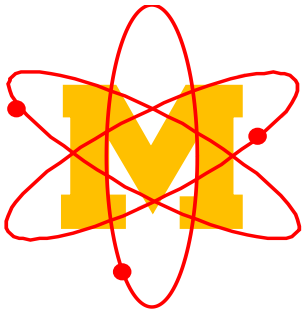




Spreading Resistance of Thin Film Contacts

Peng Zhang, Y. Y. Lau, and R. M. Gilgenbach

Department of Nuclear Engineering and Radiological Sciences
University of Michigan
Ann Arbor, MI, USA, 48109-2104

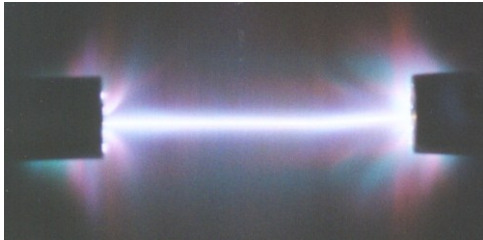
Michigan Institute for Plasma Science and Engineering
3rd Annual Graduate Student Symposium
Michigan State University, East Lansing, MI
October 3, 2012

Work supported by an AFOSR grant FA9550-09-1-0662, L-3, Northrop-Grumman.

Introduction

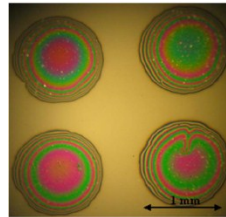
- Electrical contact is important to

Wire-array Z pinches



Z-pinch @ UM & Sandia

Metal-insulator-vacuum junctions



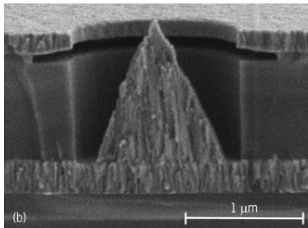
Metal-oxide-junction cathodes
[Jordan *et al.* Rev. Sci. Instrum. 79, 064705 (2008)]

High power microwave (HPM) sources



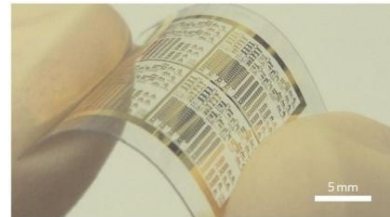
UM/ L-3-Titan relativistic magnetron

Field emitters



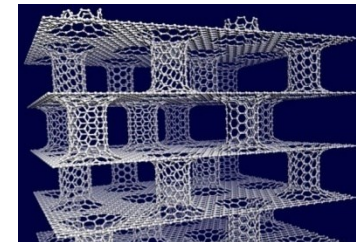
<http://accessscience.com>

Thin film devices & integrated circuits



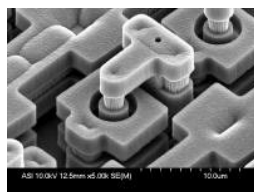
Sun et al,
Nature Nanotechnol.
6, 156 (2011)

Carbon nanotubes based cathodes and interconnects



CREDIT: SPIE

Micro-electromechanical System (MEMS)



