



Mode Transitions in Low-Temperature Aerospace Plasmas

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University of Washington

Michigan Institute for Plasma Science and Engineering

Early Career Lecture

03/31/21

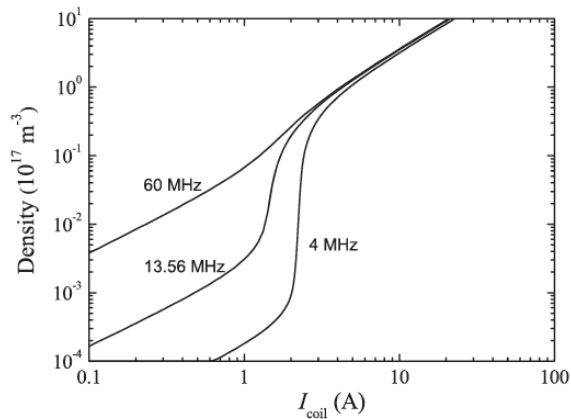
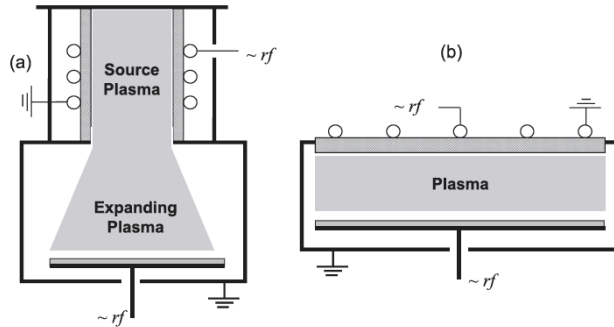


mode transition

noun

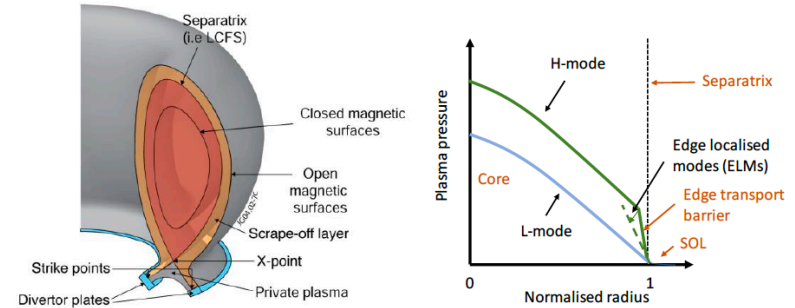
a sudden, major transformation of the structure and/or dynamics of a plasma in response to a minor change to its operating conditions

Plasma Processing

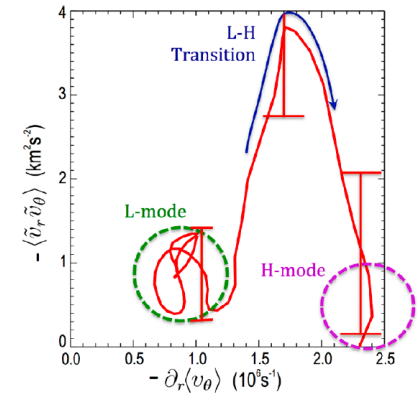
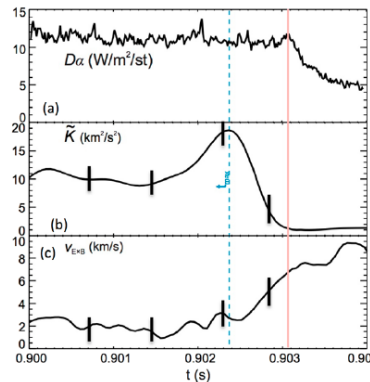


Chabert et. al., *Plasma Sources Sci. Tech.* 30.2 (2021): 024001

Fusion Energy

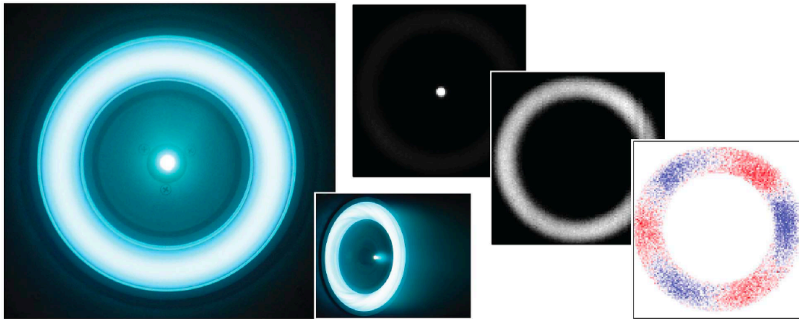


Ham et al. *Nature Reviews Physics* 2.3 (2020): 159-167.



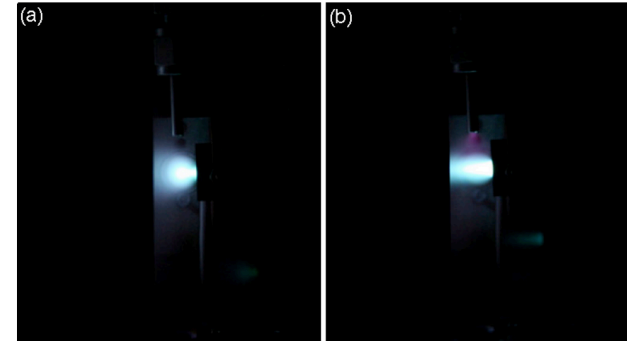
Tynan et al. *Plasma Phys. Controlled Fusion* 58.4 (2016): 044003.

Hall Thrusters

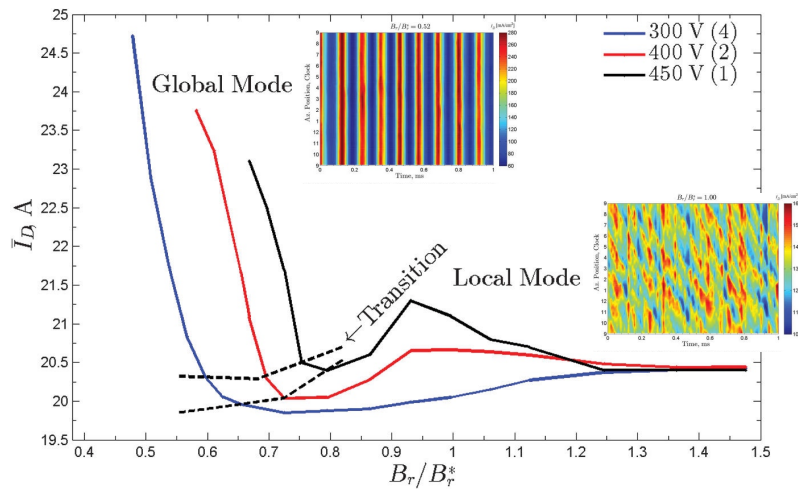


McDonald and Gallimore. *IEEE Trans. Plasma Sci.* 39.11 (2011): 2952-2953.

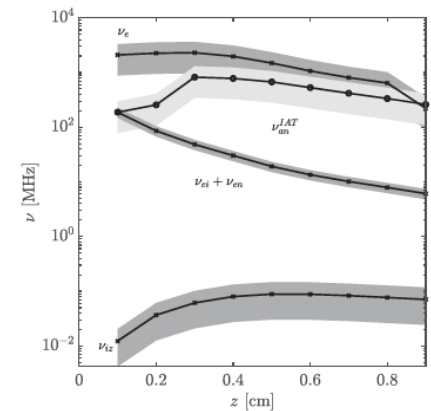
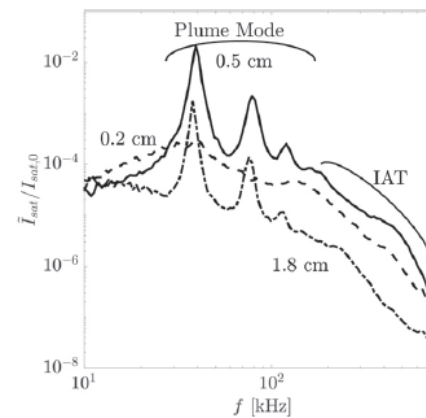
Hollow Cathodes



Goebel et al. *30th International Electric Propulsion Conference*. 2007.

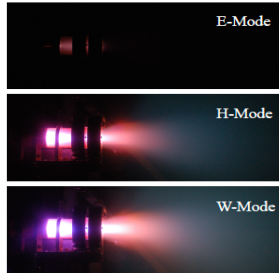


Sekerak et al. *J. Propul. Power* 32.4 (2016): 903-917.



Georgin, Jorns, and Gallimore. *Plasma Sources Sci. Tech.* 29.10 (2020): 105010.

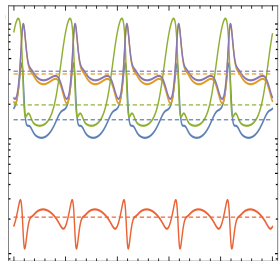
Mode Transitions in Aerospace Plasmas



Topic 1: Mode transitions in helicon thrusters

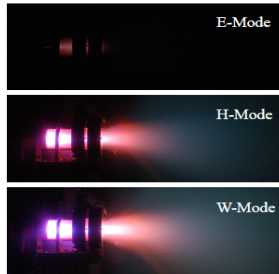


Topic 2: Critical velocities for plasma aerocapture



Topic 3: Data-driven discovery of mode transition physics

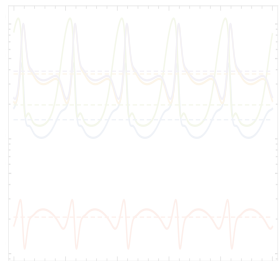
Mode Transitions in Aerospace Plasmas



Topic 1: Mode transitions in helicon thrusters



Topic 2: Critical velocities for plasma aerocapture

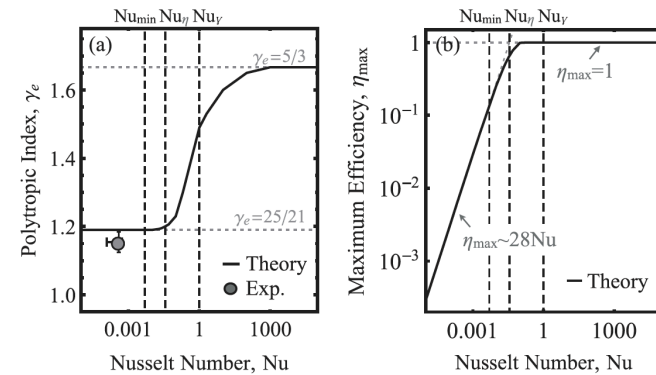
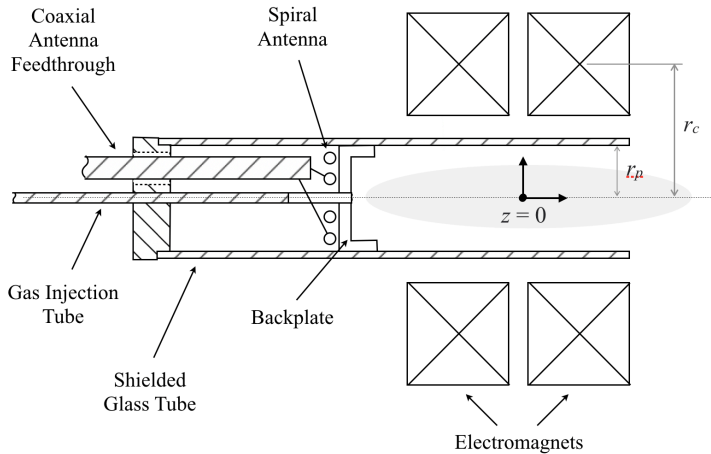


Topic 3: Data-driven discovery of mode transition physics

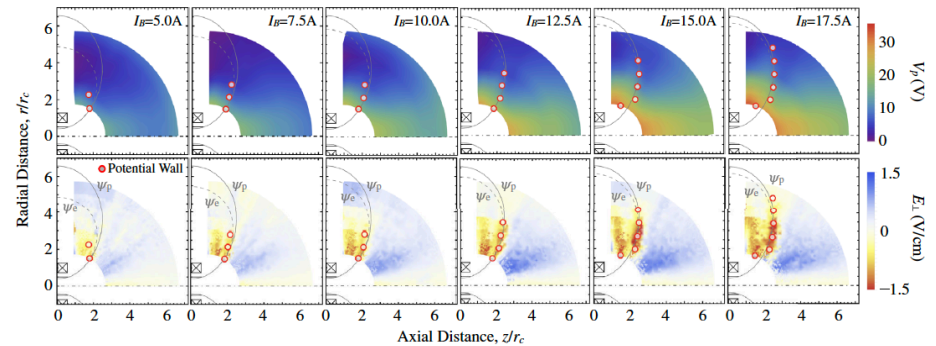
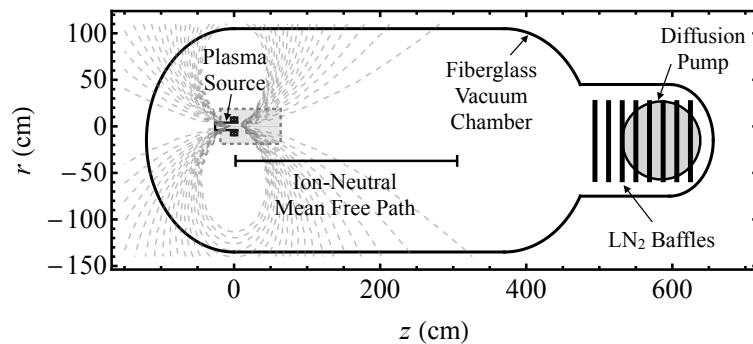
Magnetic Nozzle Experiment (Princeton University)



Goal: Understand plasma expansion and detachment from magnetic nozzle



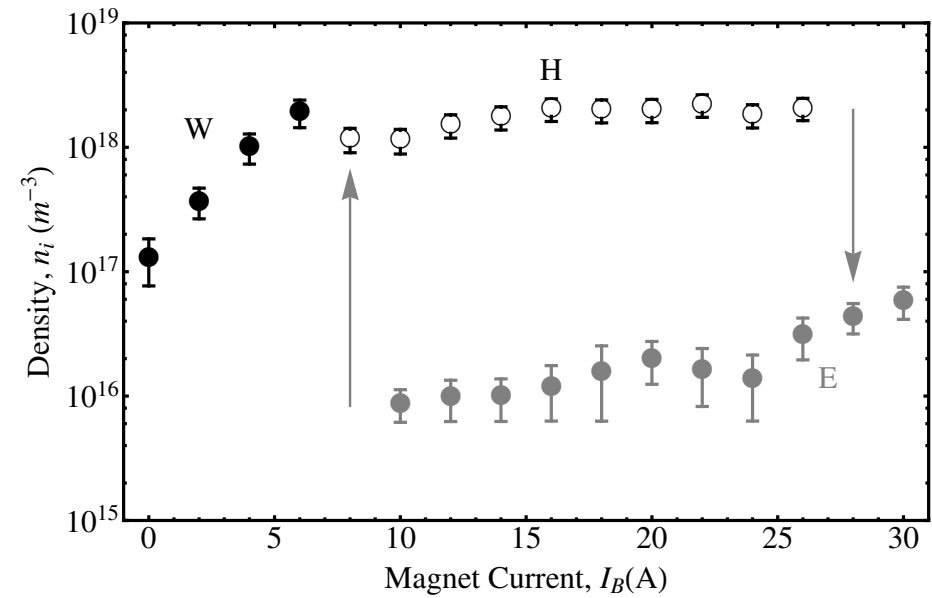
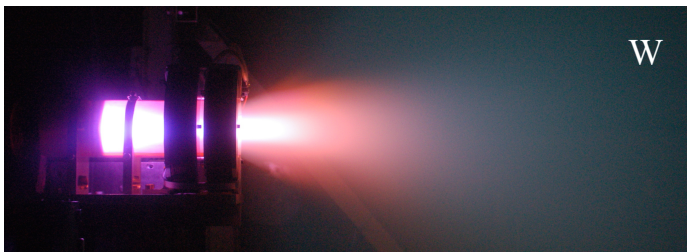
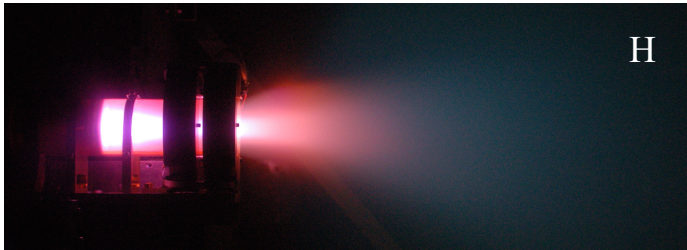
Little and Choueiri. *Phys. Rev. Lett.* 117.22 (2016): 225003.



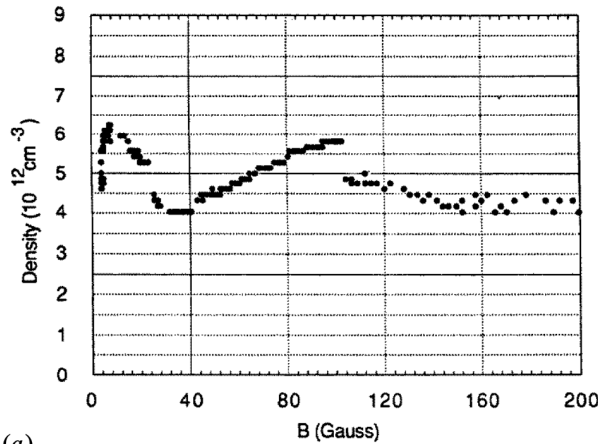
Little and Choueiri. *Phys. Rev. Lett.* 123.14 (2019): 145001.

Mode Transitions

W

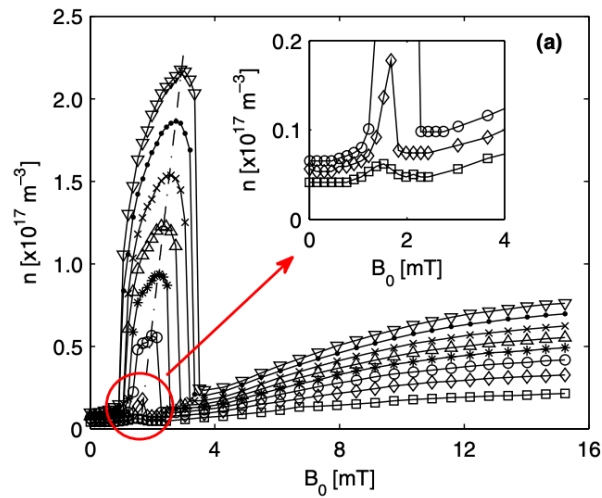


Low-Field Mode Transition (LFMT)

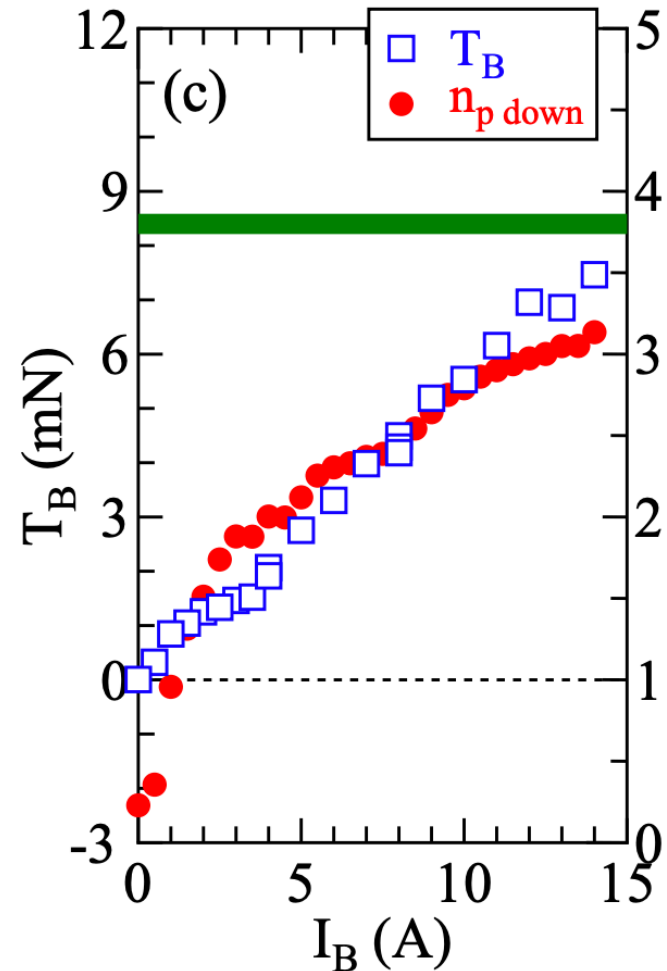


(a)

Chen, F. F., et al. "Low-field helicon discharges." *Plasma Physics and Controlled Fusion* 39.5A (1997): A411.

