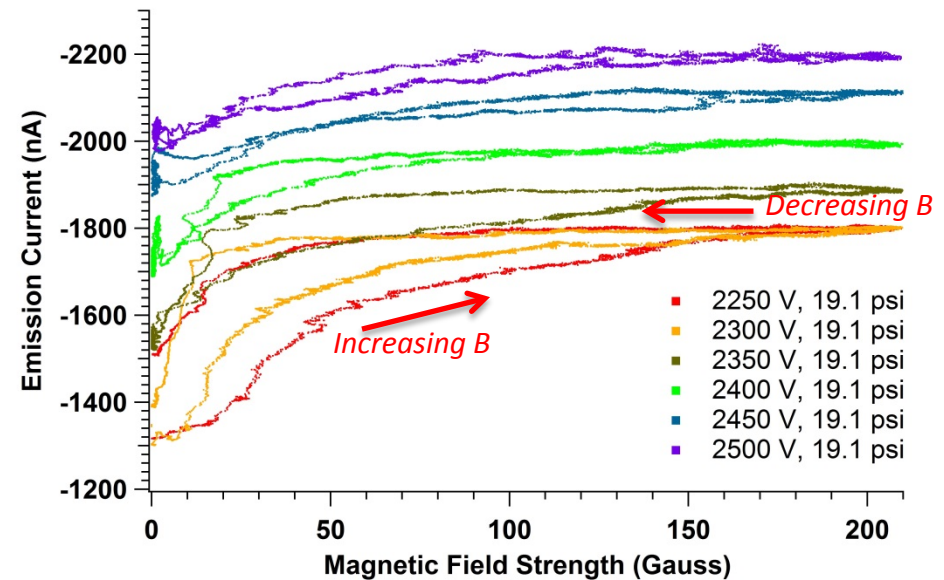
Surface tension γ Flow rate Q Conductivity K Permittivity ϵ

Spray current I

Pure EMIM-NTf2



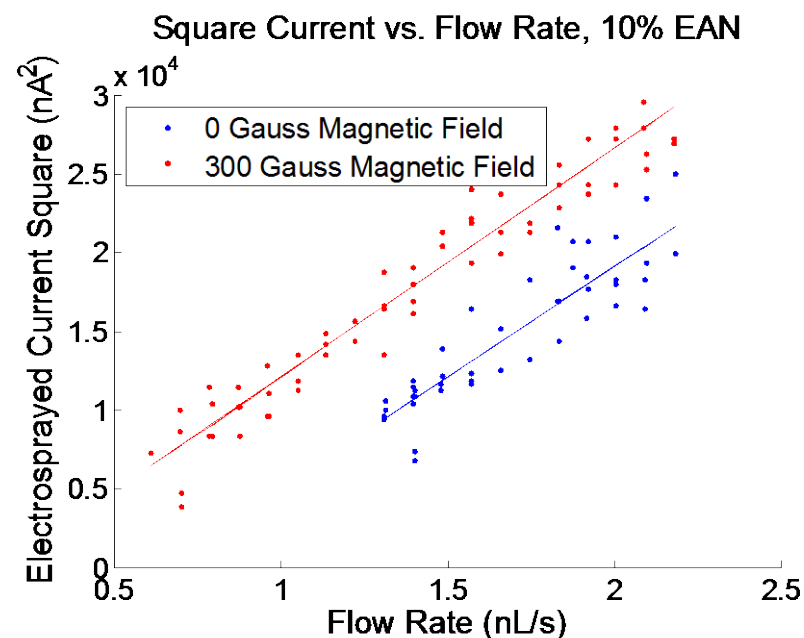
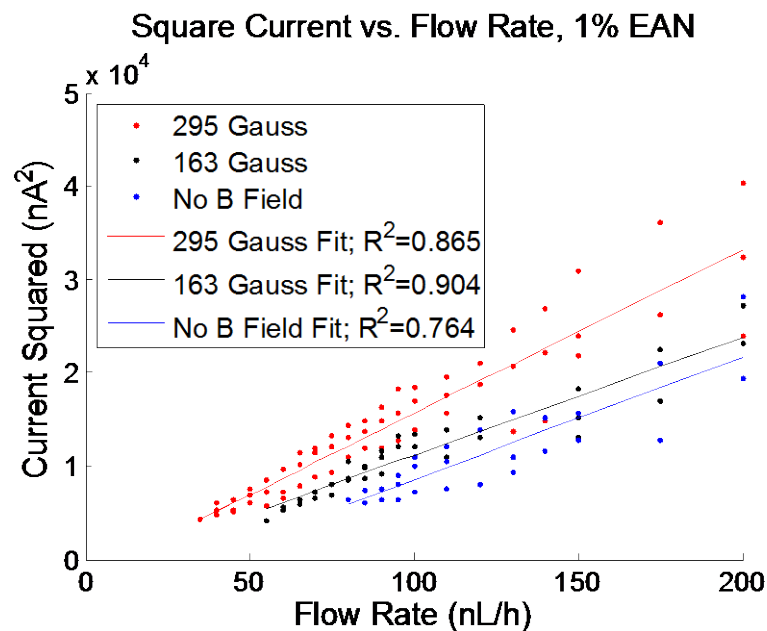
EMIM-NTf2 Ferrofluid