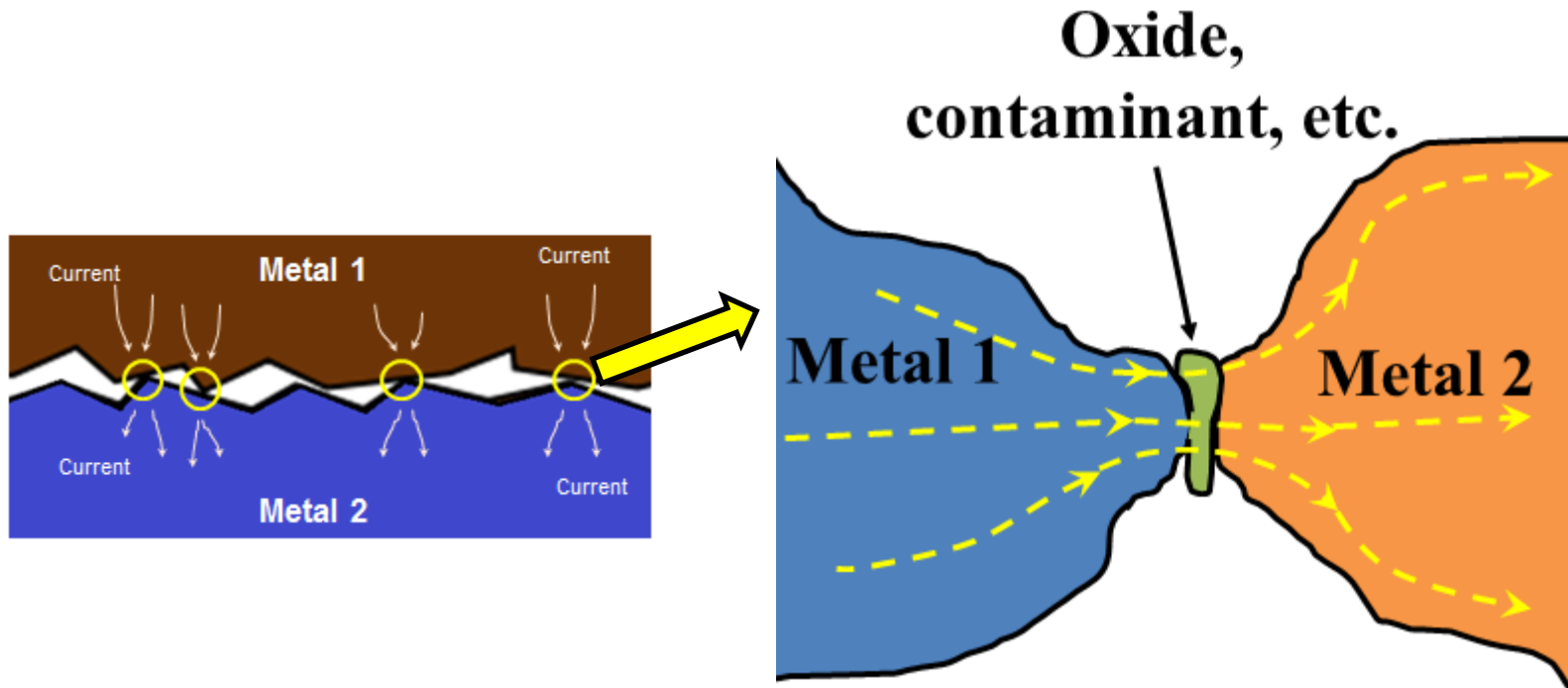
<http://www.memx.com/products.htm>

Tribology



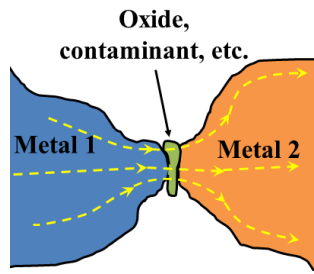
<http://machinedesign.com>

Bulk Contact Model



- Contact resistance is highly random, affected by surface roughness, pressure, hardness, **residing oxides and contaminants**, etc.





Holm's *a*-spot model (1967)