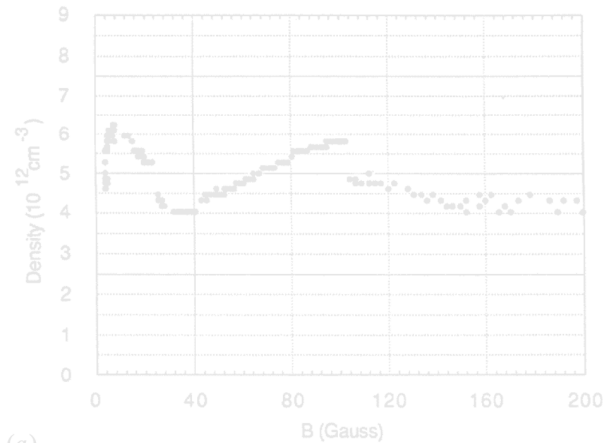


Lafleur, T., Charles, C., and R. W. Boswell. "Characterization of a helicon plasma source in low diverging magnetic fields." *Journal of Physics D: Applied Physics* 44.5 (2011): 055202.



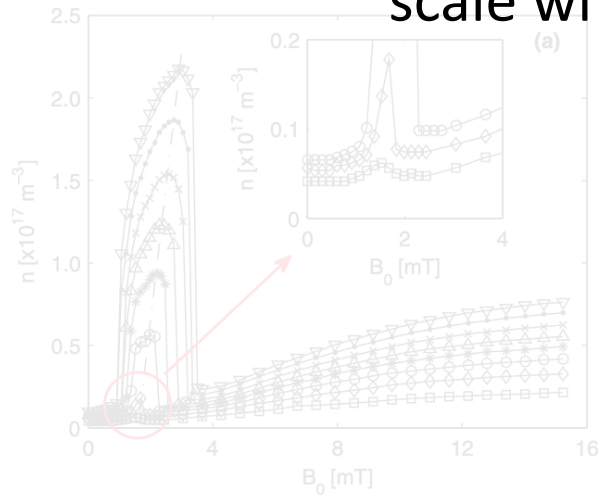
Takahashi, Kazunori, et al. "Effect of magnetic and physical nozzles on plasma thruster performance." *Plasma Sources Science and Technology* 23.4 (2014): 044004.

Low-Field Mode Transition (LFMT)

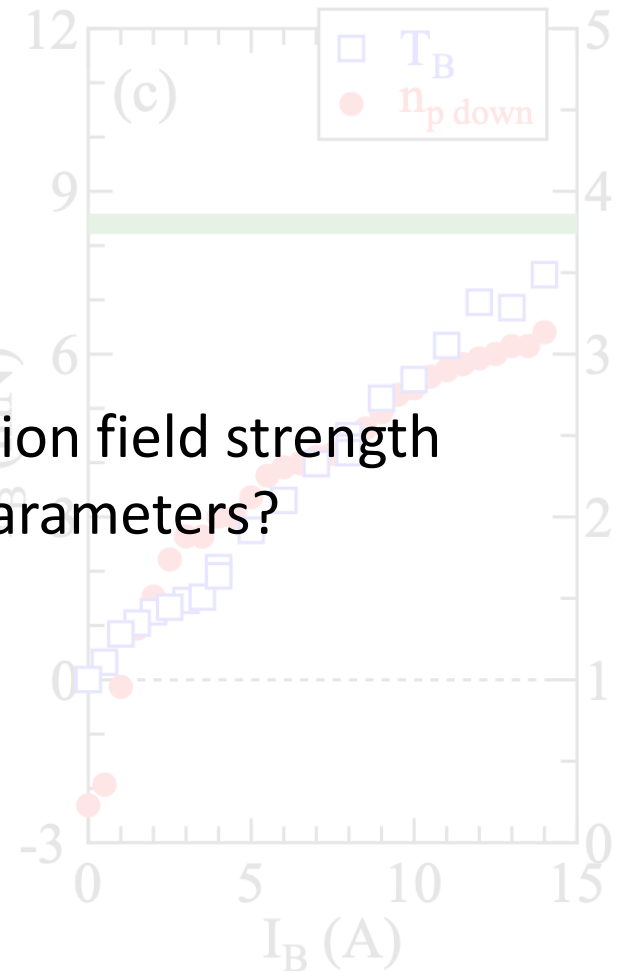


Chen, F. F., et al. "Low-field helicon discharges." *Plasma Physics and Controlled Fusion*

How does the mode transition field strength scale with thruster parameters?

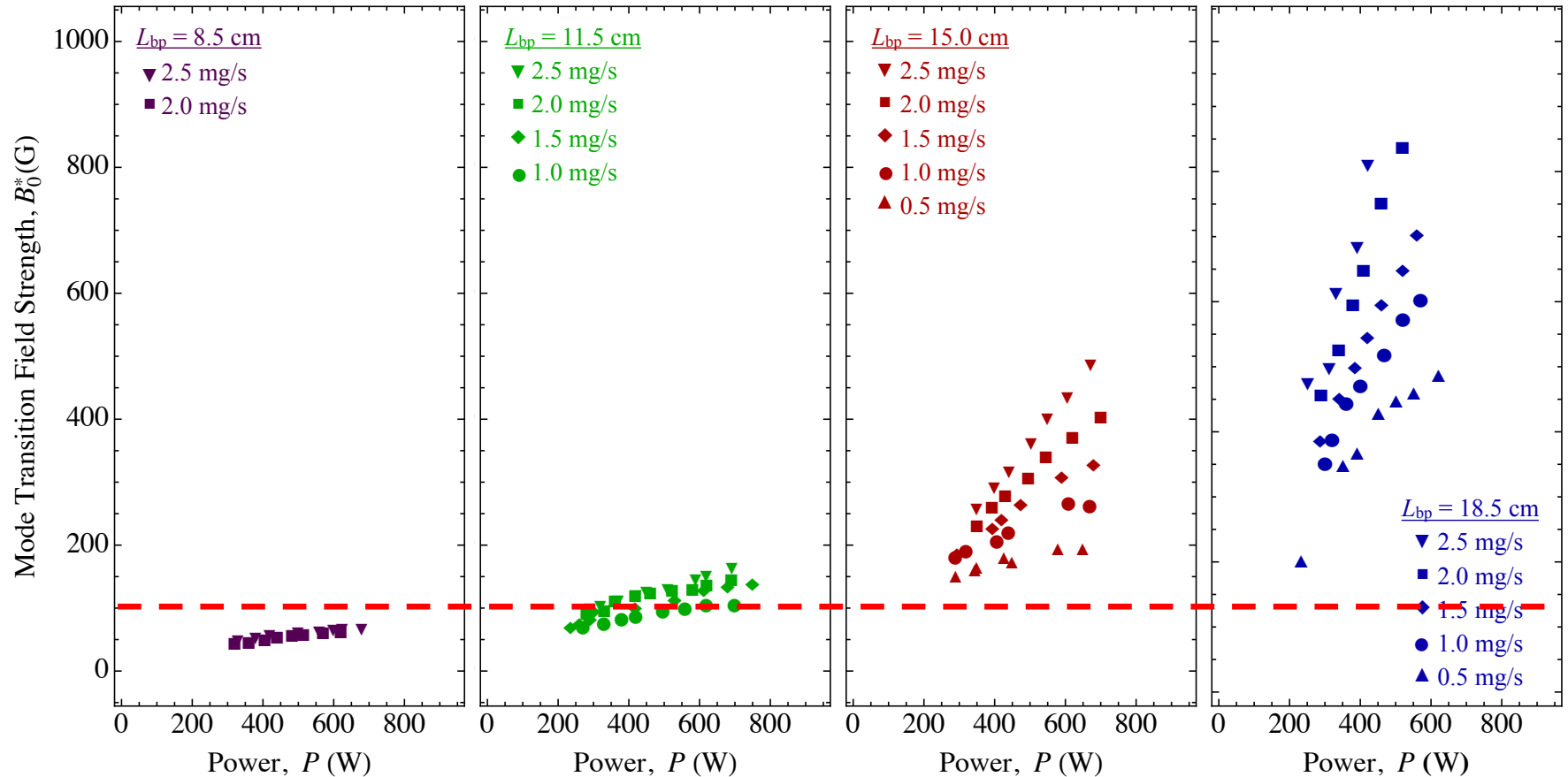
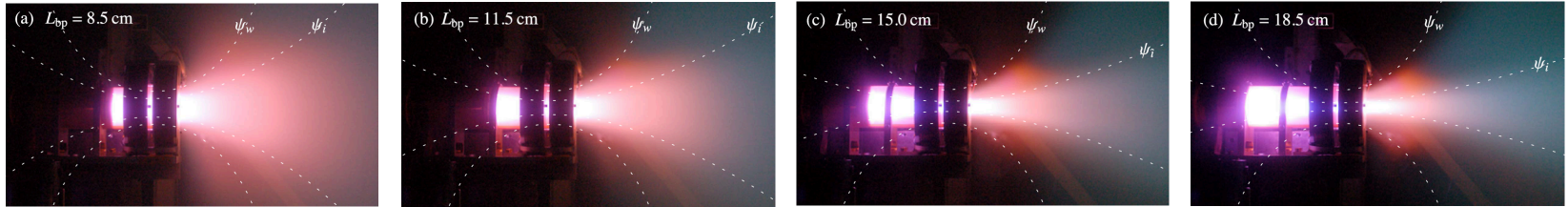


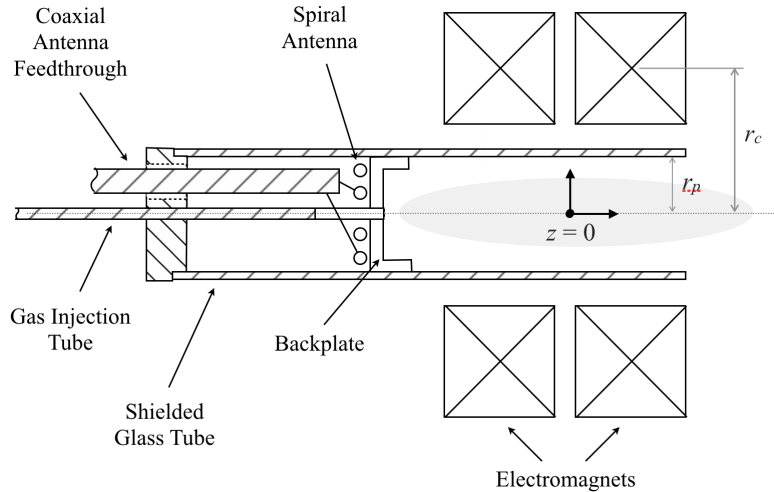
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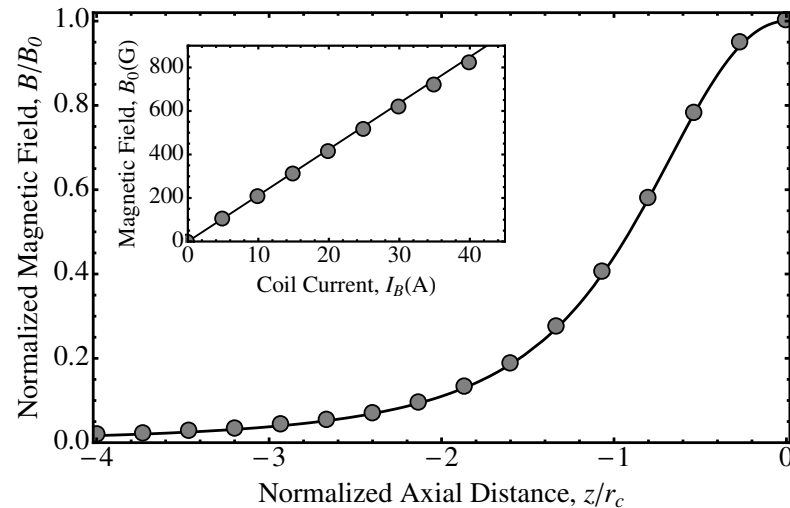
LMFT Measurements





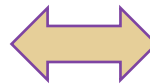
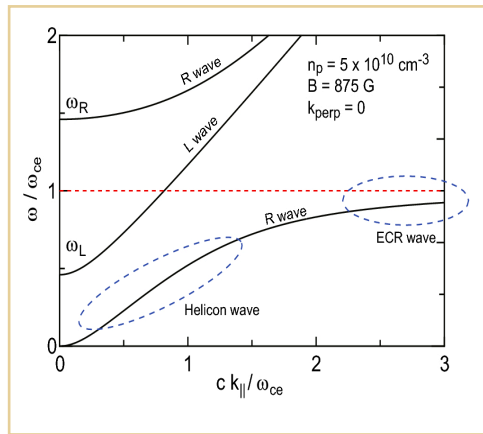
More specifically...

How does the mode transition
field strength scale for a
converging B-field and $m=0$
spiral antenna?

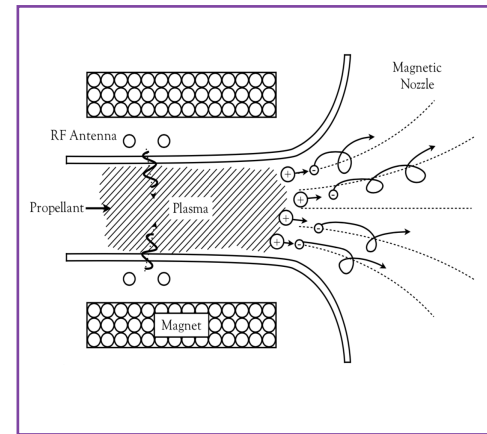


Theoretical Model of the LMFT

RF Absorption



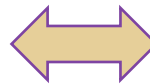
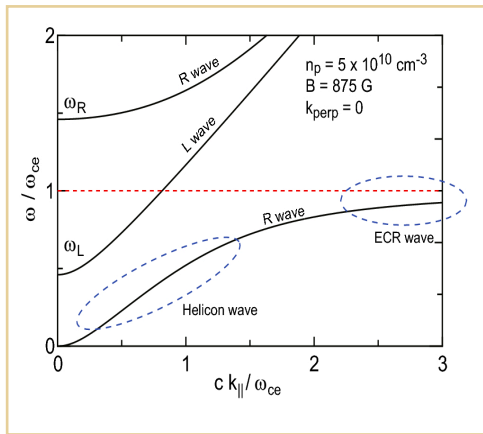
Thruster Global Model



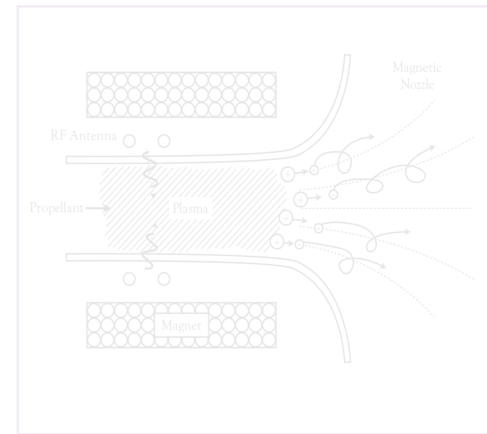
Chabert, Pascal, and Nicholas Braithwaite. *Physics of radio-frequency plasmas*.
Cambridge University Press, 2011.

Theoretical Model of the LMFT

RF Absorption



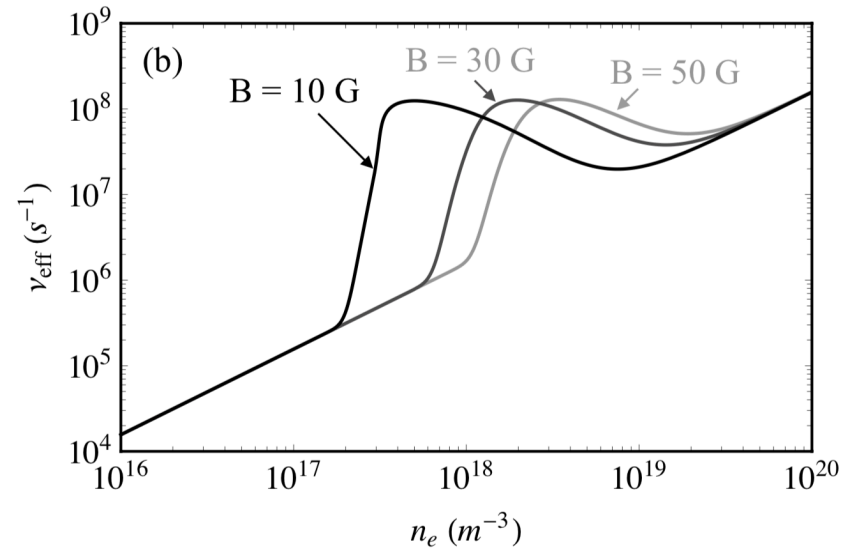
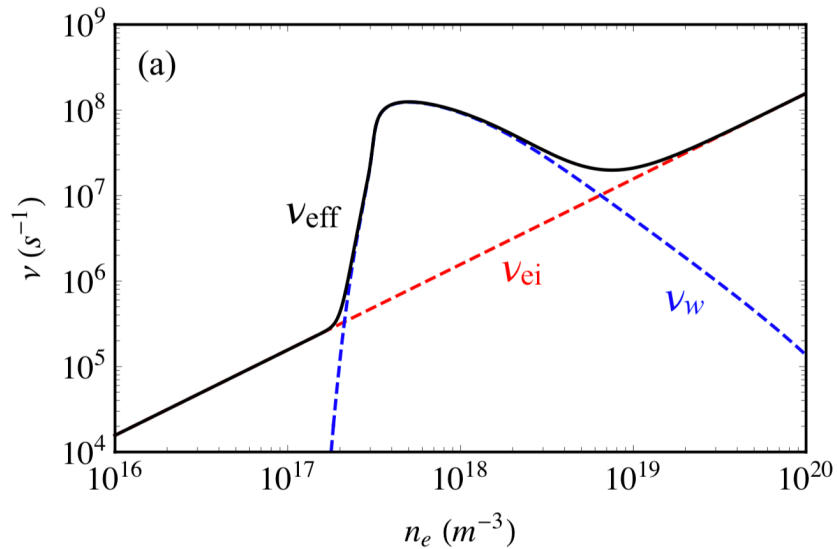
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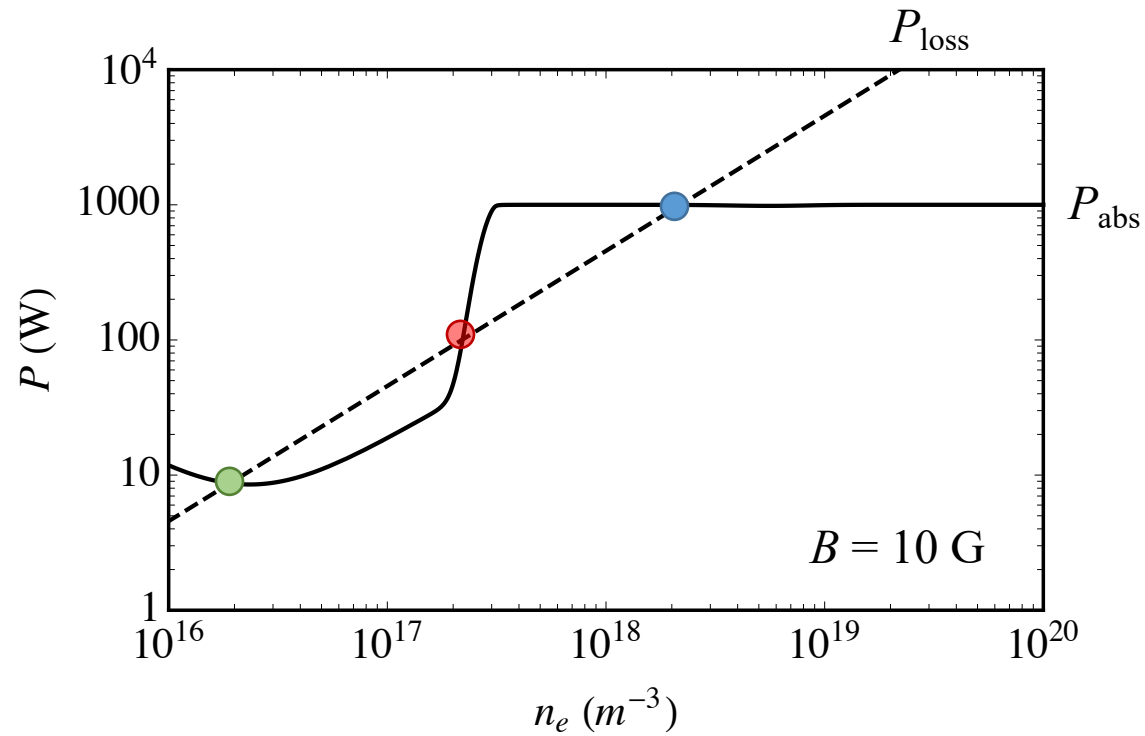
$$kk_z = \frac{\omega\omega_{pe}^2}{c^2\omega_{ce}} \left(1 - \frac{i\nu_{eff}k}{\omega_{ce}k_z} \right)$$