Magnetic effects increase current by ~ 40%

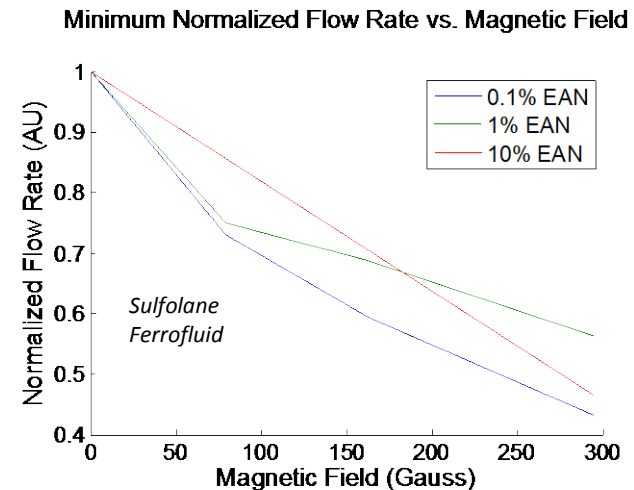
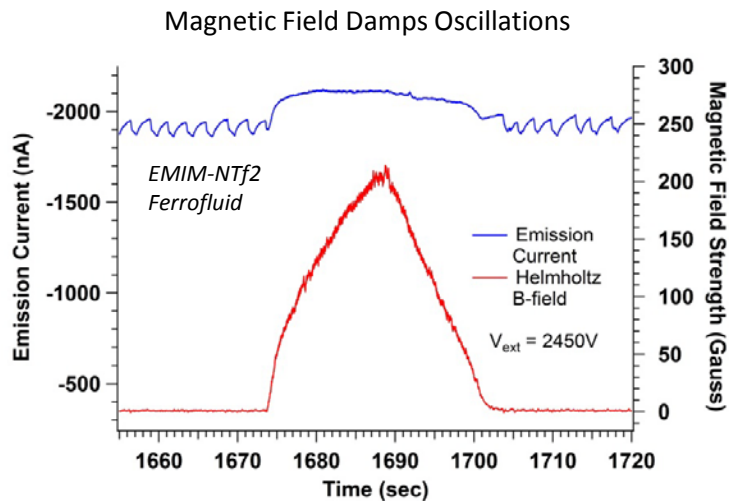
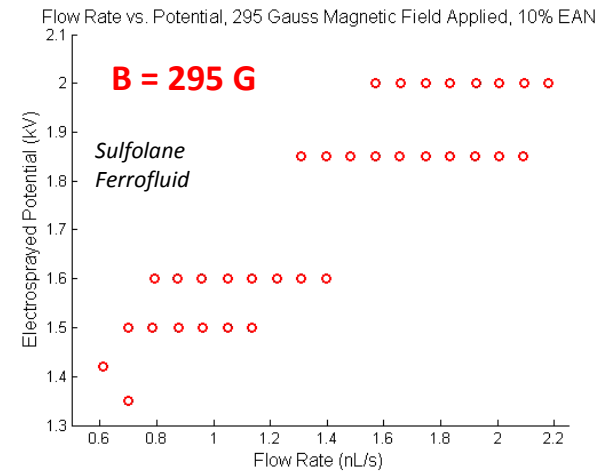
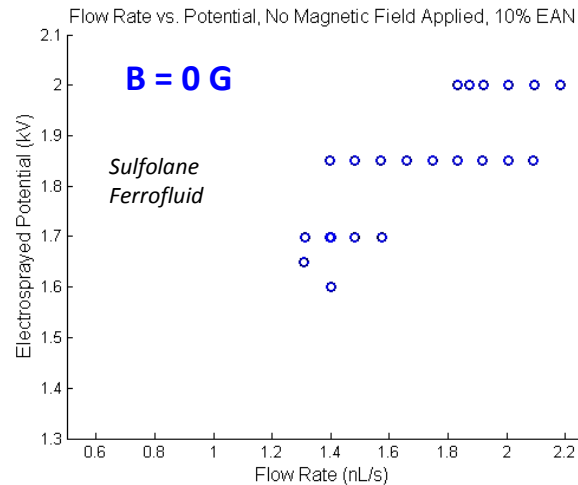
Capillary Spray Results