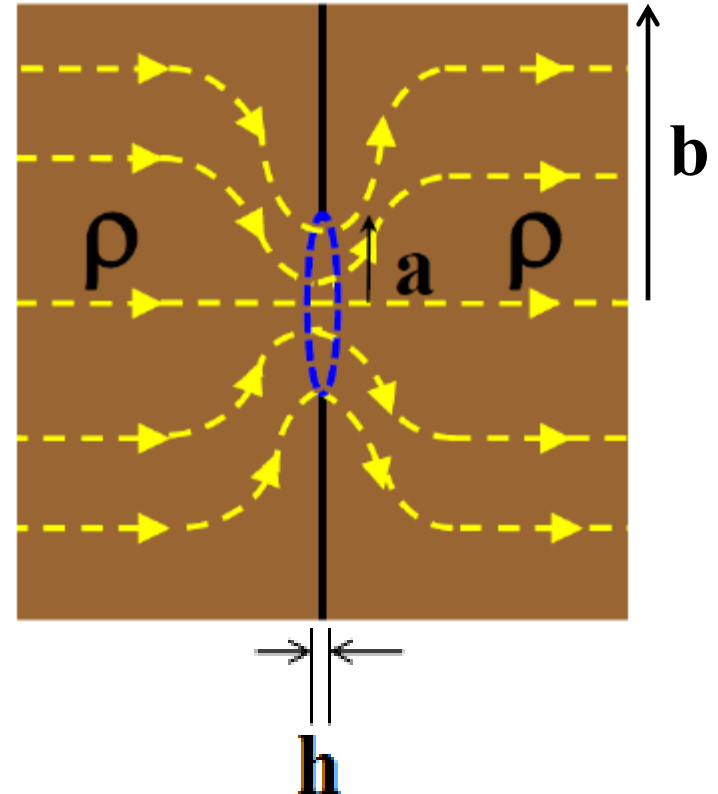
Contact Resistance

$$R_c = \frac{\rho}{2a}$$

$$h = 0$$

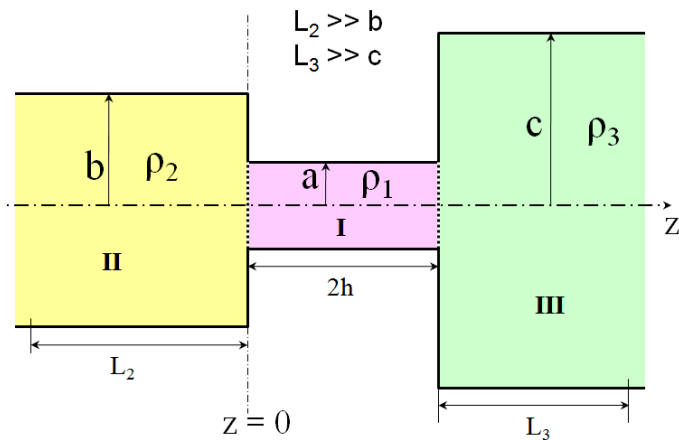
$$b \rightarrow \infty$$

Same material

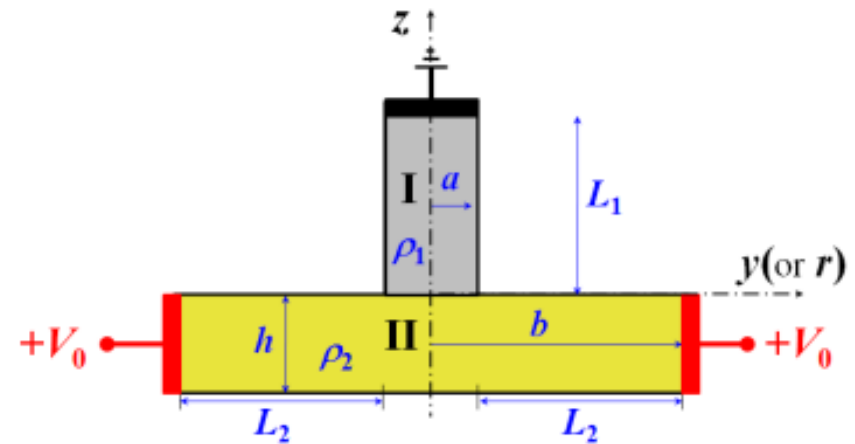


*Holm, *Electric Contacts: Theory and Application*, Springer-Verlag, NY (1967).

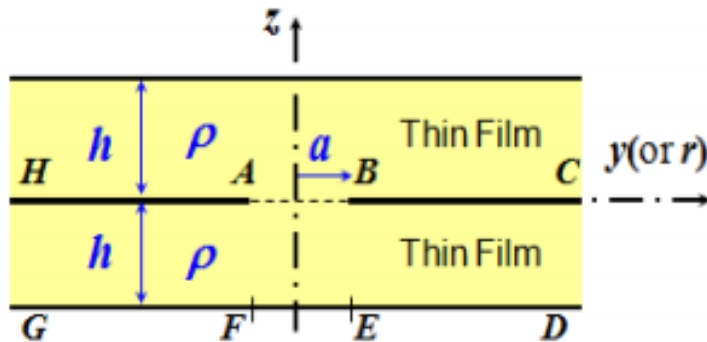
Bulk Contact [1]



Thin-film Contact [2]

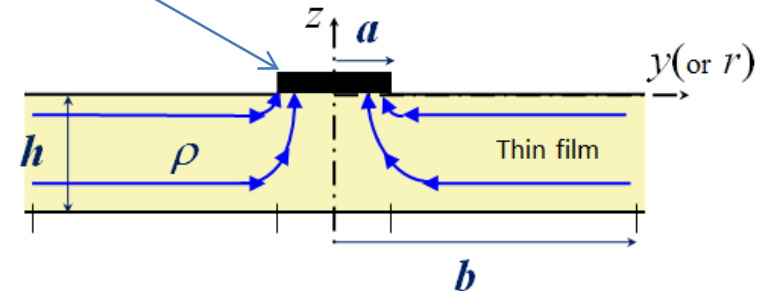


Thin-film Contact – MEMS [3]



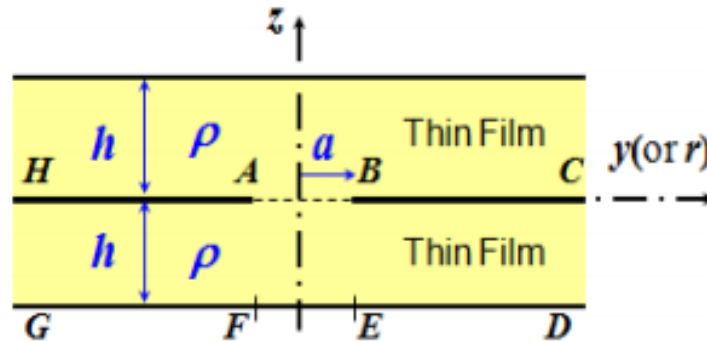
Metal-Metal Contact [3]

Contact resistivity $r_c=0$



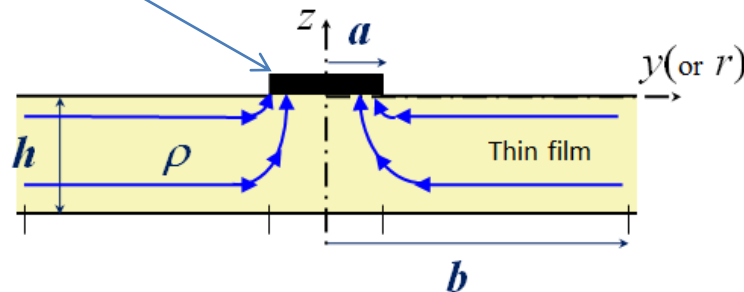
- [1] P. Zhang and Y. Y. Lau, J. Appl. Phys. **108**, 044914 (2010).
- [2] P. Zhang, Y. Y. Lau, R. M. Gilgenbach, Appl. Phys. Lett. **97**, 204103 (2010);
J. Appl. Phys. **109**, 124910 (2011).
- [3] P. Zhang, Y. Y. Lau, and R. S. Timsit, IEEE Trans. Electron Devices, **59**, 1936 (2012).