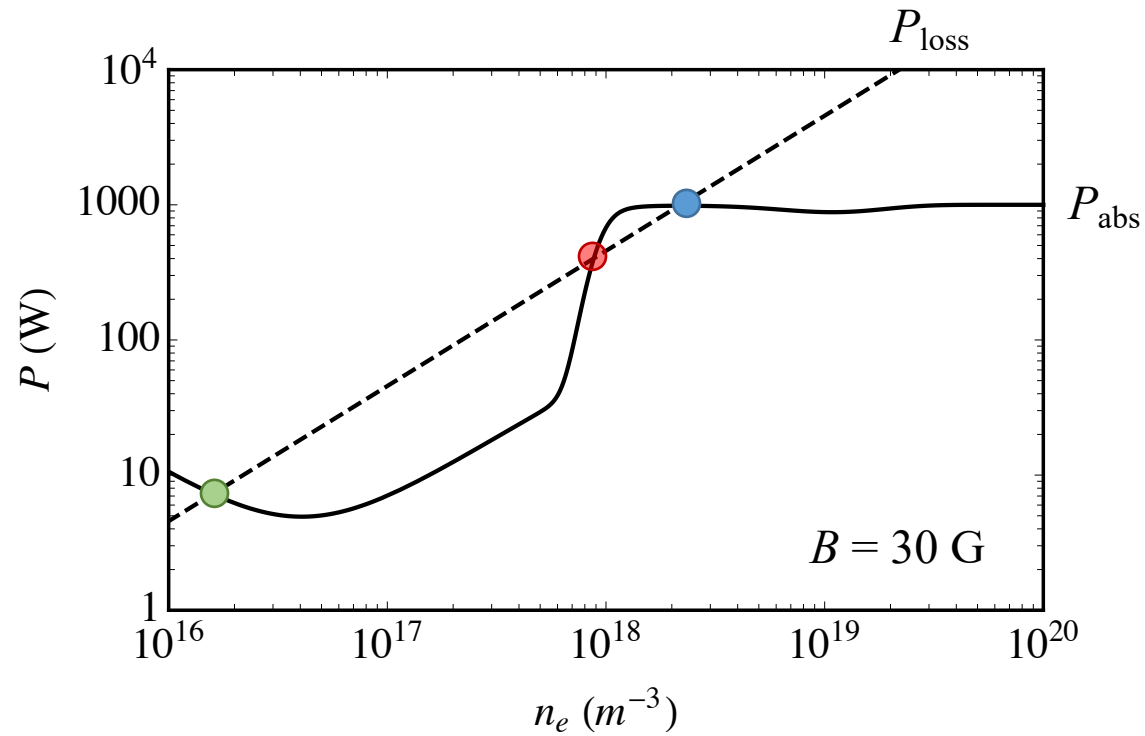
$$\nu_{eff} = \nu_{ei} + \nu_w$$

Chen, Francis F. "Plasma ionization by helicon waves." *Plasma Physics and Controlled Fusion* 33.4 (1991): 339.

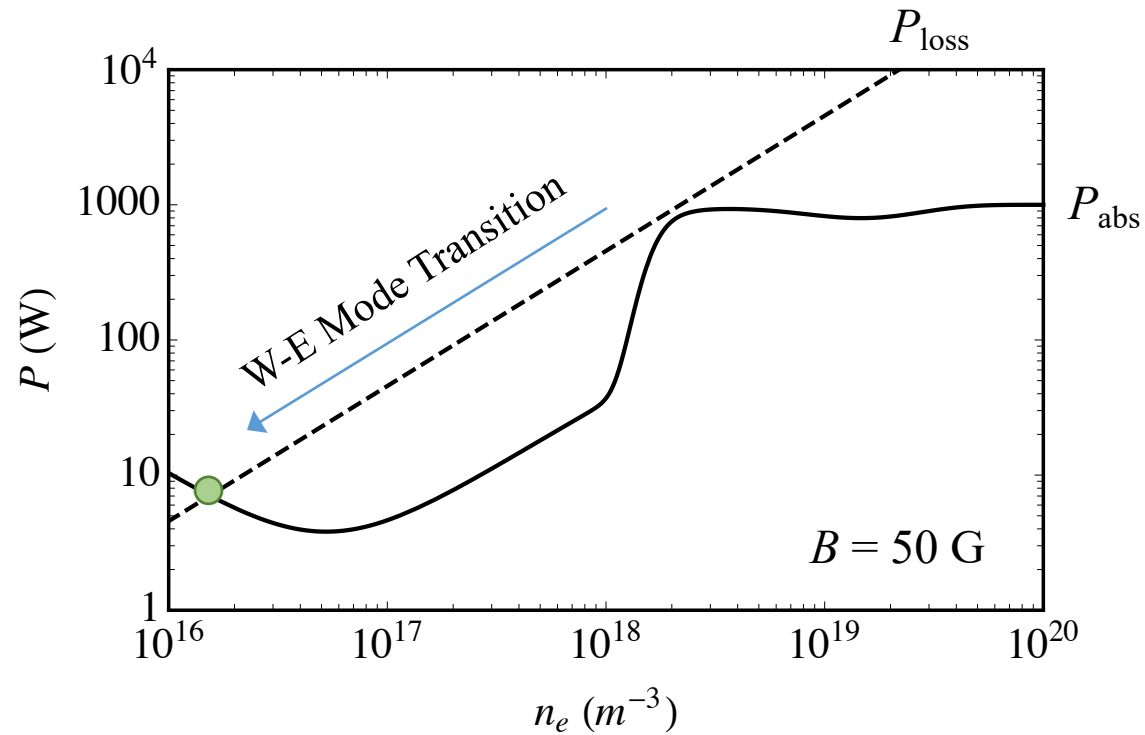
Theoretical Model of the LMFT



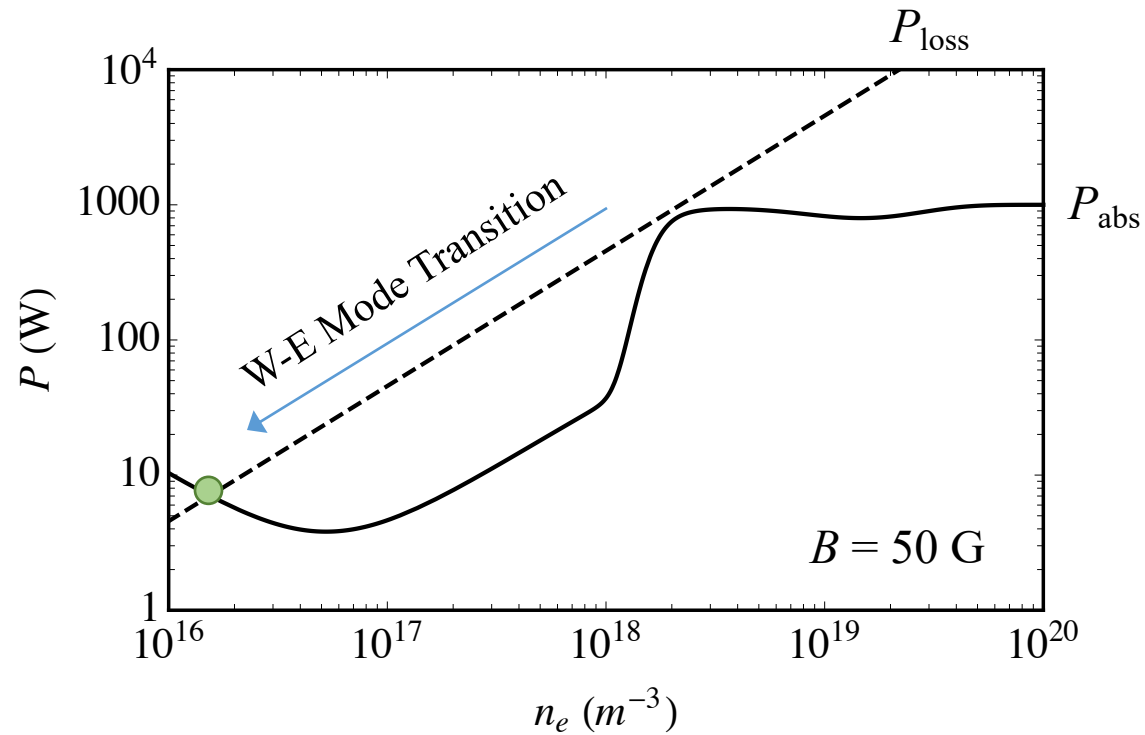
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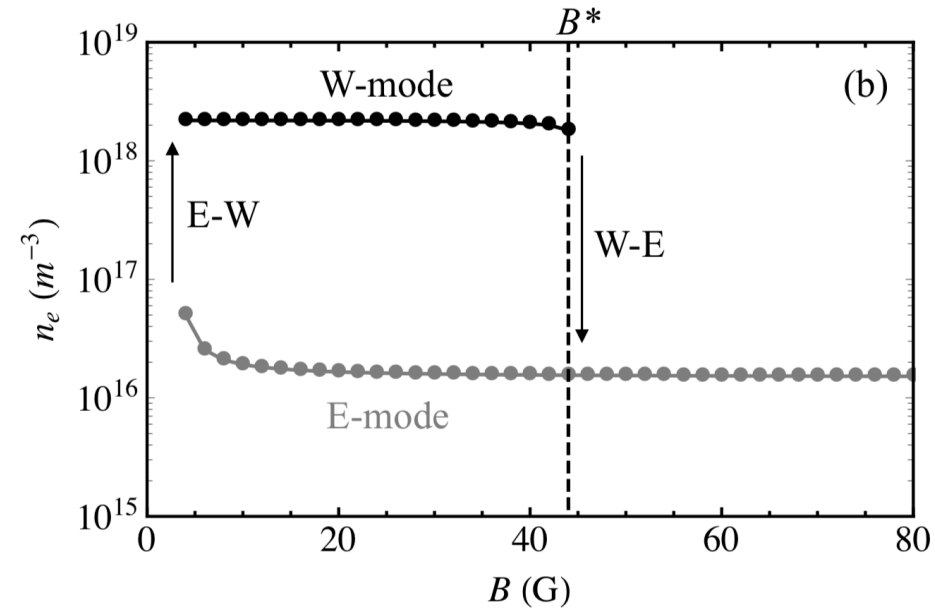
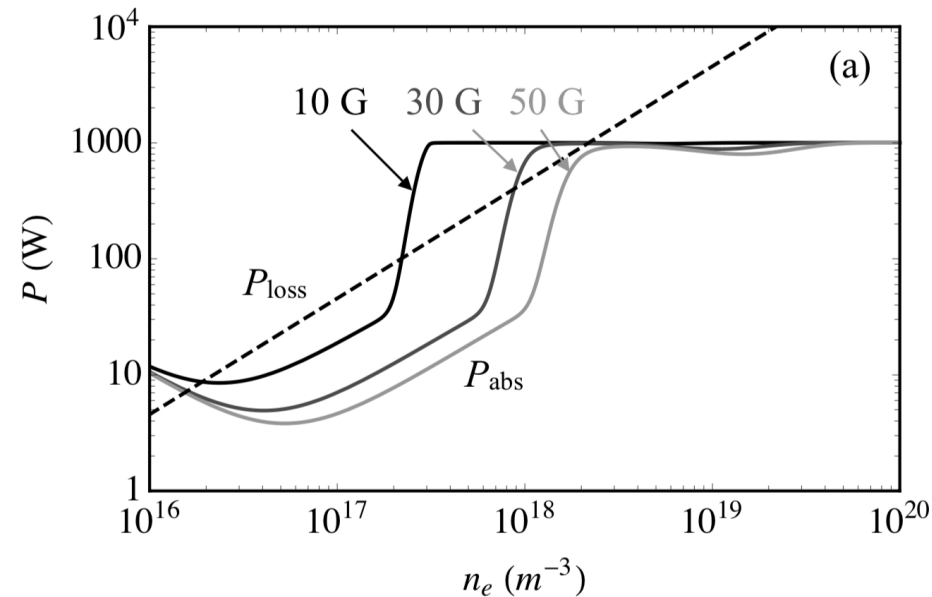


Theoretical Model of the LMFT



wave phase velocity $\gg$ electron thermal velocity

Theoretical Model of the LMFT



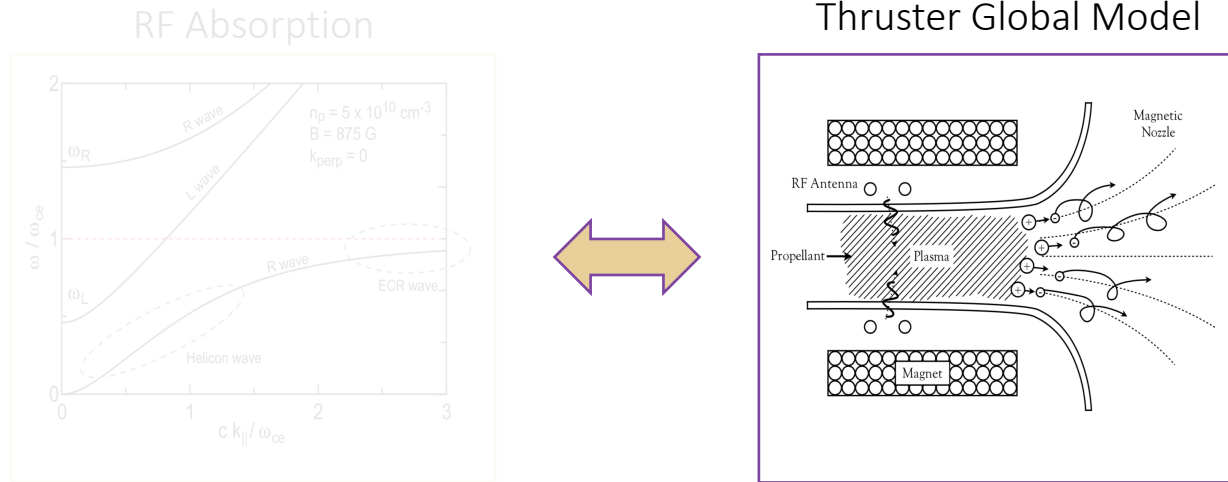
Wave absorption maximum at:

$$B_m = b_0 r_p n_e T_{\text{ev}}^{1/2}$$

Using above plot:

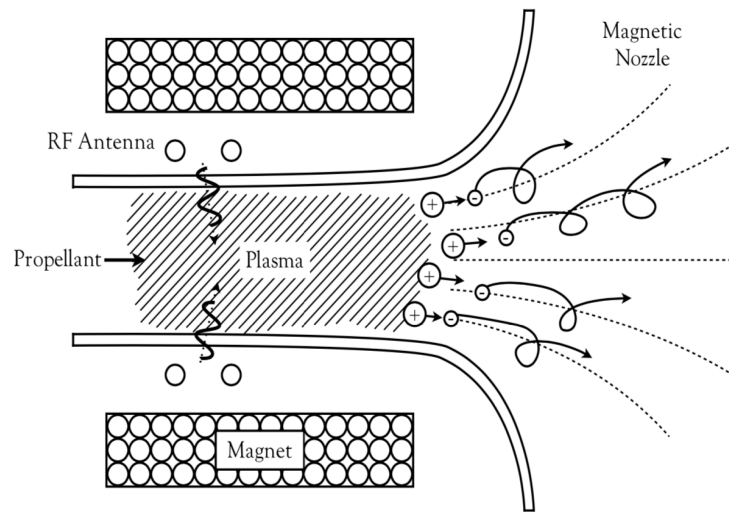
$$B^* \approx \chi B_m$$

Theoretical Model of the LMFT



Chabert, Pascal, and Nicholas Braithwaite. *Physics of radio-frequency plasmas*.
Cambridge University Press, 2011.

Theoretical Model of the LMFT



$$P_{\text{loss}} = n_e u_i \pi r_p^2 (\epsilon_{\text{ke}} + \epsilon_w + \epsilon'_{\text{ion}})$$

(exhaust kinetic power) (power lost to wall)

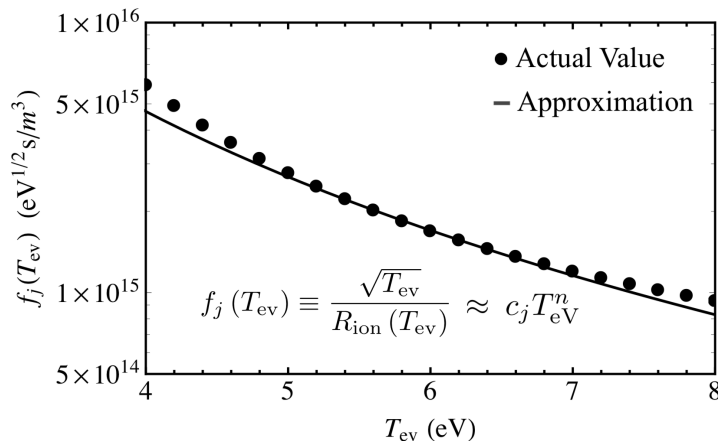
(power lost to ionization)

Power balance:

$$B^* = \frac{\chi b_1 \eta_c P_{\text{RF}}}{2 r_p \mu(\gamma) e T_{\text{ev}} \sqrt{\gamma m_i}}$$