Existing Electro spray Theory:
$$I \sim \sqrt{\frac{\gamma Q K}{\varepsilon}}$$



Current still scales with square root of flow rate, but magnetic field increases the magnitude

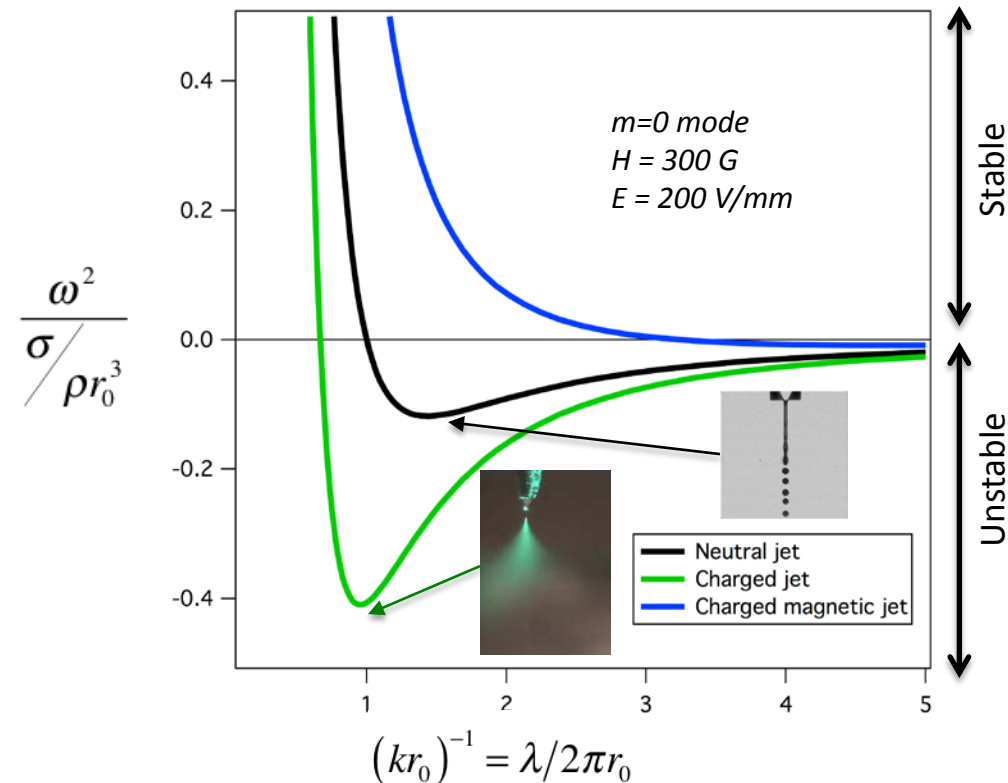
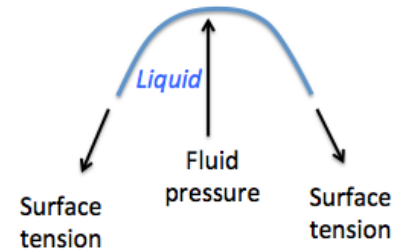
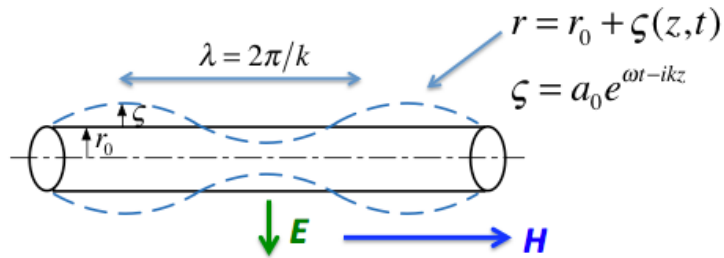
Magnetic Stress Extends Spray Stability Range