Thin-film Contact – MEMS



Same as Metal-Metal Contact, by Symmetry

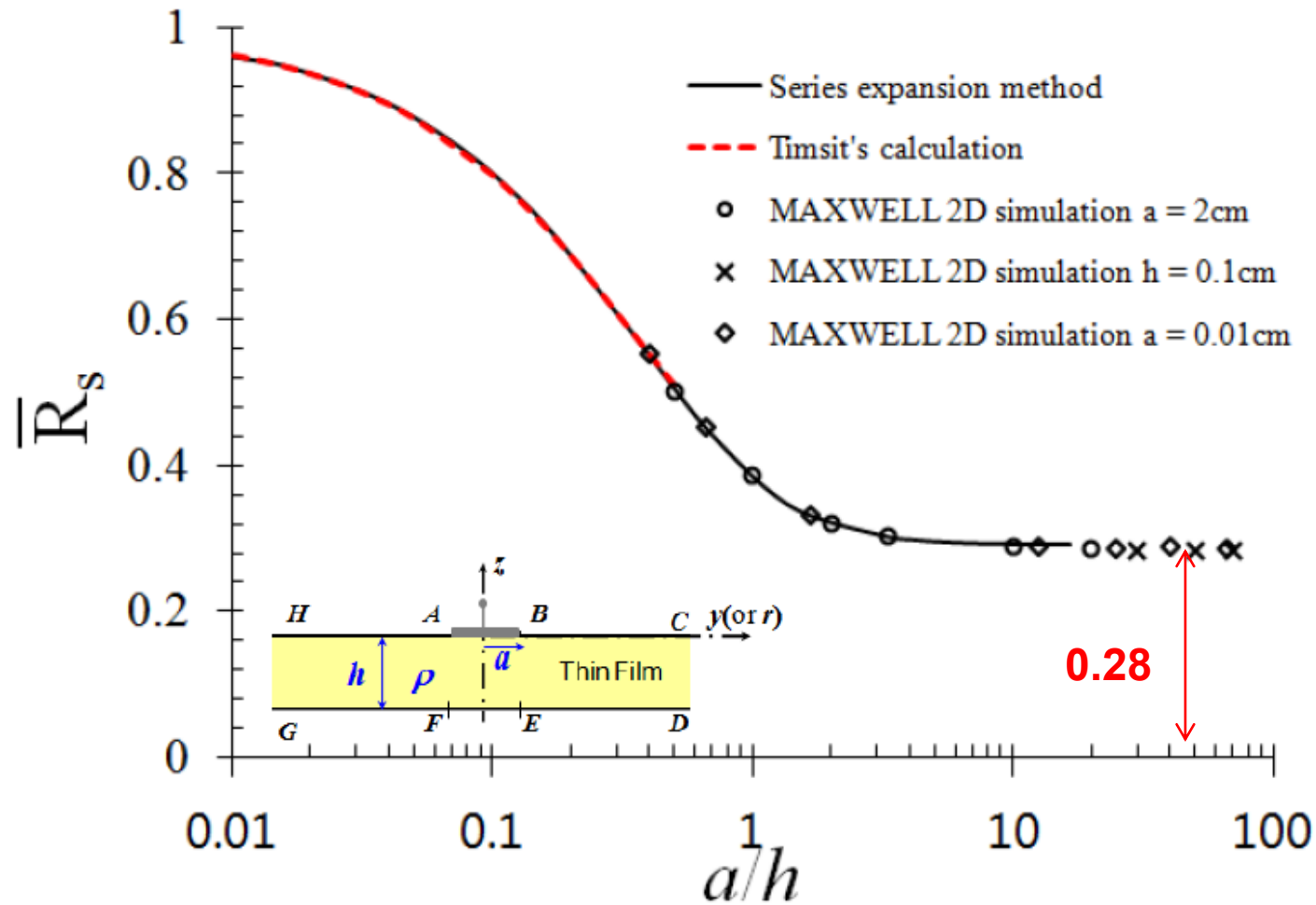
Contact resistivity $r_c=0$



Peng Zhang, Y. Y. Lau, and R. S. Timsit, "On the spreading resistance of thin-film contacts", IEEE Trans. Electron Devices **59**, 1936 (2012).