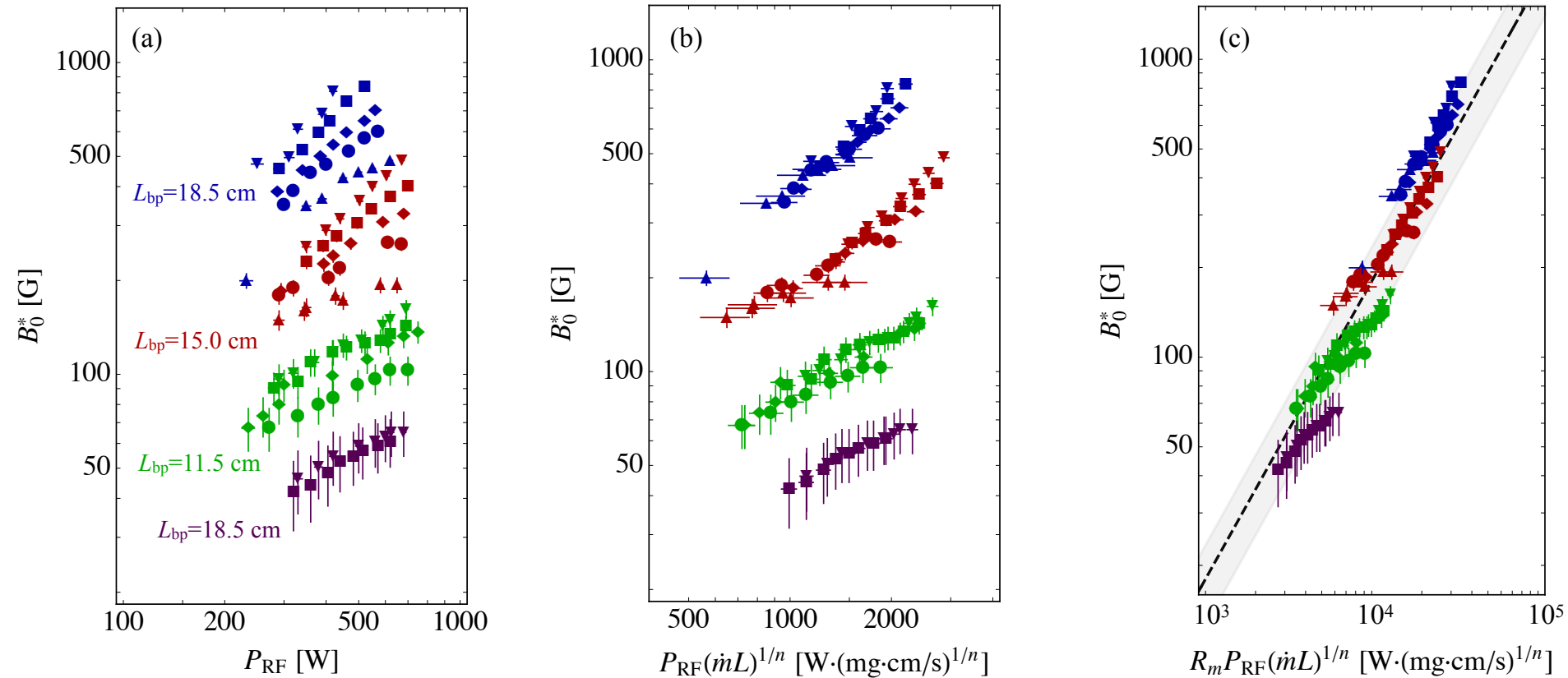
Mass balance:

$$T_{\text{ev}} \approx \left(\frac{b_0 c_j u_n r_p^2 \sqrt{m_i / \gamma}}{b_1 \dot{m} L} \right)^{1/n}$$

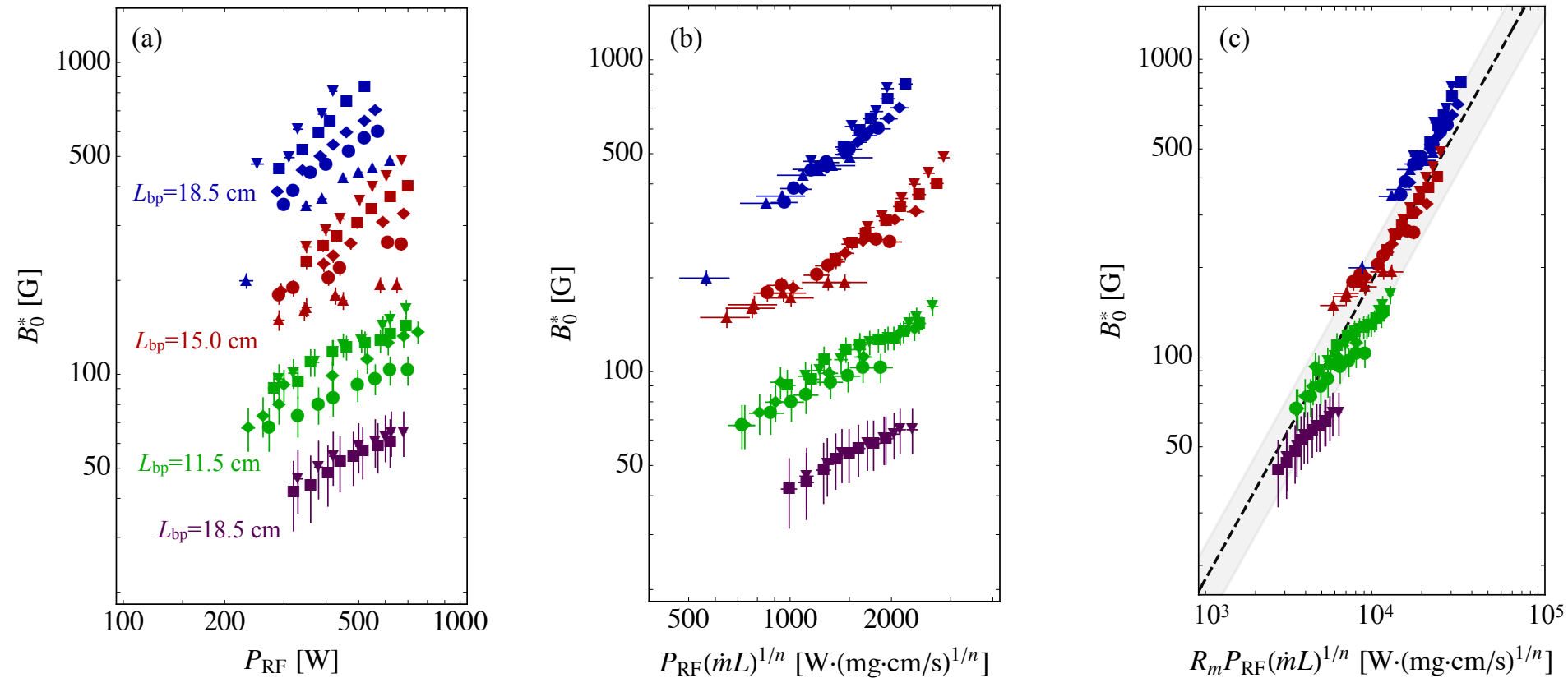


$$B^* = C_1 \frac{P_{\text{RF}}}{r_p \sqrt{m_i}} \left(\frac{\dot{m} L}{c_j r_p^2} \right)^{1/n}$$

LMFT Scaling with Thruster Parameters

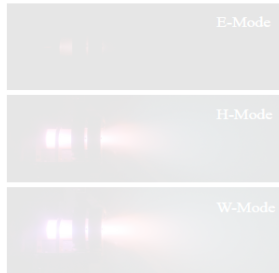


LMFT Scaling with Thruster Parameters



Transition occurs when Landau damping of wave energy can longer sustain plasma

Mode Transitions in Aerospace Plasmas

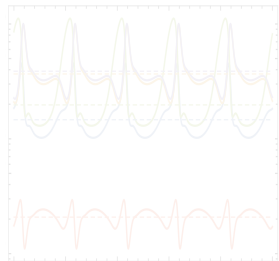


Topic 1: Mode transitions in helicon thrusters



Image: MSNW

Topic 2: Critical velocities for plasma aerocapture



Topic 3: Data-driven discovery of mode transition physics

Generating Forces using Magnetic Fields in Space

Magnetic Sail

Zubrin and Andrews. *J. Spacecraft and Rockets* 28.2 (1991): 197-203.

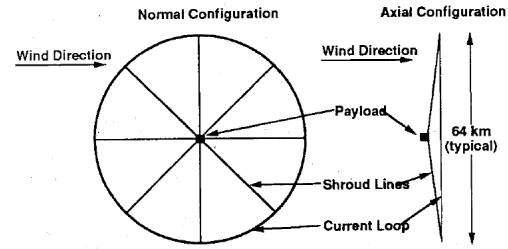
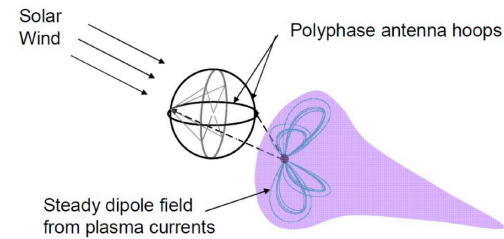


Fig. 1 Magsail deployed with payload.

Plasma Magnetic Sail (M2P2)

Winglee et al. *AIP Conference Proceedings*. Vol. 504. No. 1. American Institute of Physics, 2000.

Slough. *30th International Electric Propulsion Conference, Florence, Italy, IEPC-2007-15*. 2007.



Plasma Magnetoshell

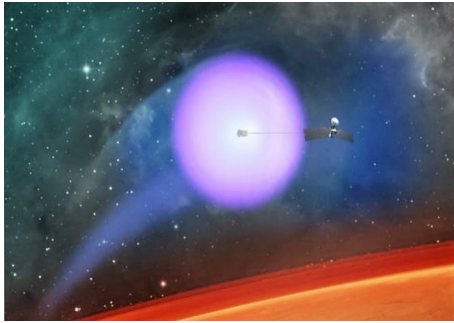
Slough, Kirtley, and Pancotti. *32nd International Electric Propulsion Conference*. 2011.

Kirtley. NIAC Phase I, NNX12AR12G Final Report (2012).



Image: MSNW

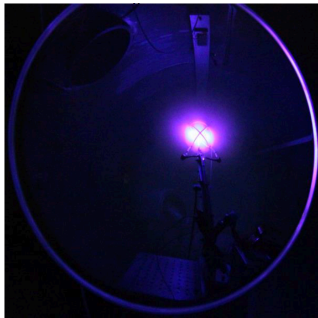
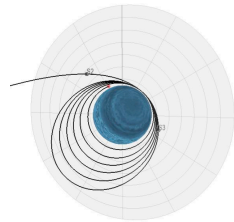
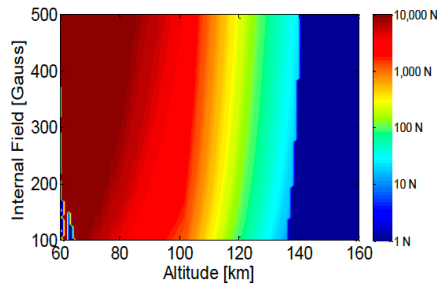
Plasma Magnetoshell Aerocapture



“Plasma parachute” enables high-velocity aerocapture at lower densities compared to aeroshells

Theoretical modeling and mission analysis:

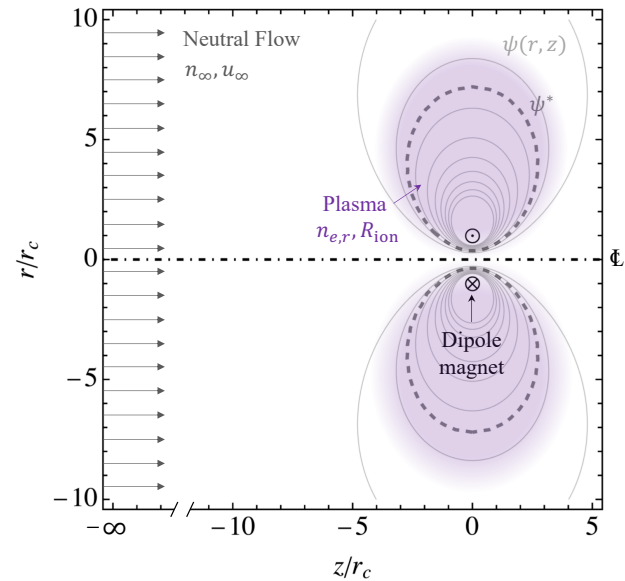
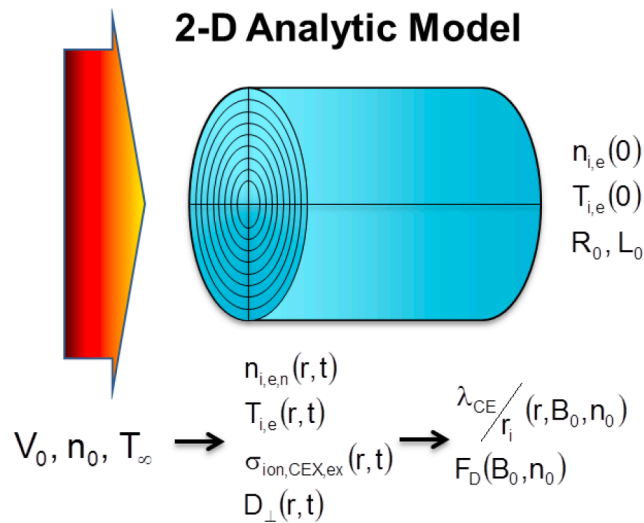
- Neptune: enables 1,000 kg orbiter spacecraft
- Mars: enables orbit insertion of 60 MT payload
- Significant reduction in TPS requirements



Proof-of-concept tests using pulsed MPDT exhaust plume

- Thrust stand → 1,000X increase in drag over aerodynamic

Magnetoshell Analytical Model



Original Model (Kirtley, 2012):

- Magnetic “layers”
- Cylindrical plasma
- No particle trajectories
- *Ad hoc* drag-area
- Partial mass/energy transfer

Our Model (Kelly and Little, 2019):

- Dipole magnetic field
- Plasma dipole equilibrium
- Particle trajectories
- Self-consistent drag area
- Full mass/energy transfer

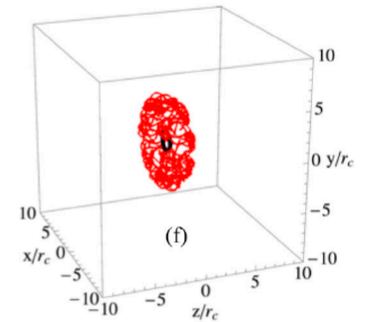
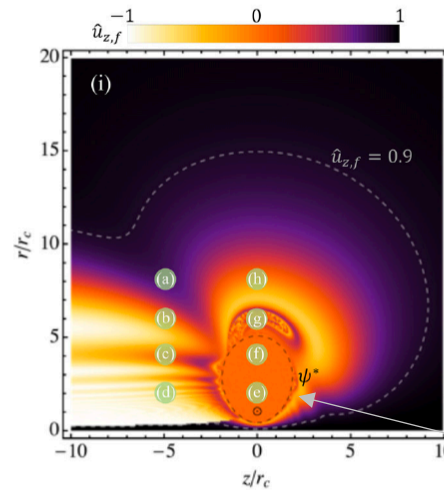
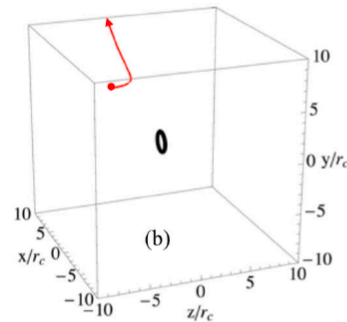
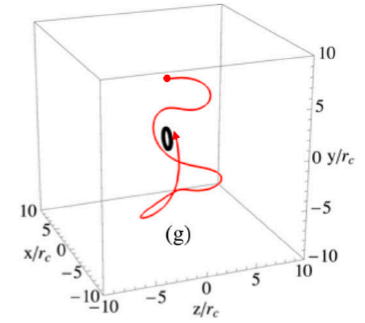
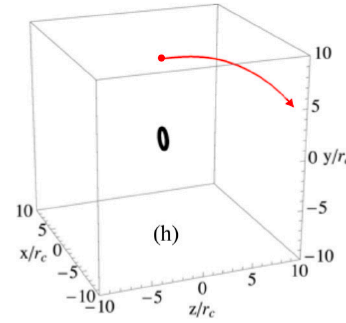
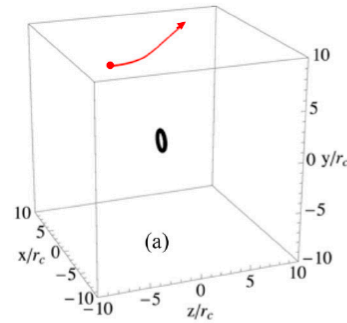
How well does the magnetoshell utilize mass/energy from the flow?

Behavior of Newly Ionized Flow Particles

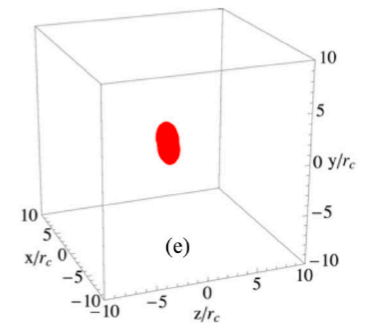
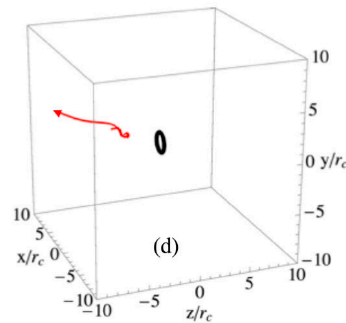
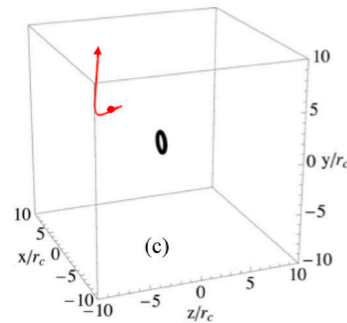
$$\frac{d\hat{\mathbf{u}}}{d\hat{t}} = \frac{1}{\rho_L} \hat{\mathbf{u}} \times \hat{\mathbf{B}}$$

$$\frac{d\hat{\mathbf{r}}}{d\hat{t}} = \hat{\mathbf{u}}$$

$$\rho_L = \frac{m_i u_\infty}{q_i B_0 r_c}$$



$$\hat{\psi}^* = \sqrt{2\rho_L}$$



Wake Formation and Flow Utilization



“Stream” neutral continuity:

$$\nabla \cdot (n_{sn} \mathbf{u}_{sn}) = -R_{tot} n_{sn} n_e$$

$$R_{tot} = R_{ion} + R_{cx} \quad (\text{ionization + charge exchange})$$

$$\hat{n}_{sn} = \exp(-\zeta_{tot} I_n)$$

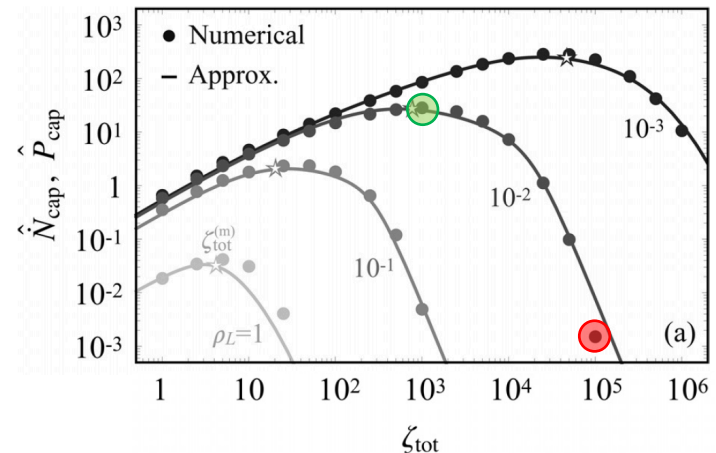
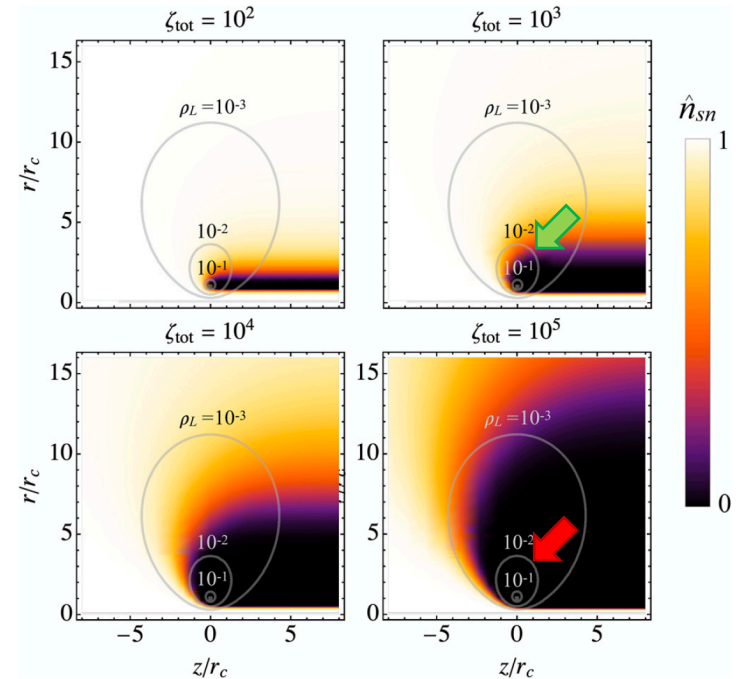
$$I_n = \int_{-\infty}^{\hat{z}} \left(\frac{\hat{\psi}}{\hat{\psi}_r} \right)^\alpha d\hat{z} \quad (\text{magnetic topology} + n_e\text{-distribution})$$

$$\zeta_{tot} \equiv \frac{R_{tot} n_{e,r}}{u_\infty / r_c} \sim \frac{(\text{Ionization frequency})}{(\text{Neutral transit frequency})}$$

$$\dot{N}_{cap} = \oint_{\psi > \psi^*} R_{tot} n_{sn} n_e dV \quad P_{cap} = \frac{1}{2} m_{sn} u_\infty^2 \dot{N}_{cap}$$

$$\hat{N}_{cap} = \hat{P}_{cap} = \zeta_{tot} I_{sn}(\rho_L, \zeta_{tot})$$

$$\rho_L = \frac{m_i u_\infty}{q_i B_0 r_c} \sim \frac{(\text{Characteristic Larmor radius})}{(\text{Magnetic coil radius})}$$



How well does the magnetoshell utilize mass/energy from the flow?