Lower stable flow rates will enable smaller droplet sizes

Theoretical Model of Jet Stability

Dispersion Relation for Surface Waves



Theoretical model of fluid cylinder stability against surface perturbation

Liquid is electrically conducting ferrofluid

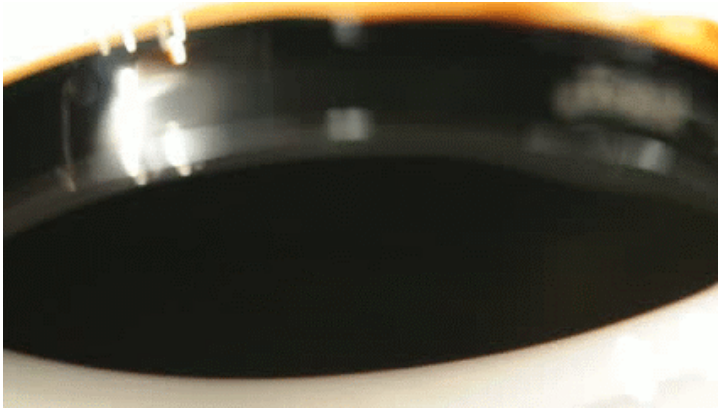
Axial magnetic field has a stabilizing effect against surface perturbations

Dipole alignment augments surface tension

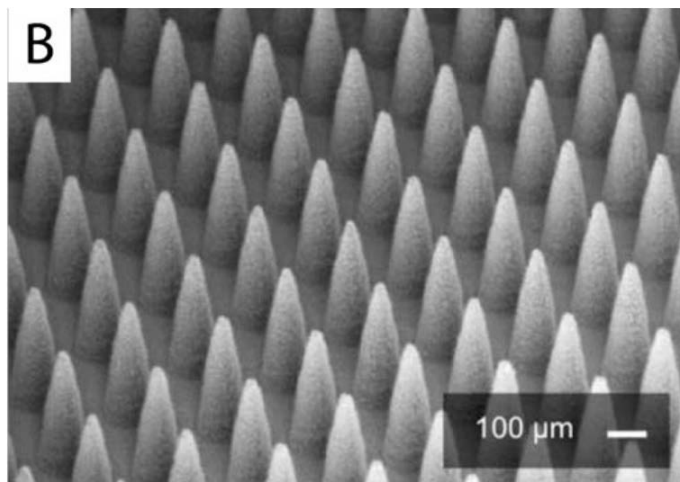


$$\Delta U = \underbrace{\frac{1}{2} \rho g \iint z^2(x, y) dx dy}_{\text{Gravitational}} + \underbrace{\sigma \iint \sqrt{1 + (\nabla z)^2} dx dy}_{\text{Surface Tension}} - \underbrace{\frac{1}{2} \iiint \mu_0 \left[\frac{(\mu_r - 1)}{1 + N(\mu_r - 1)} \right] H_0^2 dx dy dz}_{\text{Magnetic}}$$

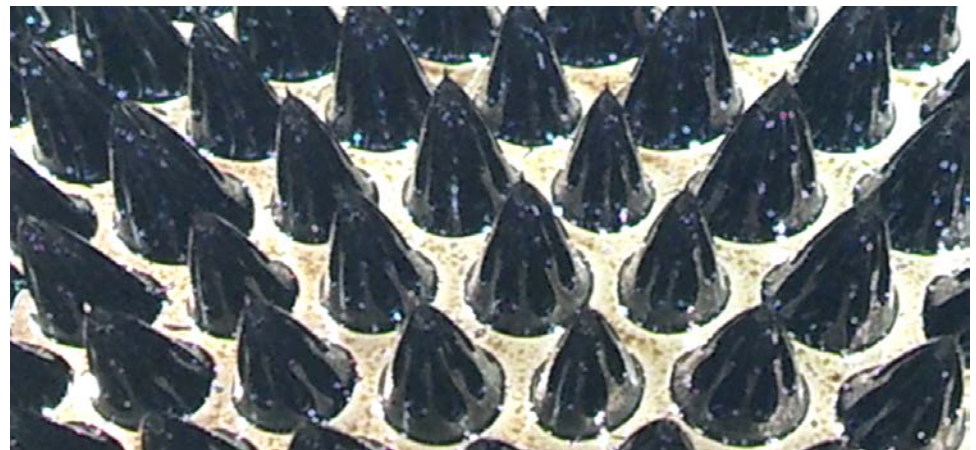
Self-assembling Array of Electrospray Emitters Fabricated from the Propellant Itself