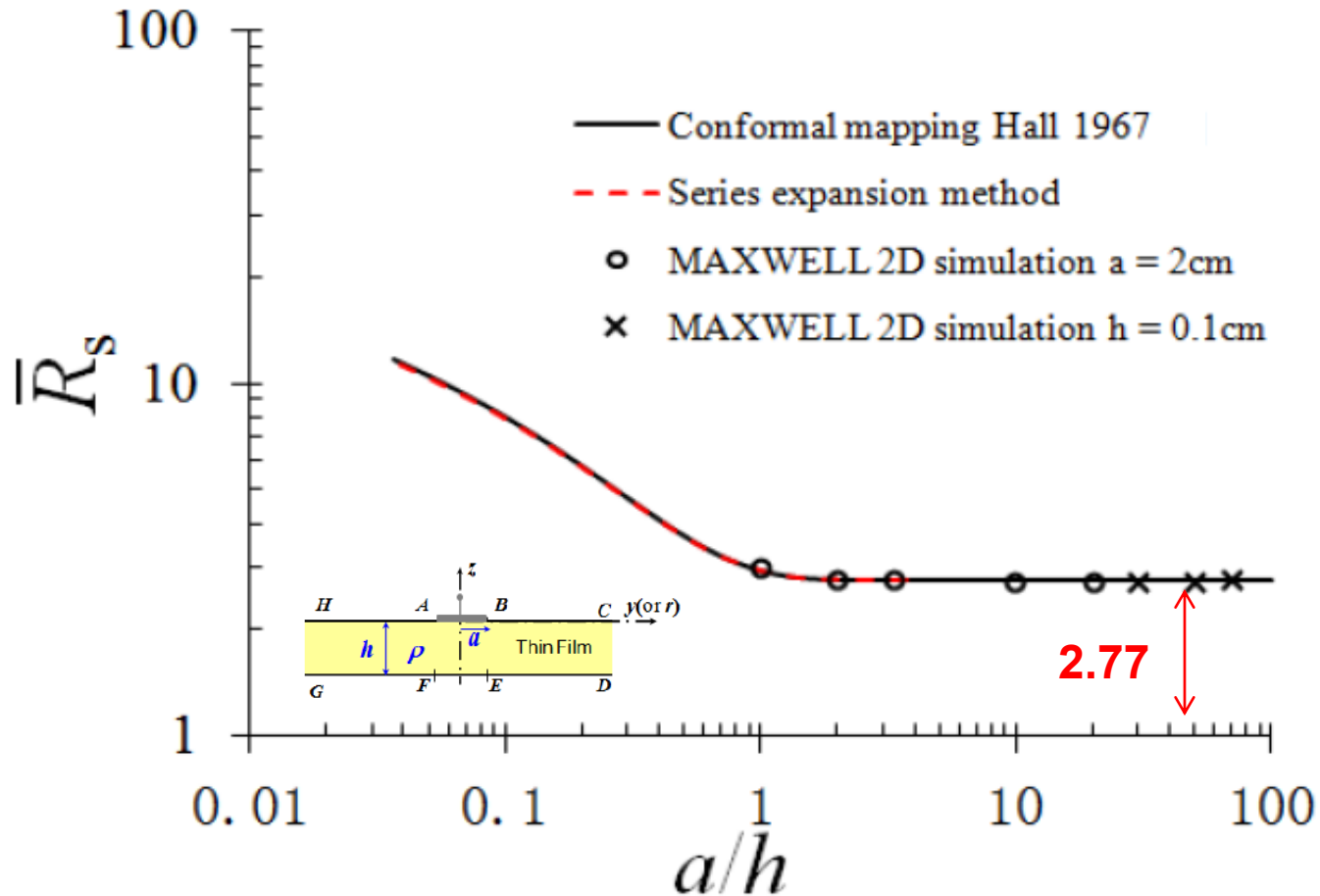
Cylindrical Thin Film Contact (Spreading) Resistance, R_s



$$R_s = R_{Total} - R_{bulk} \equiv \frac{\rho}{4a} \bar{R}_s$$



Cartesian Thin Film Contact (Spreading) Resistance, R_s

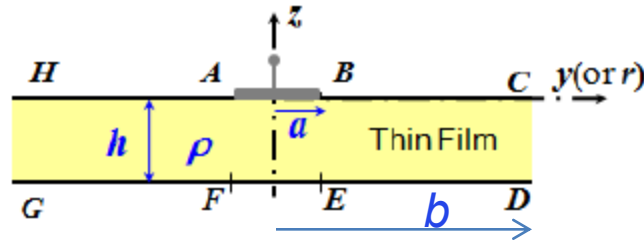


$$R_s = R_{Total} - R_{bulk} \equiv \frac{\rho}{4\pi W} \bar{R}_s$$



Current Crowding and Enhanced Heating

As $h \rightarrow 0$,



$$R_{\text{Total}} = R_S + R_{\text{bulk}} = 2.77 \times (\rho / 4\pi W) + \rho(b - a) / 2Wh$$

Cartesian

$$\equiv \rho(b - a') / 2Wh$$

$$\Rightarrow a' = a \left(1 - \frac{2 \ln 2}{\pi} h / a \right) \cong a - 0.44h$$

$$R_{\text{Total}} = R_S + R_{\text{bulk}} = 0.28 \times (\rho / 4a) + (\rho / 2\pi h) \ln(b / a)$$