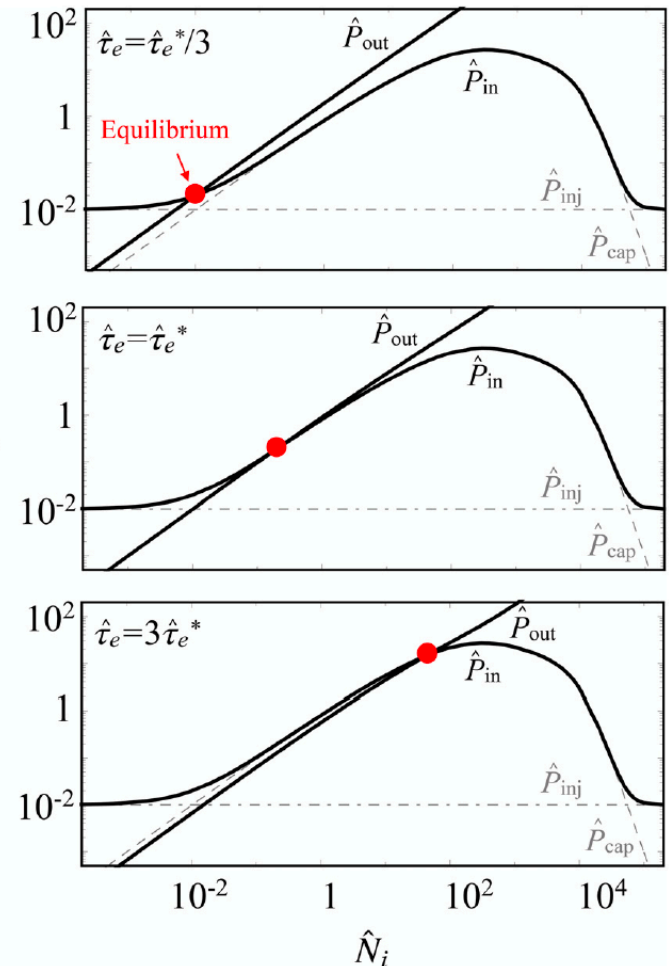
Power (and mass) balance in ψ^* :

$$\underbrace{\hat{P}_{\text{cap}} + \hat{P}_{\text{inj}}}_{\hat{P}_{\text{in}}} = \underbrace{\frac{\hat{N}_i}{\hat{\tau}_e} (\hat{T}_e + \hat{\varepsilon}_{\text{ion}})}_{\hat{P}_{\text{out}}} + \hat{N}_{\text{cap}} \hat{T}_i$$

$\hat{P}_{\text{cap}} + \hat{P}_{\text{inj}}$ (Power captured from the stream neutrals)
 $\frac{\hat{N}_i}{\hat{\tau}_e} (\hat{T}_e + \hat{\varepsilon}_{\text{ion}})$ (Diffusion of electron thermal power)
 $\hat{N}_{\text{cap}} \hat{T}_i$ (Net diffusion of ion + 2n thermal power)
 $\hat{\varepsilon}_{\text{ion}}$ (Ionization power loss)

$$\hat{\tau}_e^* = \left(\frac{\hat{T}_e + \hat{\varepsilon}_{\text{ion}}}{1 - \hat{T}_i} \right) \hat{\tau}_{\text{cap}}$$

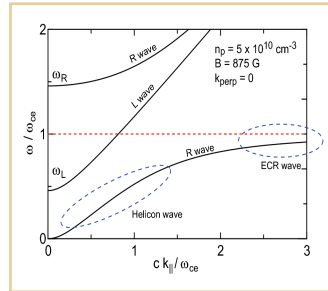
$$\hat{\tau}_{\text{cap}} = \frac{u_\infty / r_c}{R_{\text{tot}} n_\infty}$$



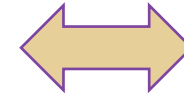
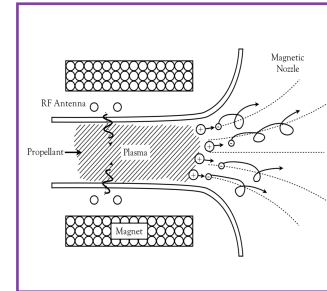
*Critical condition on electron confinement time

Mode Transitions in Aerospace Plasmas

RF Absorption

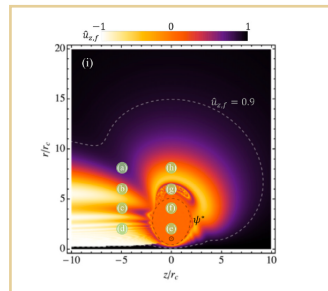


Thruster Global Model

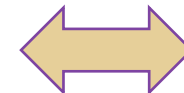
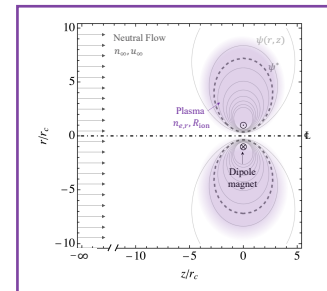


MODE
TRANSITION

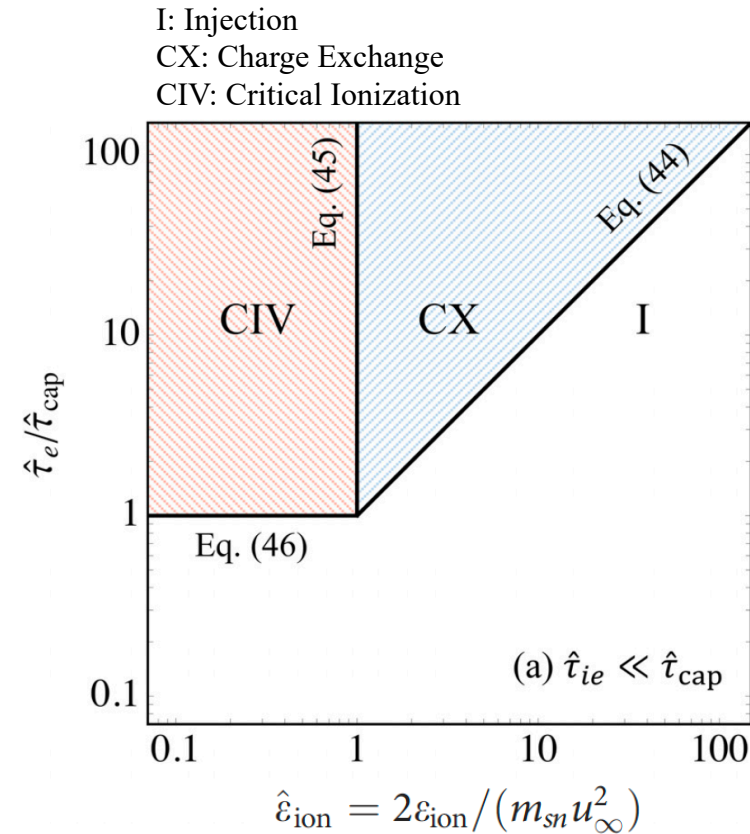
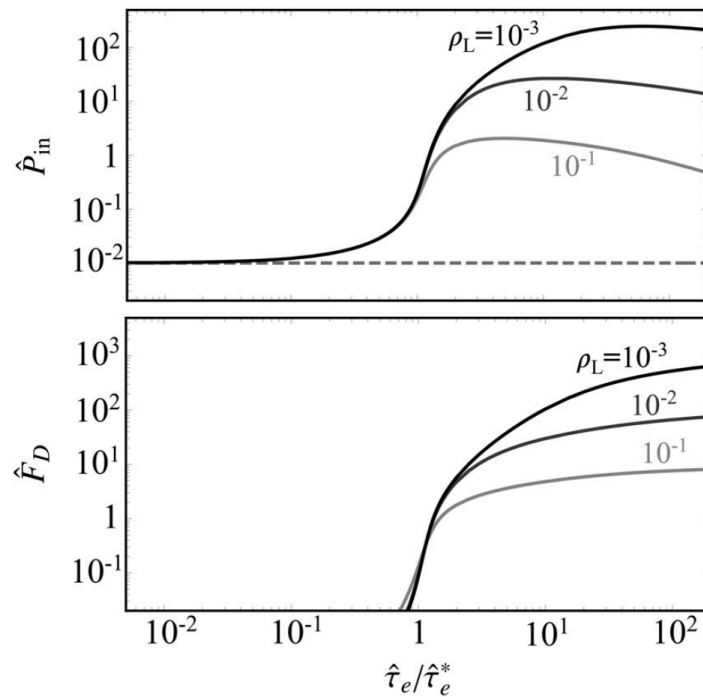
Flow Absorption



Magnetoshell Global Model

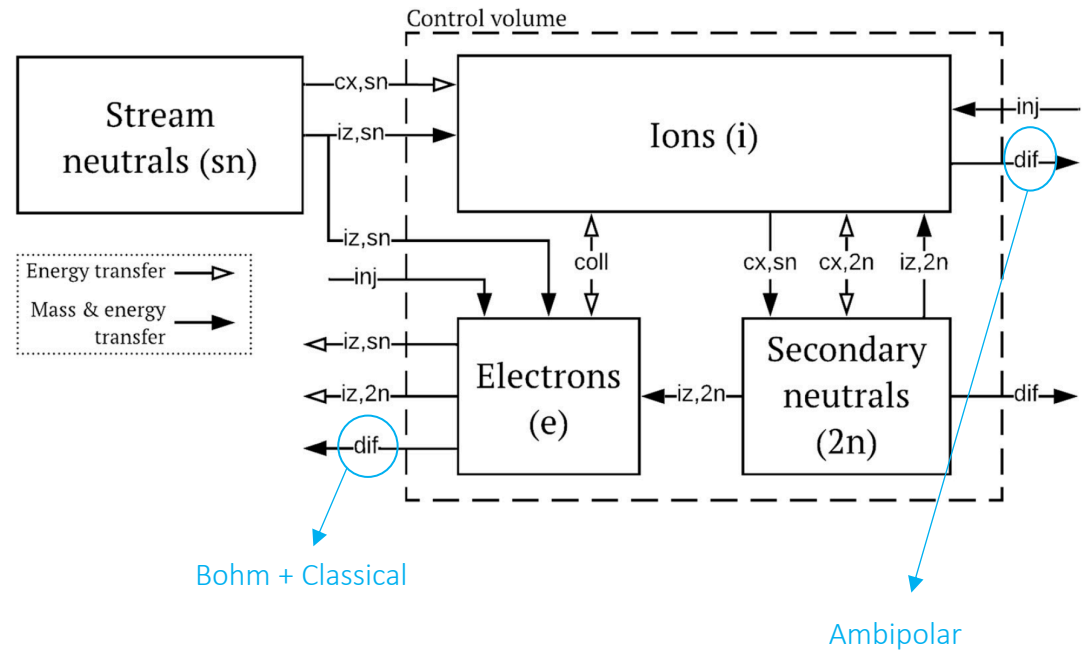
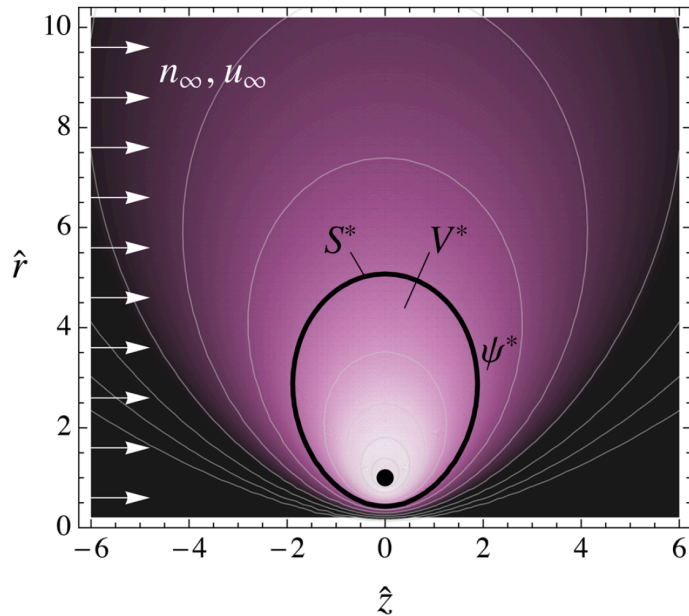


Influence of Mode Transition on Performance



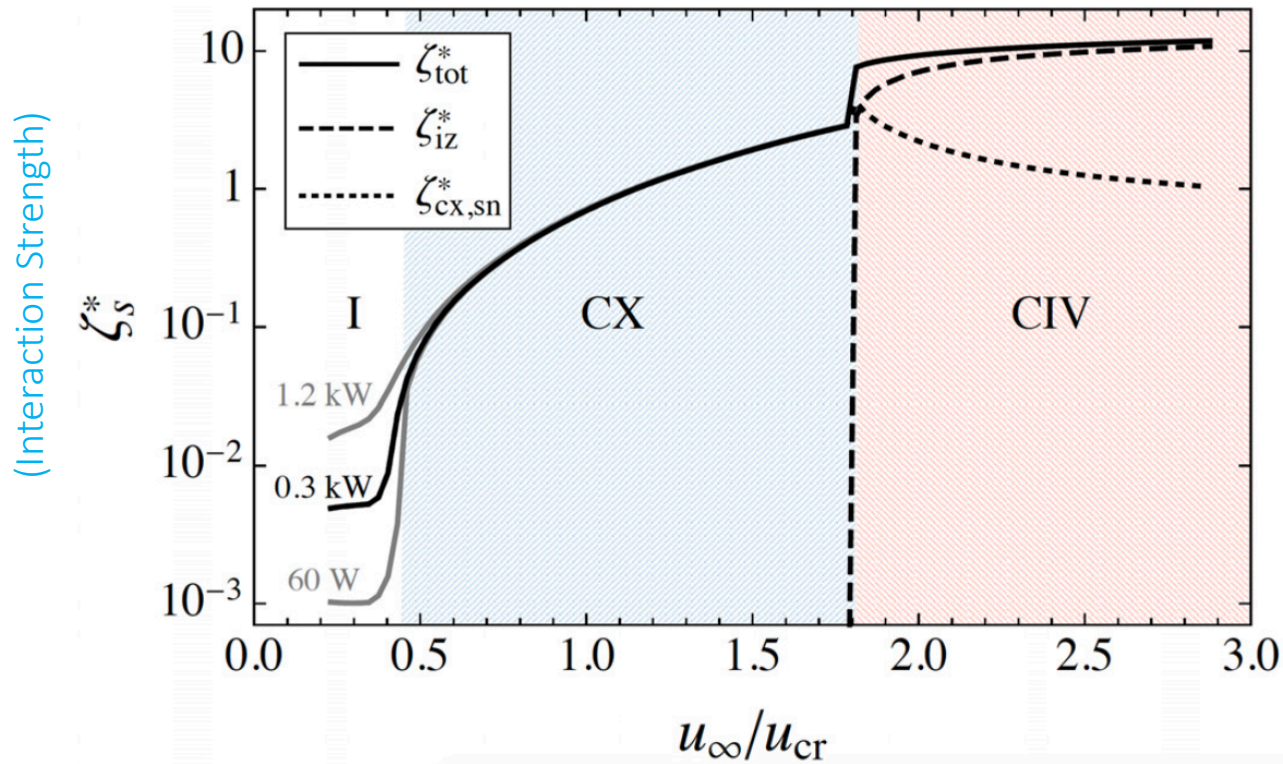
Increasing electron energy confinement time critical to performance!

Do our predictions hold for “standard” diffusion models?

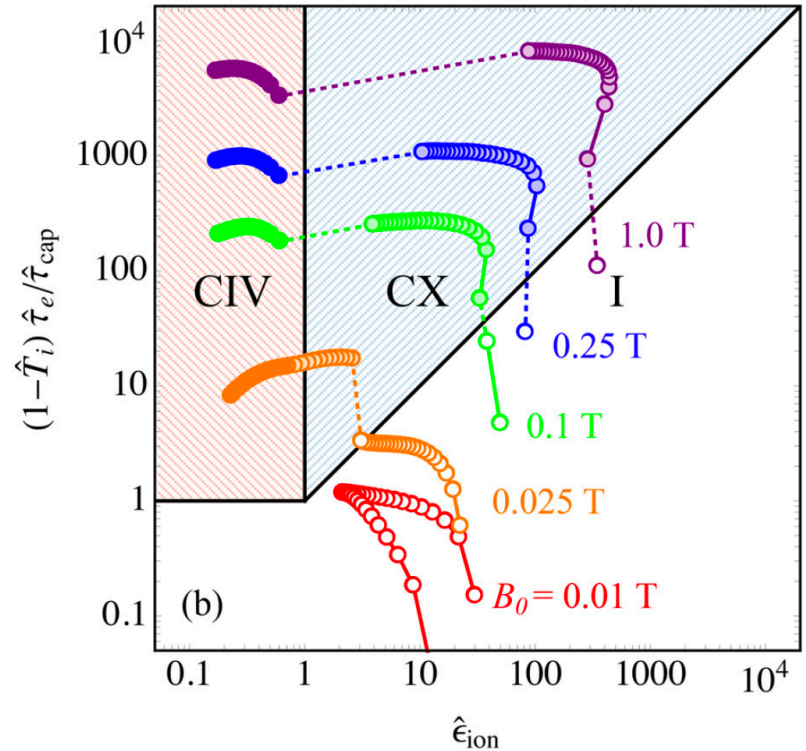
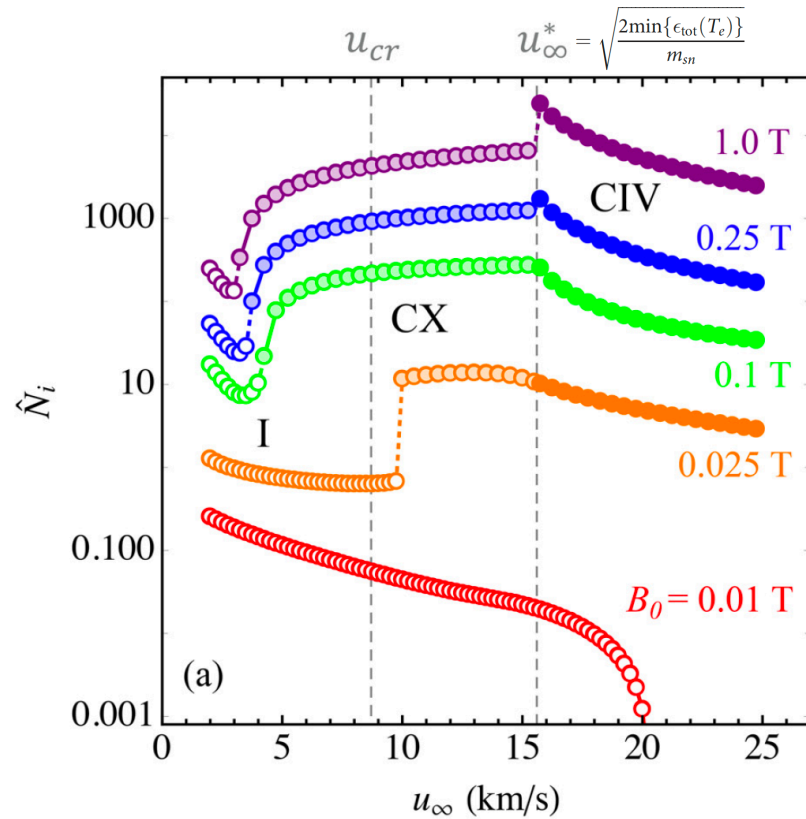