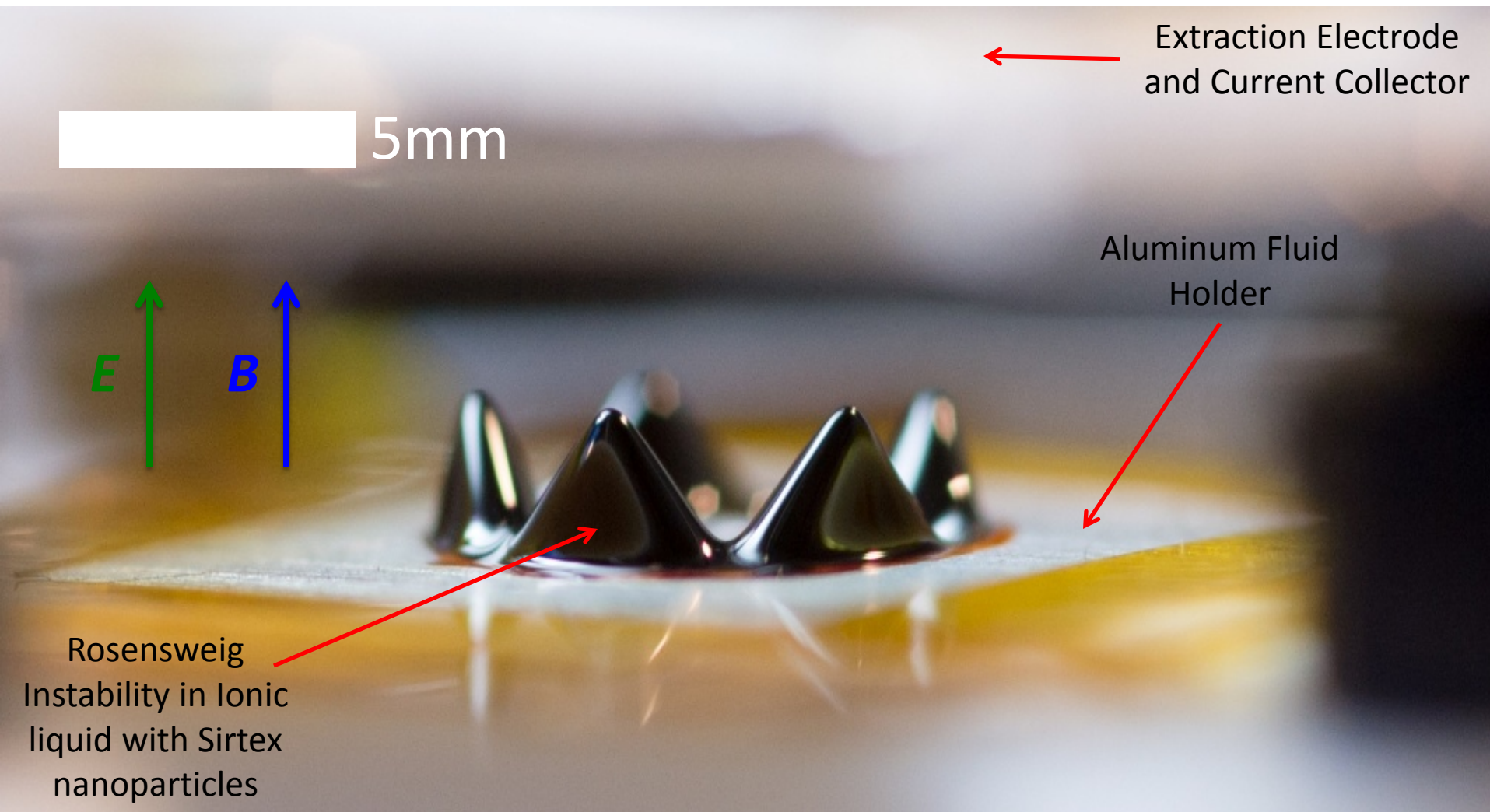


Emitter array fabricated in silicon

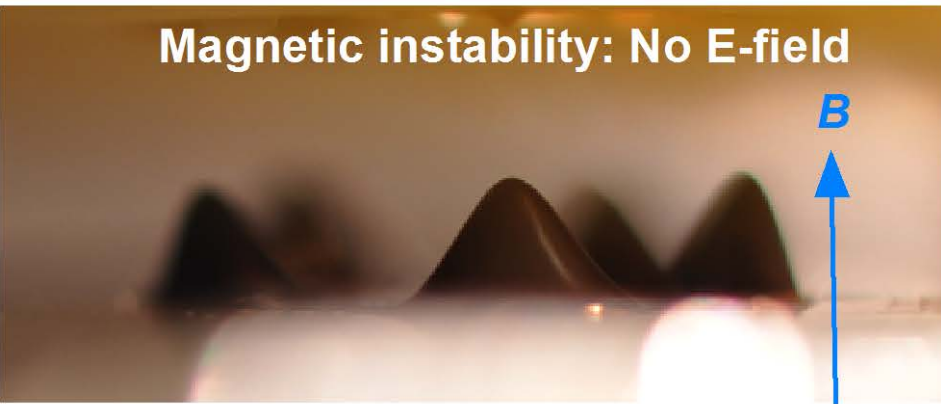