Cylindrical

$$\equiv (\rho / 2\pi h) \ln(b / a')$$

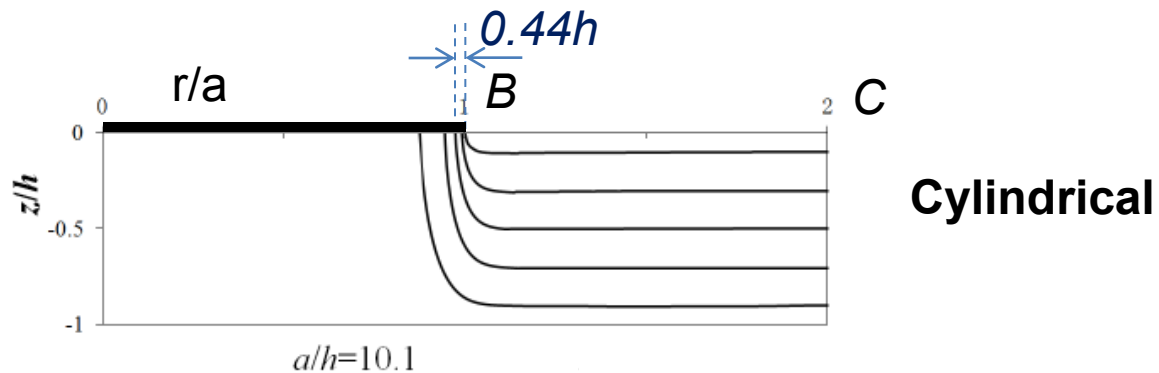
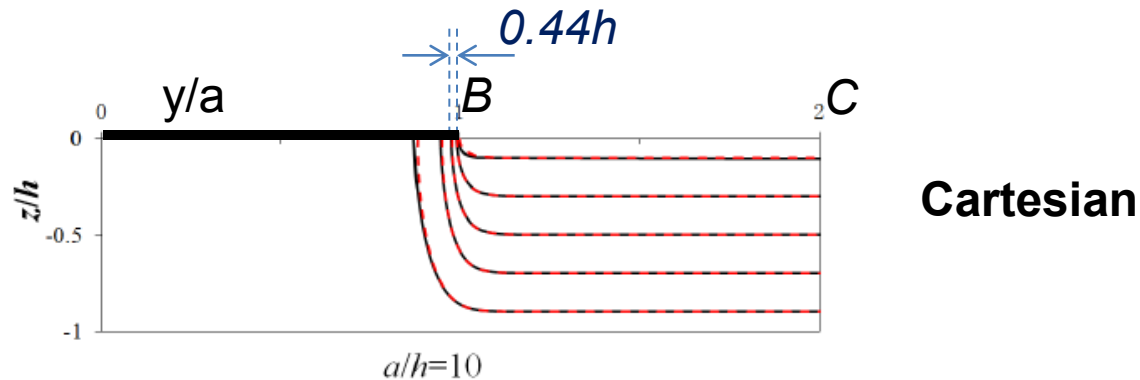
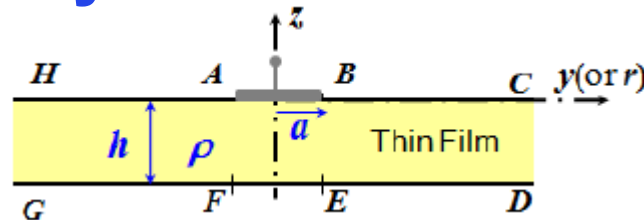
$$\Rightarrow a' = ae^{-0.28 \times \frac{\pi h}{2a}} = ae^{-0.44h/a} \cong a - 0.44h$$

In general, current-crowding region $\sim 0.44 h$



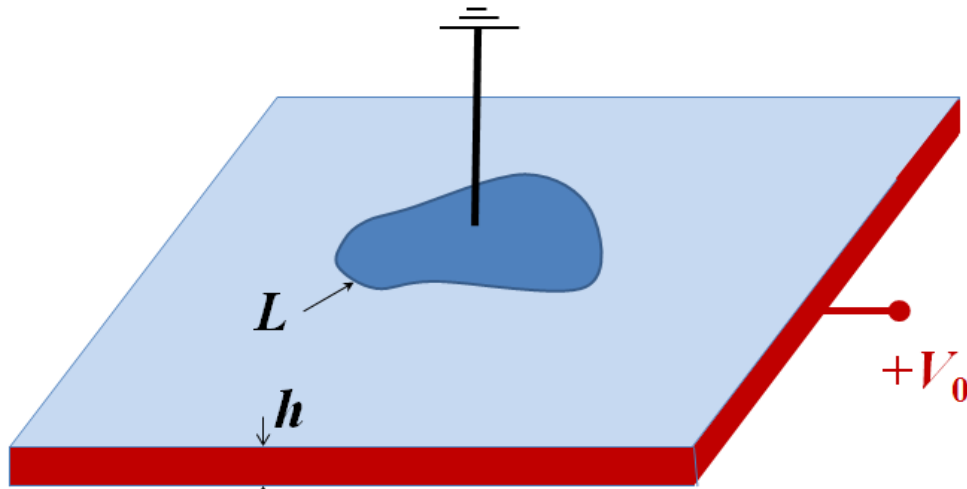
Identical Field Line Patterns for Both Cartesian and Cylindrical Thin Film Contacts