Mode Transition with Increasing Flow Velocity

$$\zeta_s^* = \frac{R_s n_e^*}{u_\infty / r_c}$$



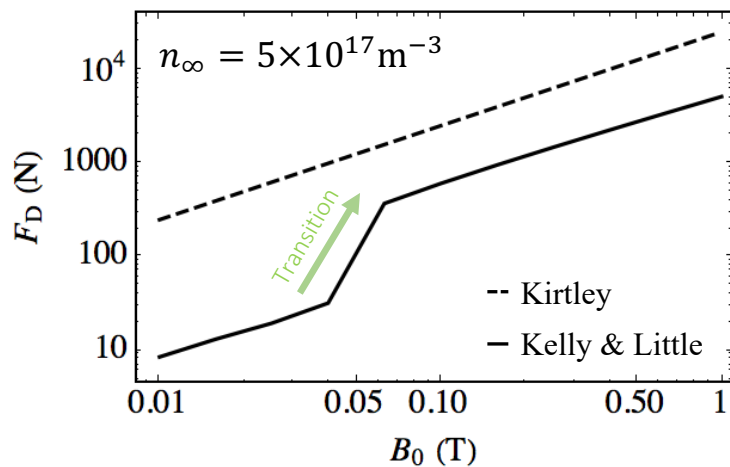
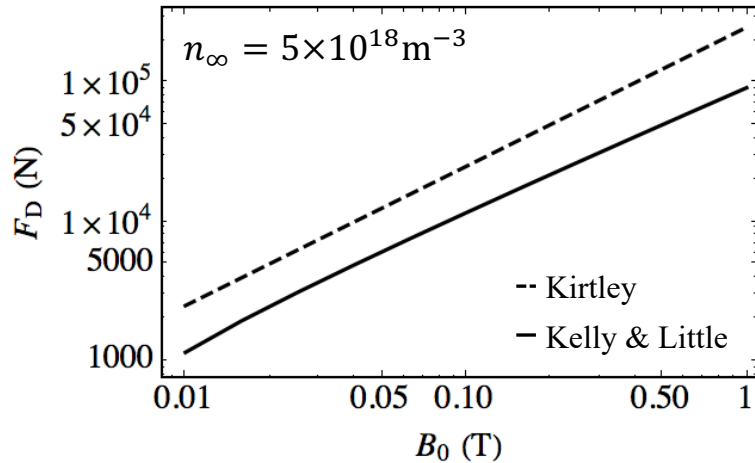
Map of Magnetoshell Operating Modes



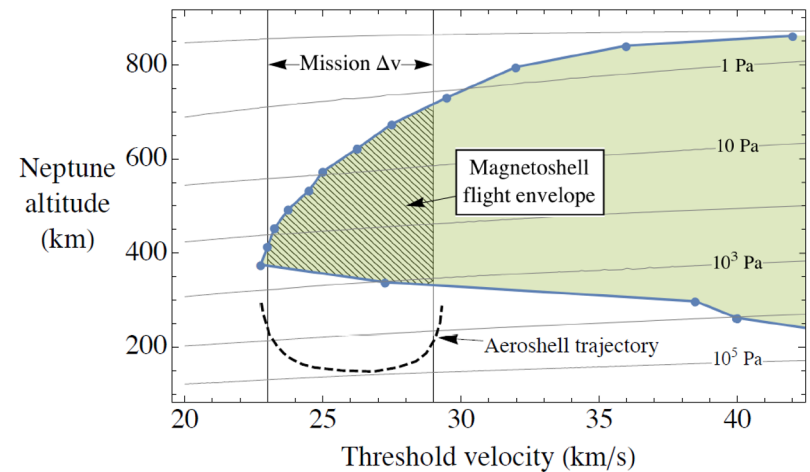
How does the performance compare to the original model?

Performance Comparison

Neptune Orbiter: $r_c = 2$ meters
 $u_\infty = 25$ km/s



Flight envelope of magnetoshell viability at Neptune



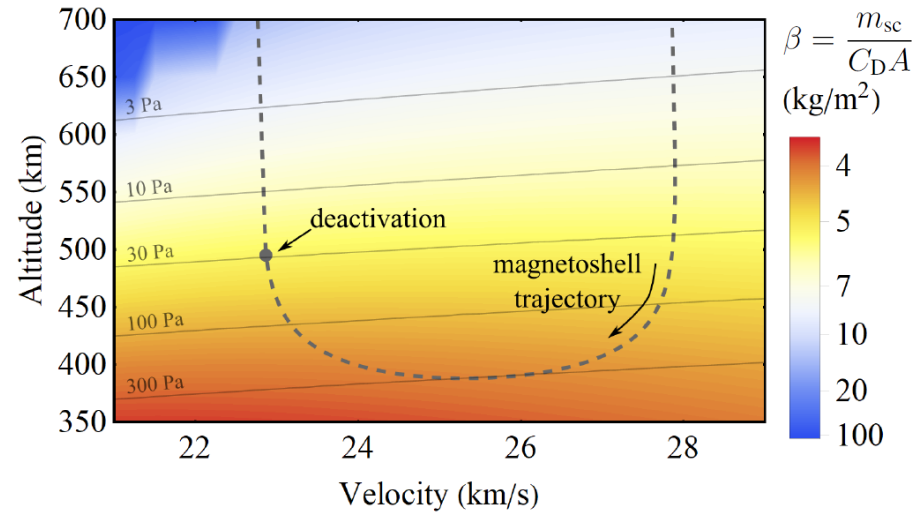
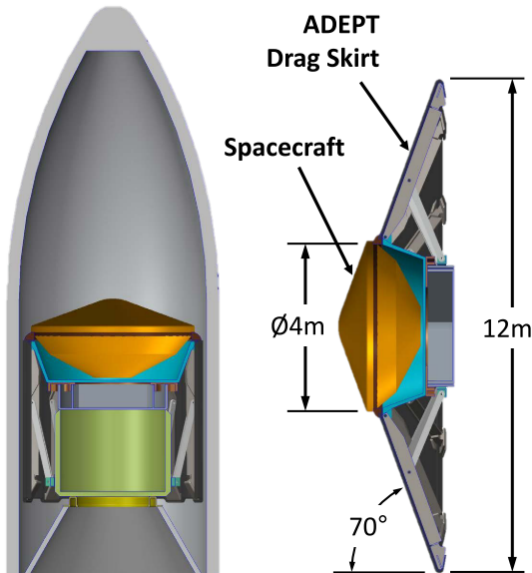
Kelly and Little. 36th International Electric Propulsion Conference, Vienna, Austria, IEPC Paper 2019-202. 2019.

Do the benefits still outweigh the added mass/complexity?

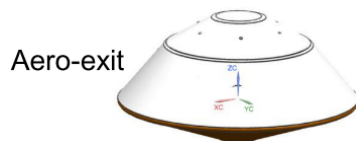
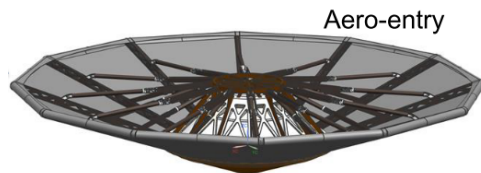
Magnetoshell Aerocapture for Neptune Orbiter Mission

Neptune DMA Concept with ADEPT

(Stowed in 5m Fairing) - (Deployed for Entry)



Kelly and Little. 42nd IEEE Aerospace Conference, 2.0304, 2021.



+70% payload mass

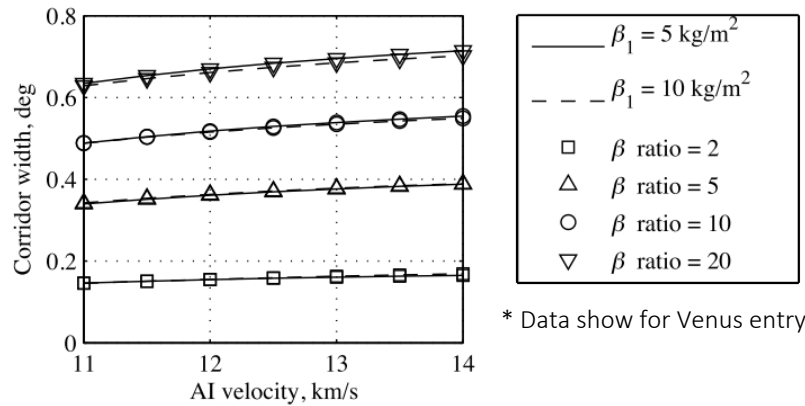
-30% aerocapture system mass

-30% peak heat flux , **-45%** total heat load

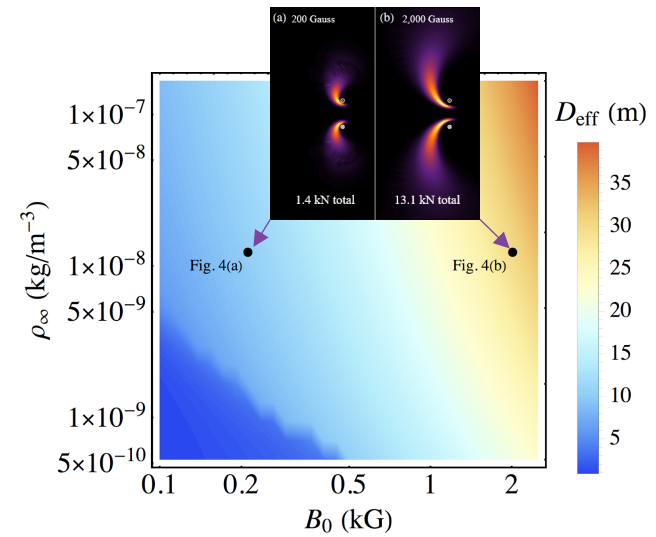
16x improvement in variable drag control

Magnetoshell Aerocapture for Neptune Orbiter Mission

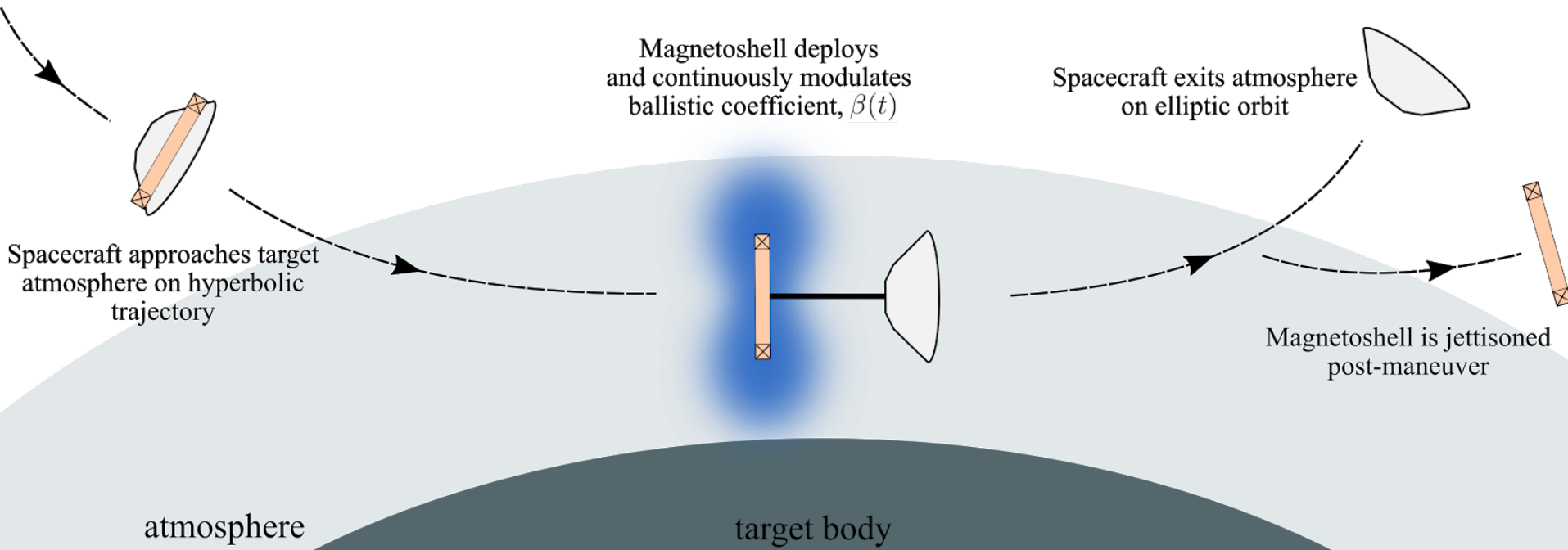
Variable drag increases entry corridor width



Putnam and Braun, J. Spacecr. Rockets **51**, 139 (2014)

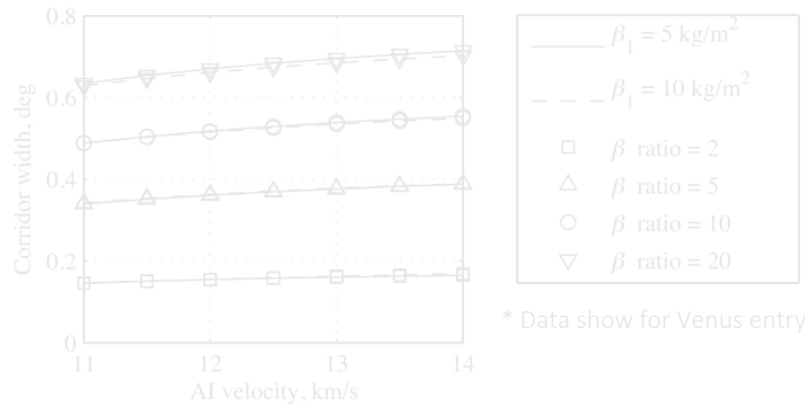


Kelly and Little. 42nd IEEE Aerospace Conference, 2.0304, 2021.



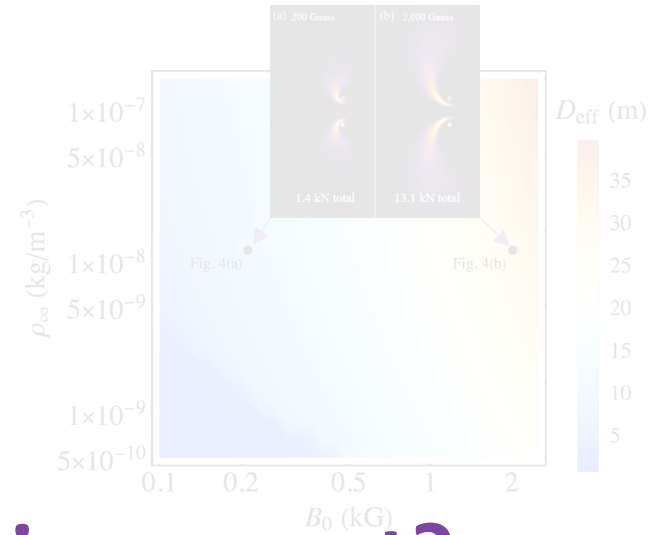
Magnetoshell Aerocapture for Neptune Orbiter Mission

Variable drag increases entry corridor width



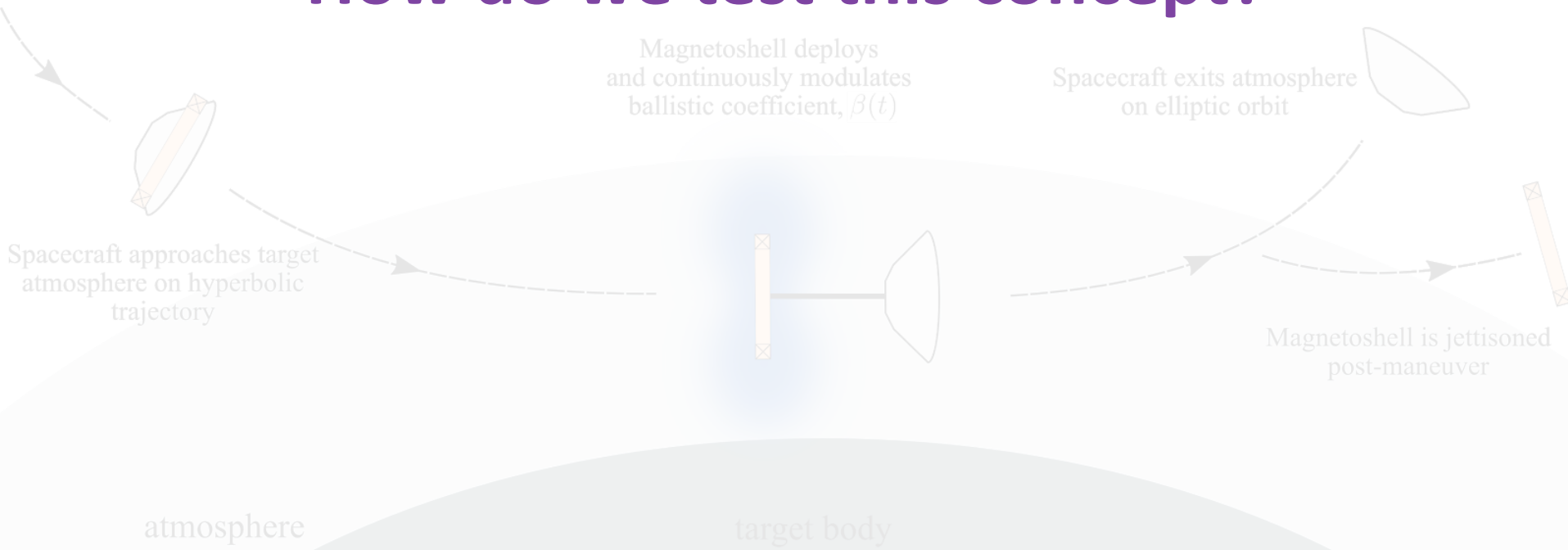
* Data show for Venus entry

Putnam and Brun, J. Spacecr. Rocket, 51, 139 (2014)

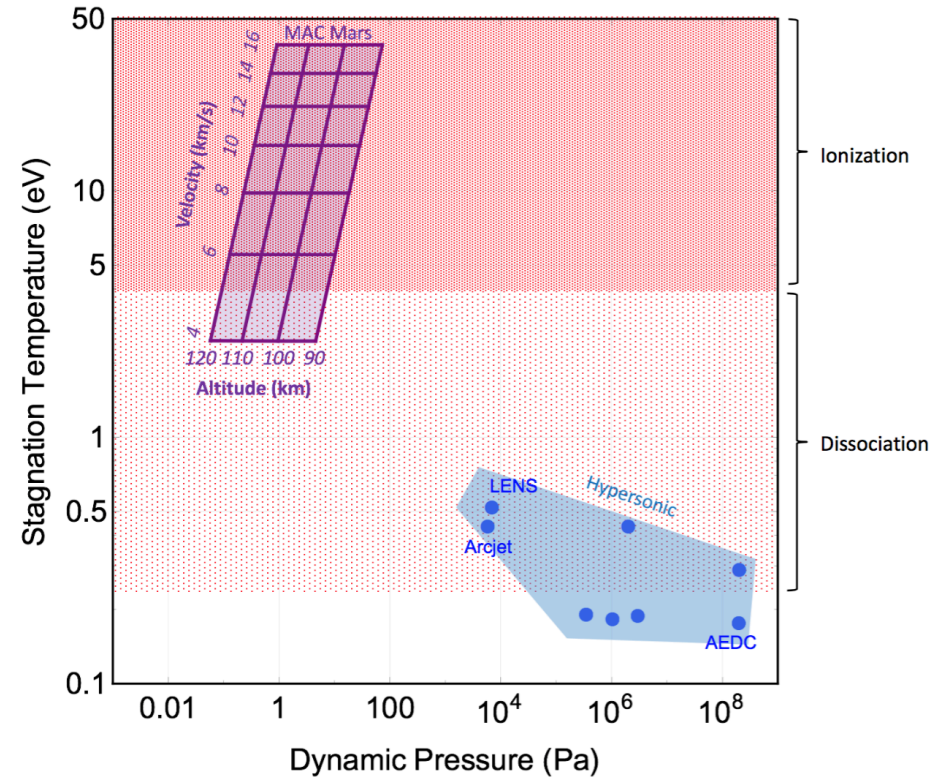
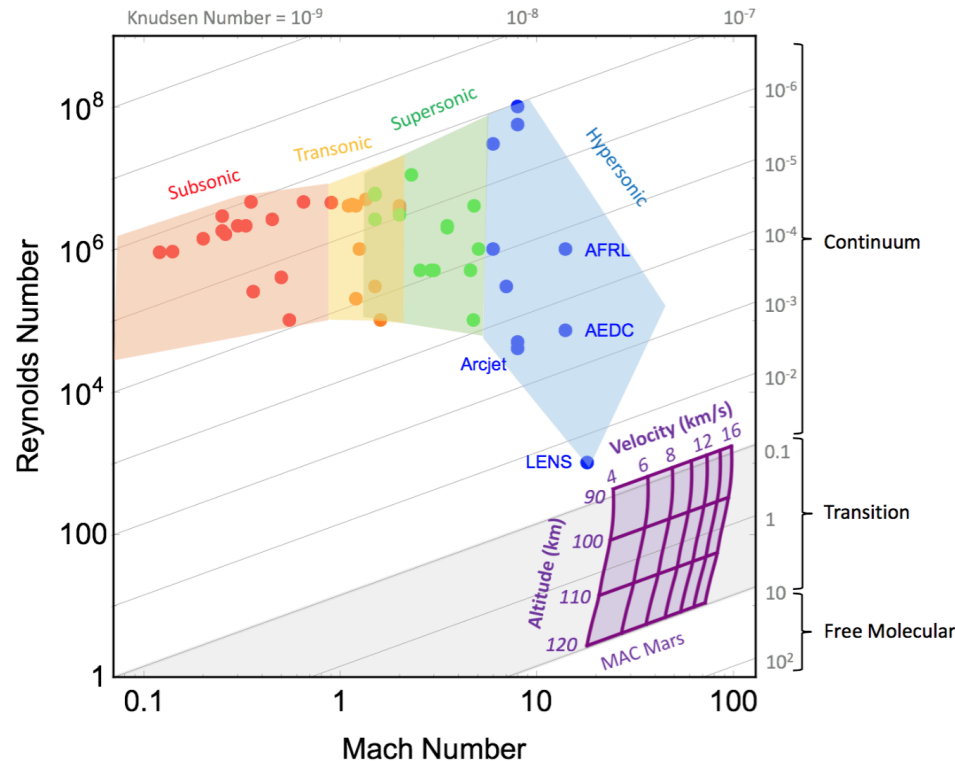


Kern et al., J. Spacecr. Rocket, 57, 1000, 2021

How do we test this concept?