Rosensweig instability in ionic liquid ferrofluid





Magnetic instability: No E-field

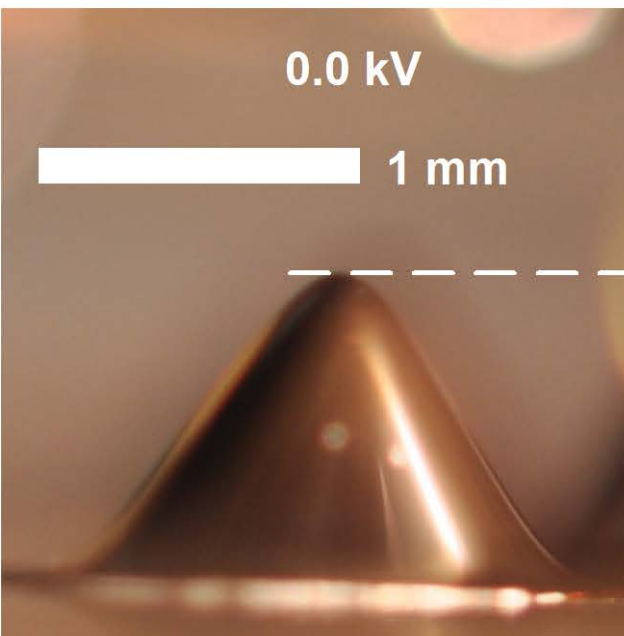


Electrospray Jetting