As $h \rightarrow 0$,



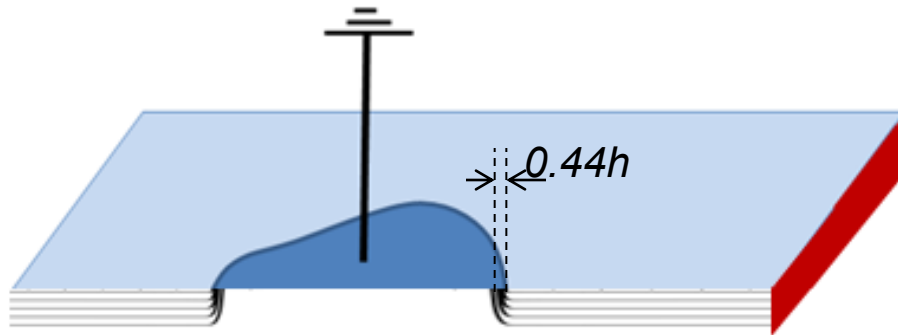
Note: Enhanced heating at Edge “B” (& “A”).

Contact Resistance in an Electrode of Arbitrary Shape*



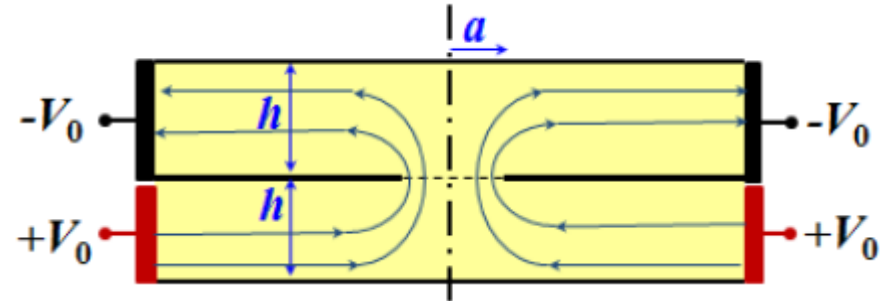
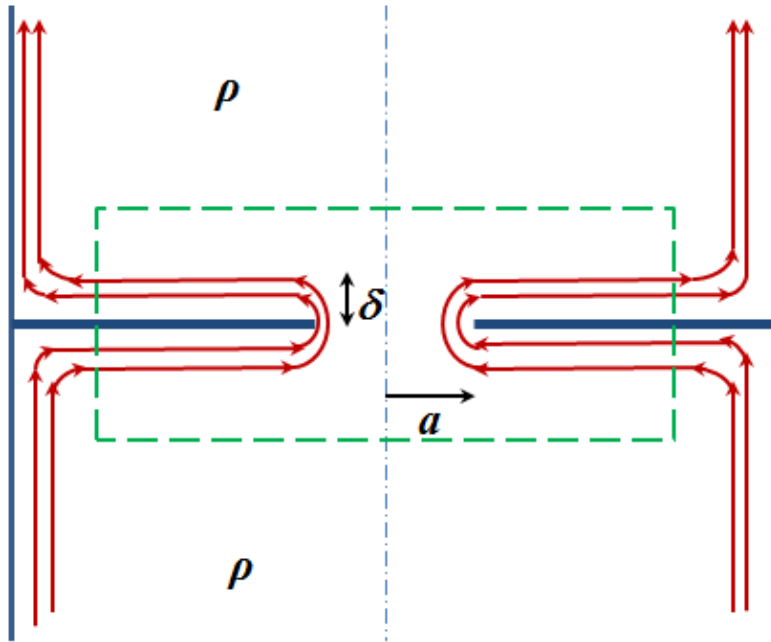
$$R_s = \left(\frac{\rho}{L} \right) \frac{2\ell}{\pi}, \quad \dots \rightarrow 0$$

L : circumference of electrode



Note: Intense local heating on electrode rim because of crowding of field lines there.

Relation of high frequency AC bulk contact and DC thin-film contact



AC Case (Bulk Contact)

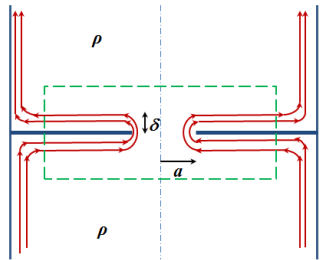
Lavers and Timsit, *IEEE Trans. Compon. Packag. Technol.*, **25**, 446–452, 2002.

DC Case (Thin Film)

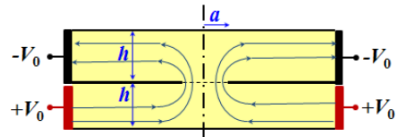
P. Zhang, Y. Y. Lau, and R. S. Timsit, *IEEE Trans. Electron Devices* **59**, 1936 (2012).