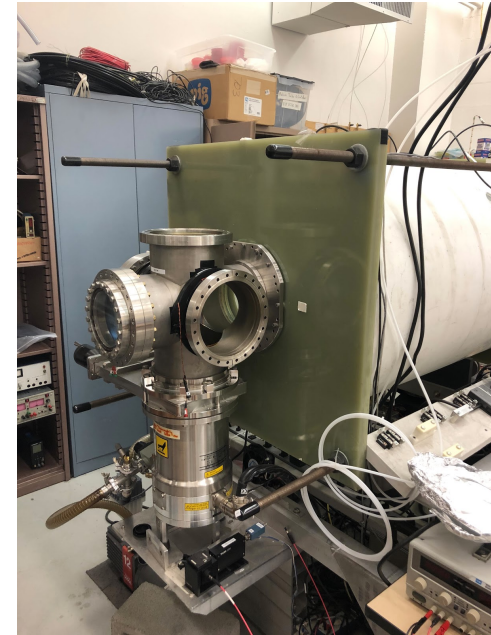
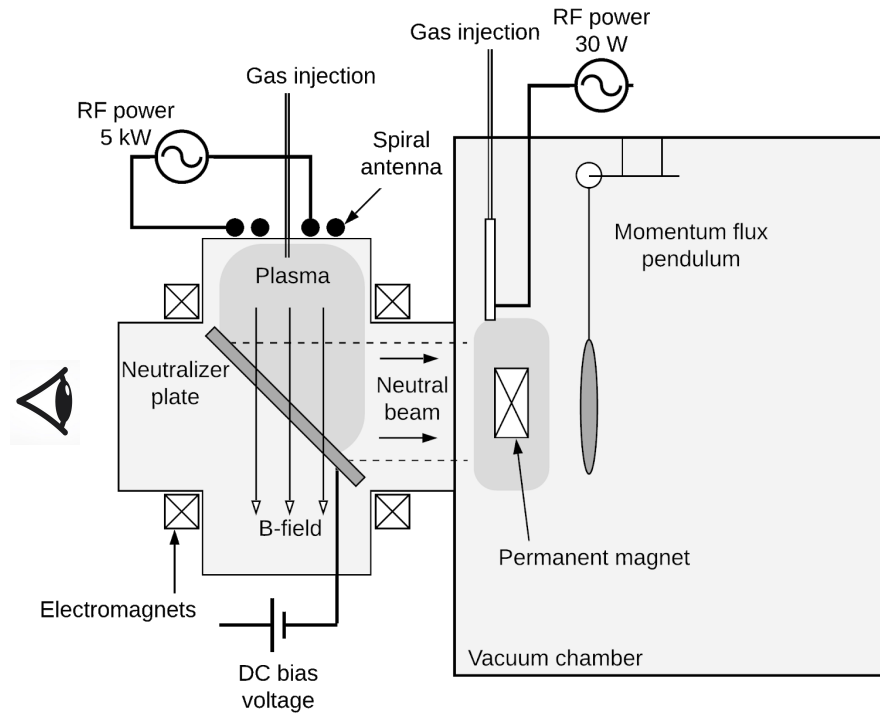
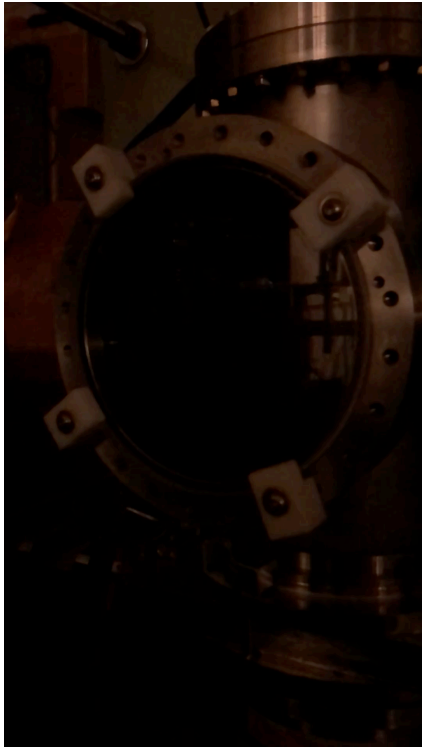


Flow Requirements of Magnetoshell Experiments

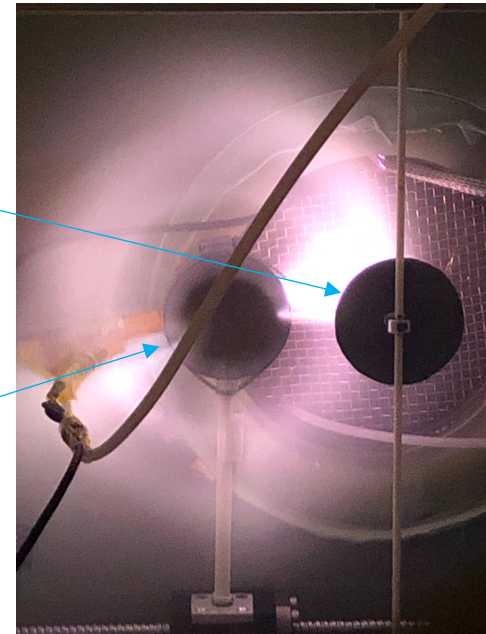
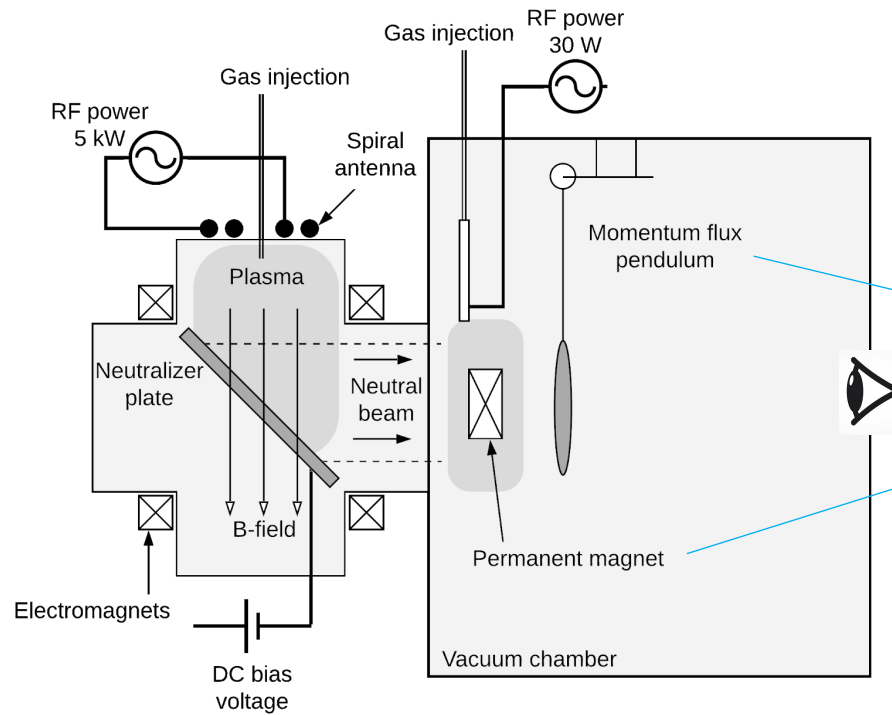


Wind tunnels unable to produce relevant flow regime!

UW Plasma Magnetoshell Aerocapture Experiment



UW Plasma Magnetoshell Aerocapture Experiment

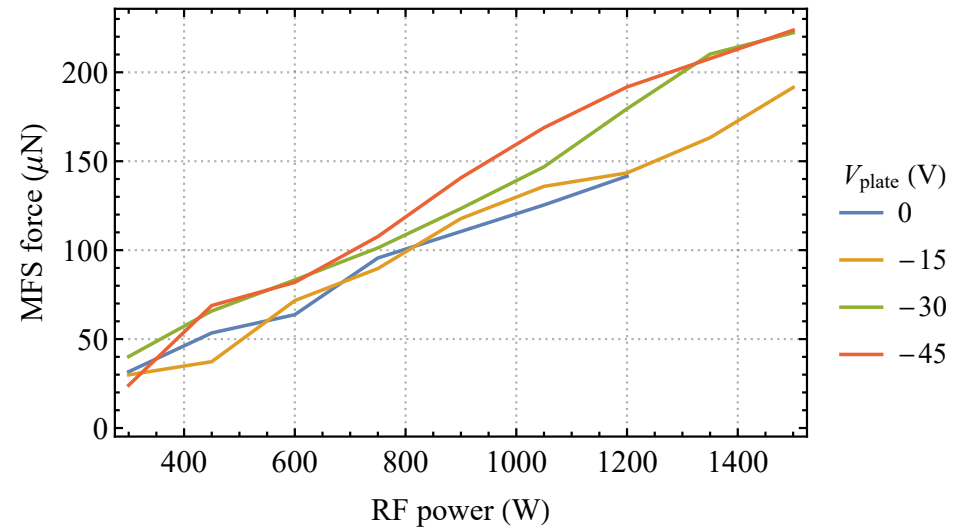
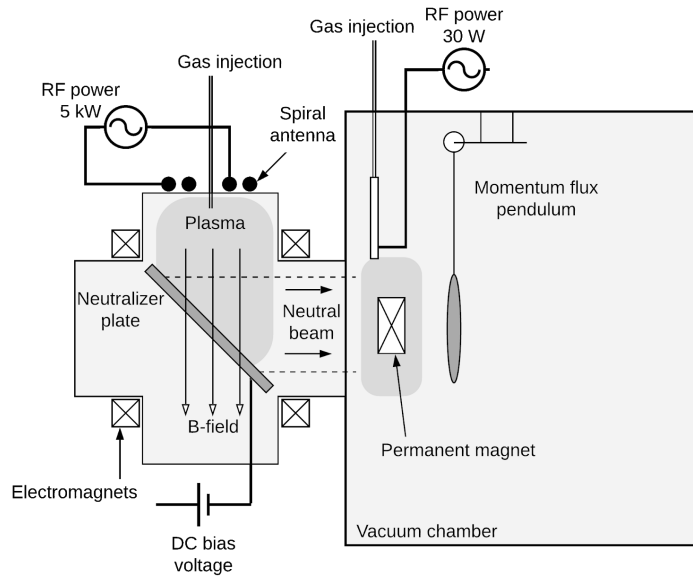


UW Plasma Magnetoshell Aerocapture Experiment

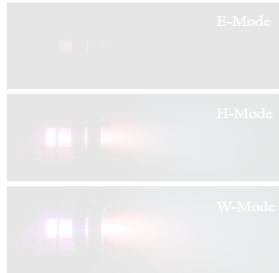
W



UW Plasma Magnetoshell Aerocapture Experiment



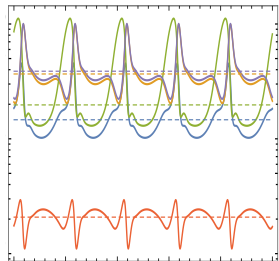
Mode Transitions in Aerospace Plasmas



Topic 1: Mode transitions in helicon thrusters



Topic 2: Critical velocities for plasma aerocapture

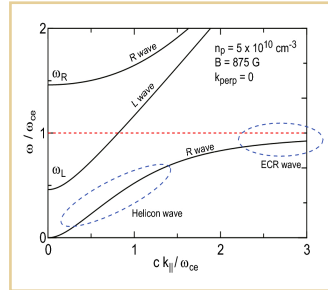


Topic 3: Data-driven discovery of mode transition physics

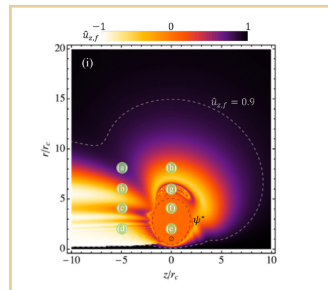
Mode Transitions in Aerospace Plasmas

MICROSCOPIC PROCESSES

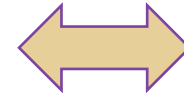
RF Absorption



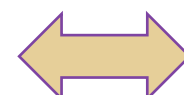
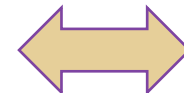
Flow Absorption



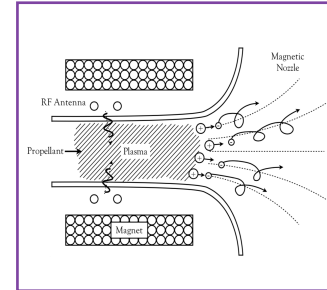
Driving Physics



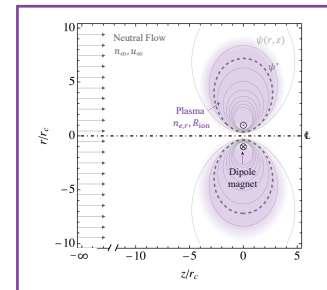
MODE
TRANSITION



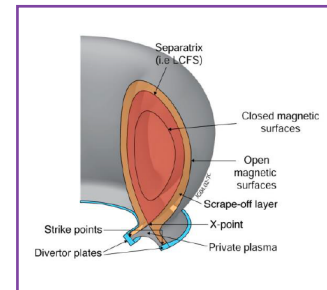
Thruster Global Model



Magnetoshell Global Model

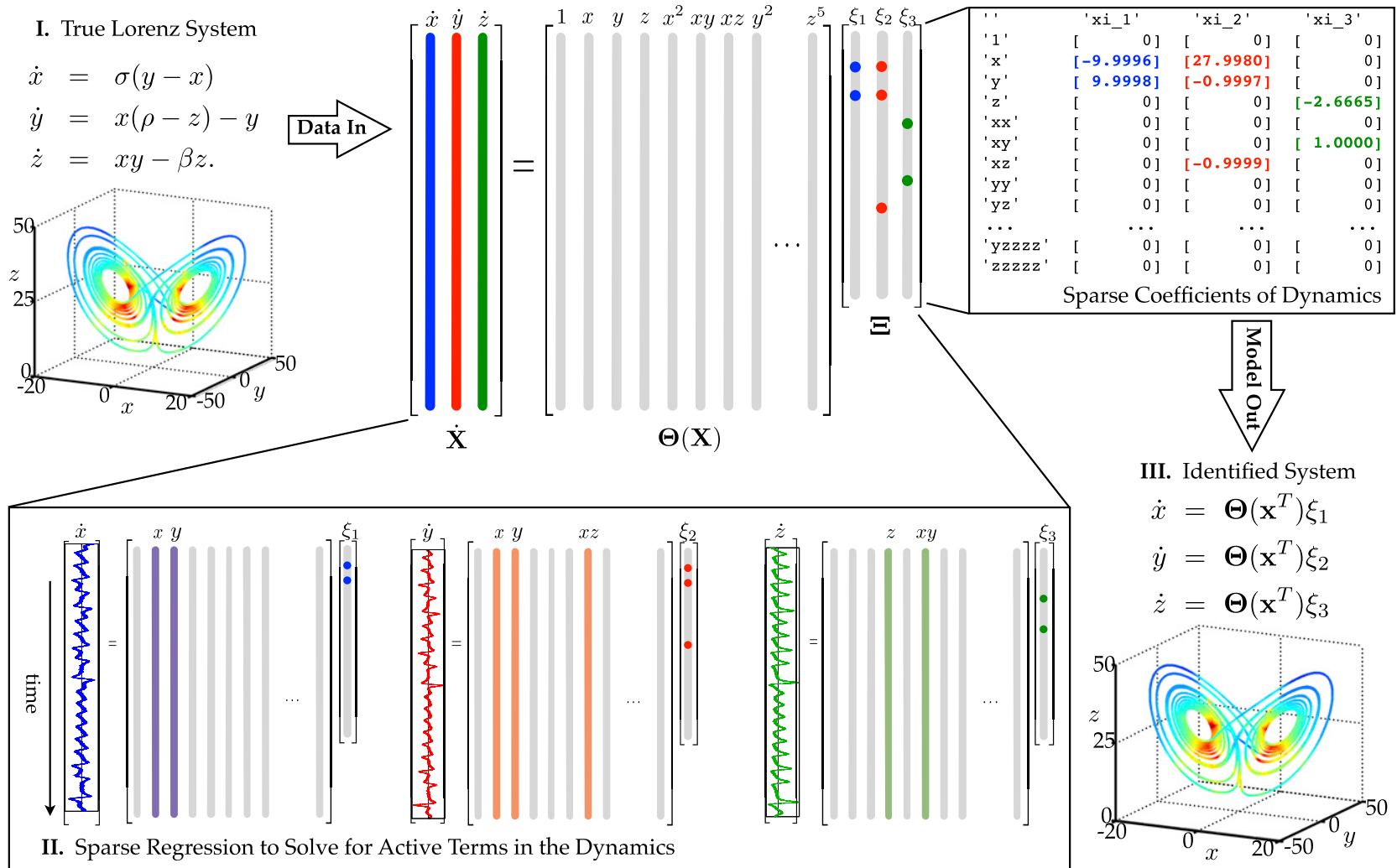


Plasma Configuration



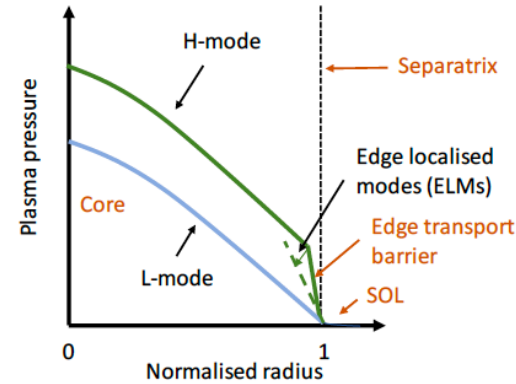
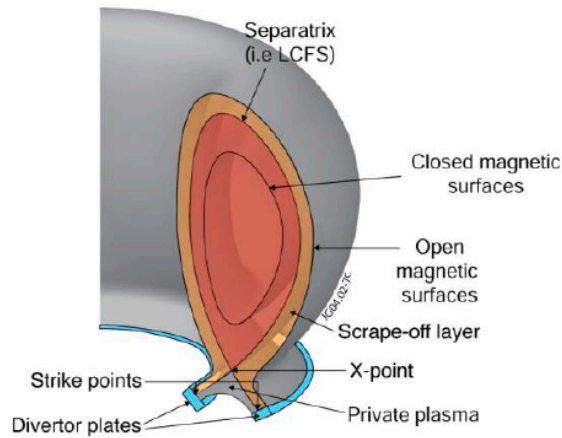
MACROSCOPIC ORGANIZATION