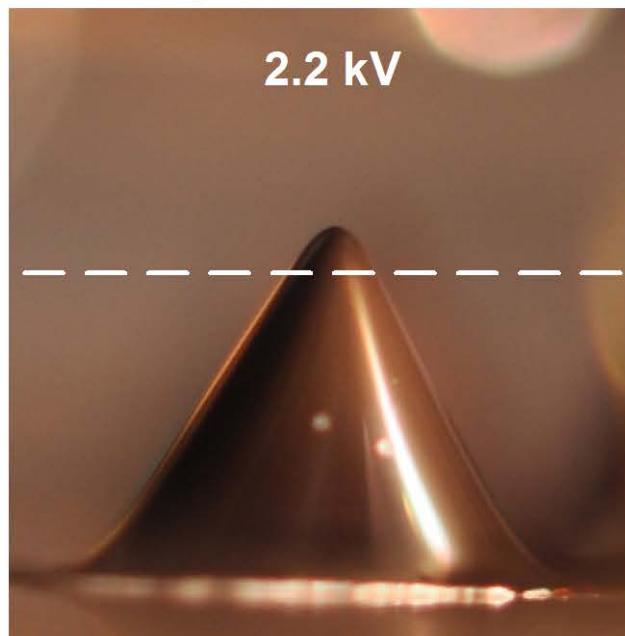


0.0 kV

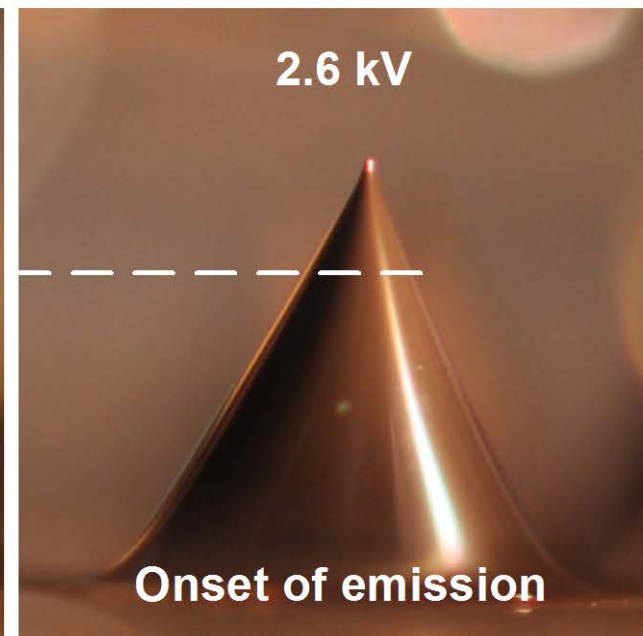
1 mm

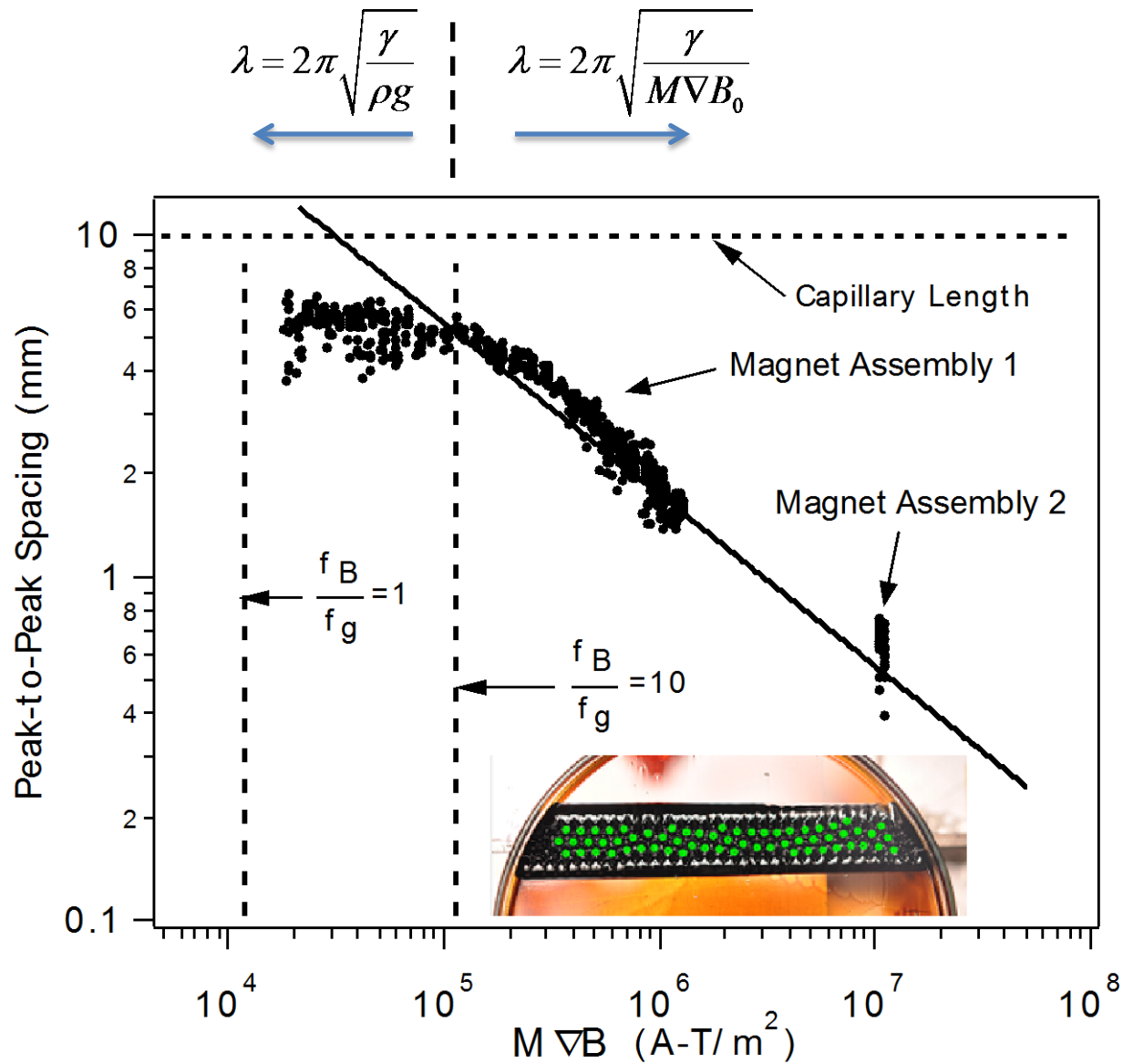