Sparse Identification of Nonlinear Dynamics (SINDy)

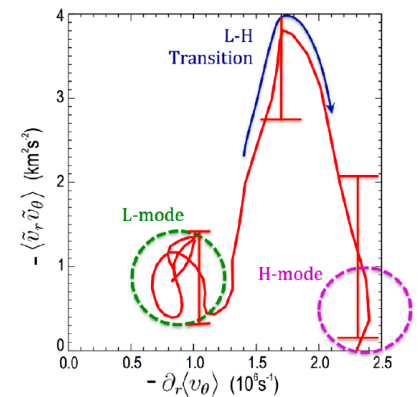
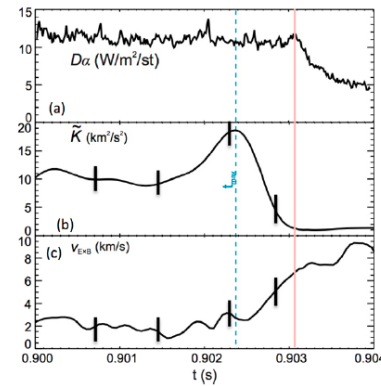
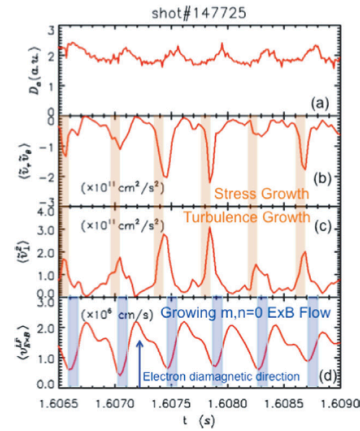
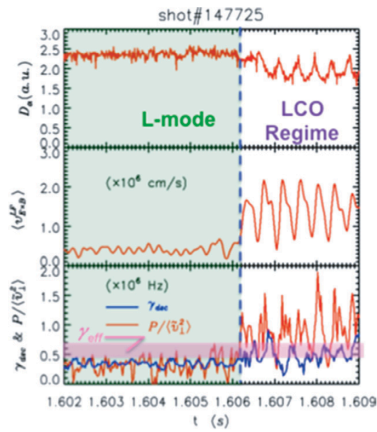


Brunton, Proctor, and Kutz. *Proceedings of the national academy of sciences* 113.15 (2016): 3932-3937.

L-H Mode Transition in Magnetically-Confinement Plasma



Ham et al. *Nature Reviews Physics* 2.3 (2020): 159-167.



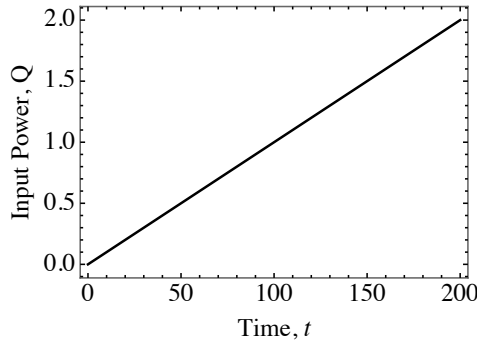
Tynan et al. *Nuclear Fusion* 53 (2013): 073053.

Tynan et al. *Plasma Phys. Controlled Fusion* 58.4 (2016): 044003.

Dynamical Model of the L-H Transition



Turbulence envelope equations in 0D provide dynamical model for L-H transition



$$Q = 0.01t$$

$$a_1 = 0.2$$

$$a_2 = a_3 = 0.7$$

$$b_1 = 1.5$$

$$b_2 = b_3 = 1.0$$

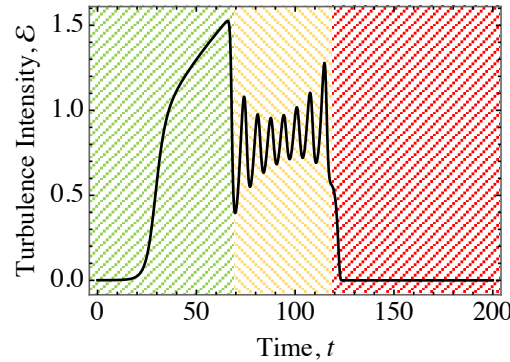
$$c_1 = 1.0$$

$$c_2 = 0.5$$

$$d = 1.0$$

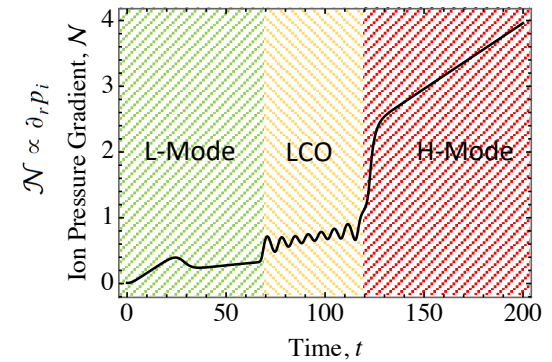
$$\partial_t \mathcal{E} = \mathcal{E} \mathcal{N} - a_1 \mathcal{E}^2 - \overbrace{a_2 V^2 \mathcal{E} + a_3 V_{ZF}^2 \mathcal{E}}^{\text{Shear suppression}}$$

Linear instability Non-linear saturation



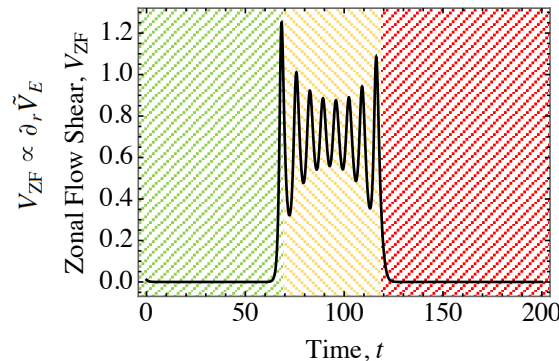
$$\partial_t \mathcal{N} = -c_1 \mathcal{E} \mathcal{N} - c_2 \mathcal{N} + Q$$

Turbulent diffusion Neoclassical transport



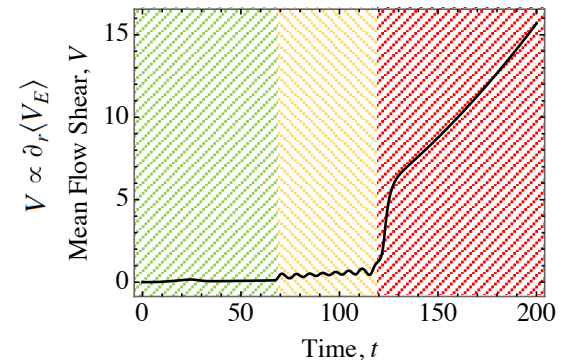
$$\partial_t V_{ZF} = b_1 \frac{\mathcal{E} V_{ZF}}{1 + b_2 V^2} - \overbrace{b_3 V_{ZF}}^{\text{Damping}}$$

Reynolds stress



$$V = d \mathcal{N}^2$$

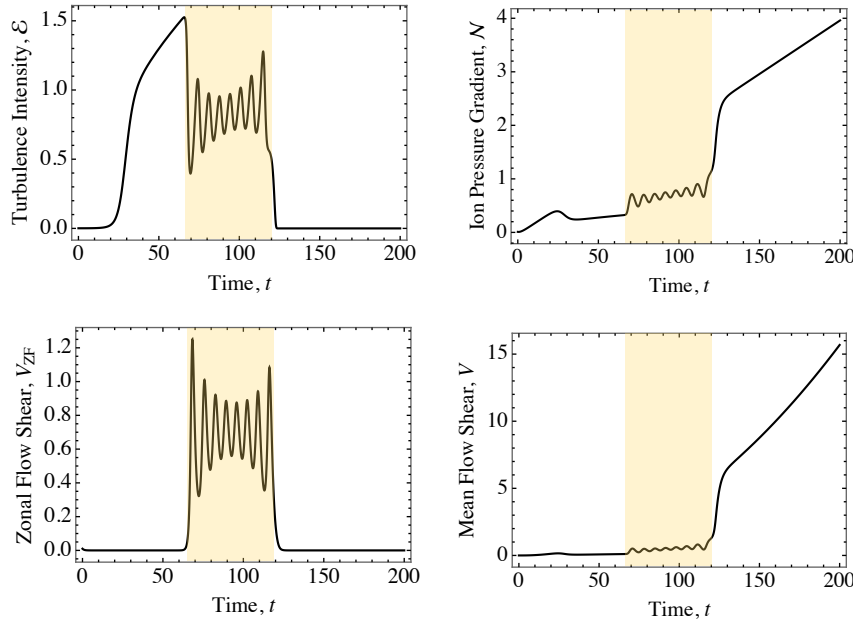
Force balance



Application of SINDy to L-H Mode Transition



Can SINDy find coefficients using LCO data?



$$Q = 0.01t$$

$$a_1 = 0.2$$

$$a_2 = a_3 = 0.7$$

$$b_1 = 1.5$$

$$b_2 = b_3 = 1.0$$

$$c_1 = 1.0$$

$$c_2 = 0.5$$

$$d = 1.0$$

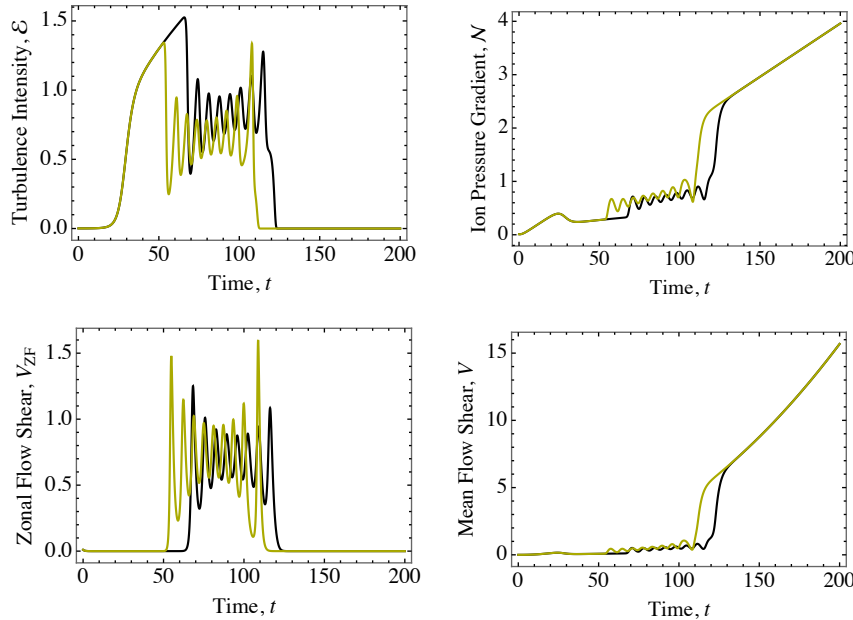
$$\partial_t \mathcal{N} = -c_1 \varepsilon \mathcal{N} - c_2 \mathcal{N} + Q$$

	$\dot{\varepsilon}$	$\dot{V}_{ZF}$	$\dot{N}$
t	0	0	0.01
ε	0	0	0
V_{ZF}	0	-0.979254	0
N	0	0	-0.5
ε^2	-0.2	0	0
εV_{ZF}	0	0	0
εN	1.	0	-1.
V_{ZF}^2	0	0	0
$V_{ZF} N$	0	0	0
N^2	0	0	0
ε^3	0	0	0
$\varepsilon^2 V_{ZF}$	0	0	0
$\varepsilon^2 N$	0	0	0
εV_{ZF}^2	-0.7	0	0
εN^2	0	0	0
εN^4	-0.7	0	0
V_{ZF}^3	0	0	0
$V_{ZF}^2 N$	0	0	0
$V_{ZF} N^2$	0	0	0
N^3	0	0	0
$\frac{\varepsilon V_{ZF}}{1+N^4}$	0	1.57443	0

Application of SINDy to L-H Mode Transition



What if we add “unknown” physics?

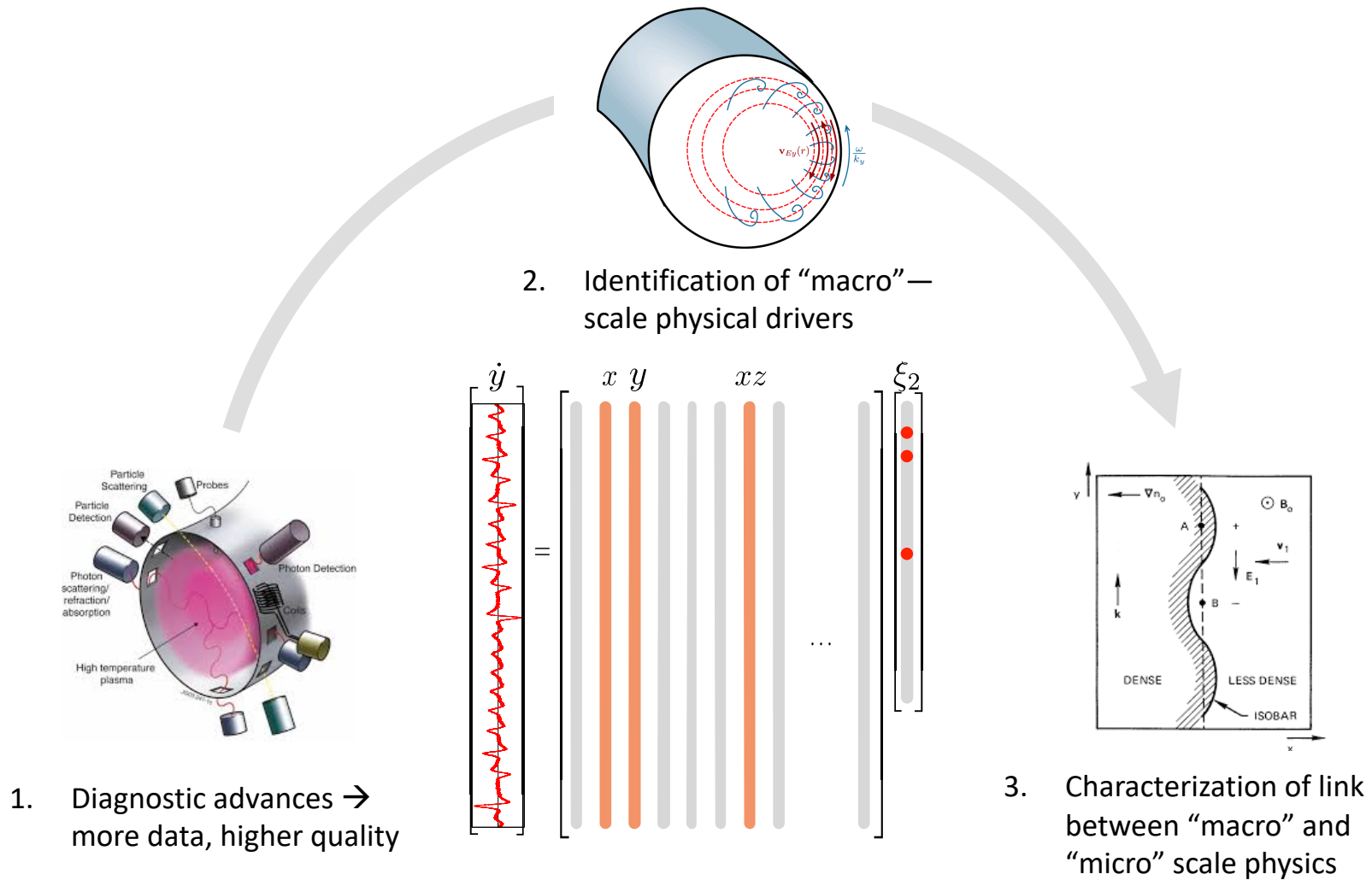


$$\partial_t V_{ZF} = b_1 \frac{\varepsilon V_{ZF}}{1 + b_2 V^2} - b_3 V_{ZF} + b_4 \varepsilon^2 V_{ZF}$$

$$b_4 = 0.5$$

	$\dot{\varepsilon}$	$\dot{V}_{ZF}$	$\dot{N}$
t	0	0	0.01
ε	0	0	0
V_{ZF}	0	-1.01465	0
N	0	0	-0.5
ε^2	-0.2	0	0
εV_{ZF}	0	0	0
εN	1.	0	-1.
V_{ZF}^2	0	0	0
$V_{ZF} N$	0	0	0
N^2	0	0	0
ε^3	0	0	0
$\varepsilon^2 V_{ZF}$	0	0.484106	0
$\varepsilon^2 N$	0	0	0
εV_{ZF}^2	-0.7	0	0
εN^2	0	0	0
εN^4	-0.7	0	0
V_{ZF}^3	0	0	0
$V_{ZF}^2 N$	0	0	0
$V_{ZF} N^2$	0	0	0
N^3	0	0	0
$\frac{\varepsilon V_{ZF}}{1+N^4}$	0	1.6598	0

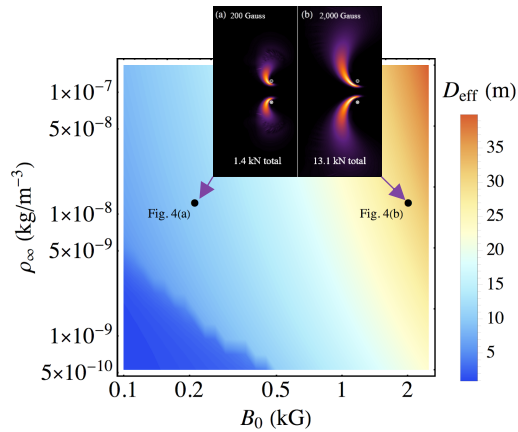
Application of SINDy to Mode Transitions



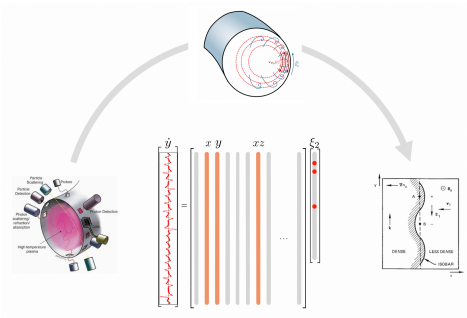
Conclusions



- Plasmas exhibit bizarre, oftentimes unexpected behavior



- Understanding “non-ideal” physics critical for space technology



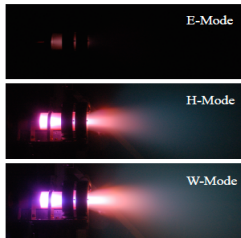
- Exciting new methods on the horizon enabled by “big data”

Acknowledgements



Julia Falkovitch-Khain

Prof. Mark Kushner



Prof. Edgar Choueiri (Princeton University)

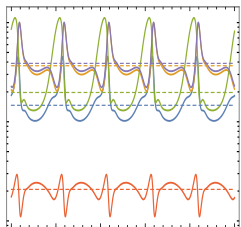
Funding: National Defense Science and Engineering graduate Fellowship (AFOSR)



Charlie Kelly (PhD Student, University of Washington)

Dr. David Kirtley & Dr. Anthony Pancotti (Helion Energy), Dr. Bob Moses (NASA)

Funding: NASA Space Technology Research Fellowship (Kelly)



Dr. Justin Koo, Dr. Daniel Eckhardt, Dr. Robert Martin (AFRL)

Funding: AFOSR Young Investigator Program (FA9550-21-1-0167)

QUESTIONS?