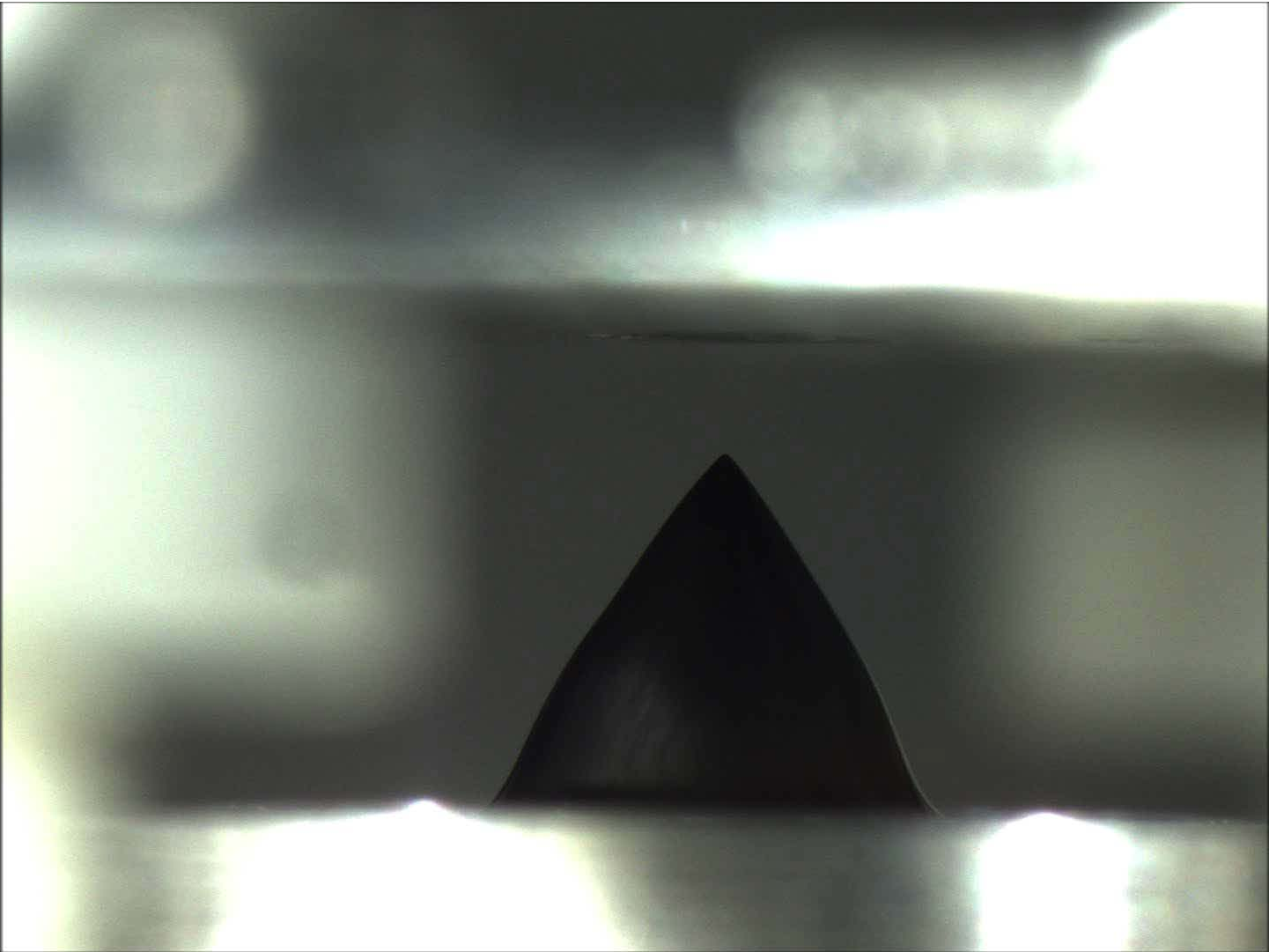
2.2 kV



2.6 kV







$\uparrow M$

Permanent Magnet

$\uparrow M$

Where we're going...