Rule: Identify skin depth (δ) with thin-film thickness (h).

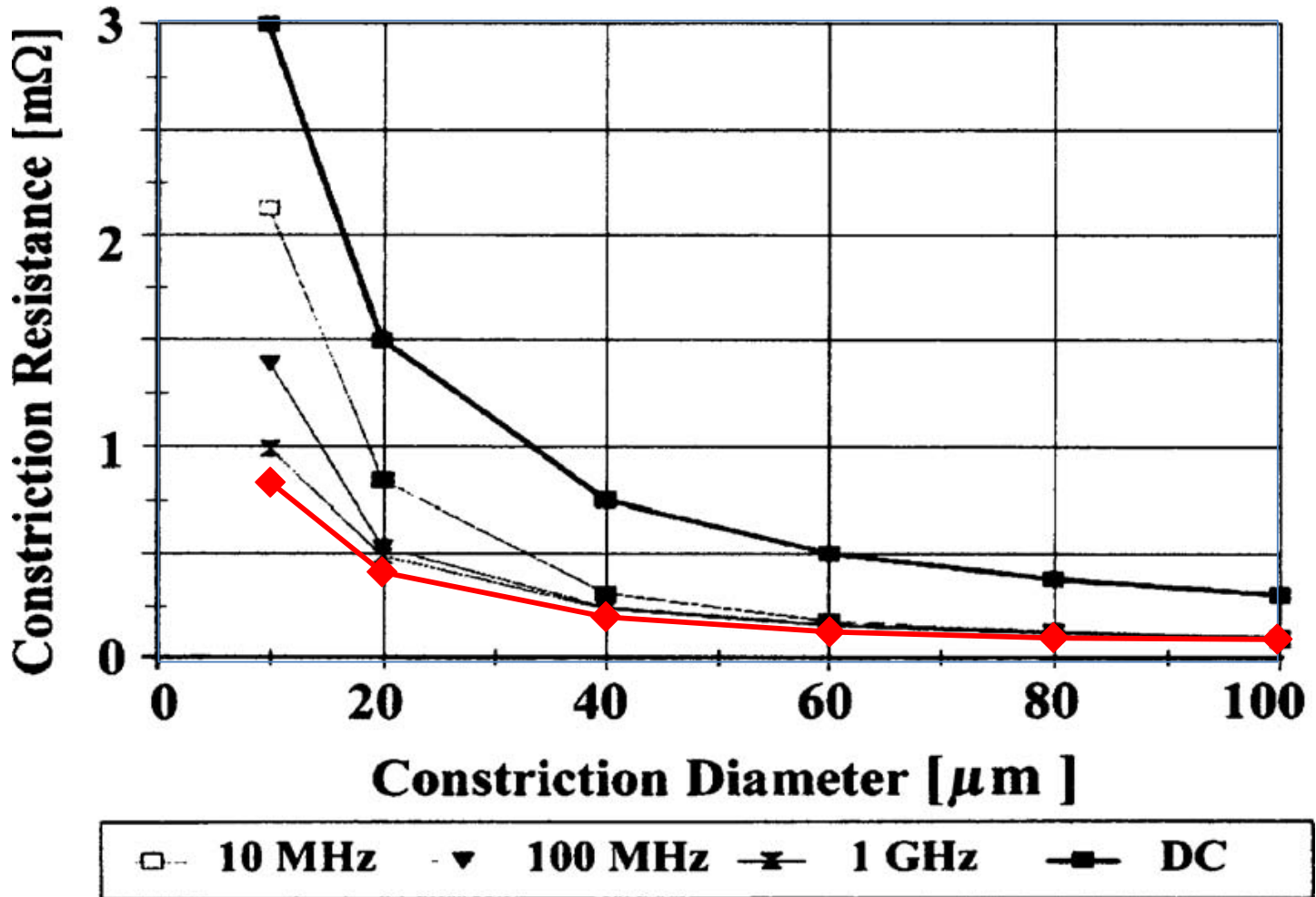
AC bulk constriction resistance for frequencies ranging from dc to 1 GHz*



AC case



Our DC model

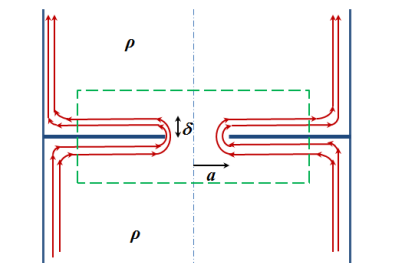


◆ Our DC Thin Film Model ($h \rightarrow 0$)

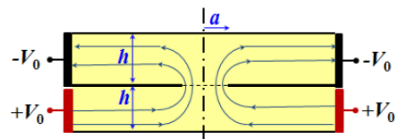
*Lavers and Timsit, *IEEE Trans. Compon. Packag. Technol.*, 25, 446–452, 2002.

*Peng Zhang, Y. Y. Lau, and R. S. Timsit, *IEEE Trans. Electron Devices* **59**, 1936 (2012).

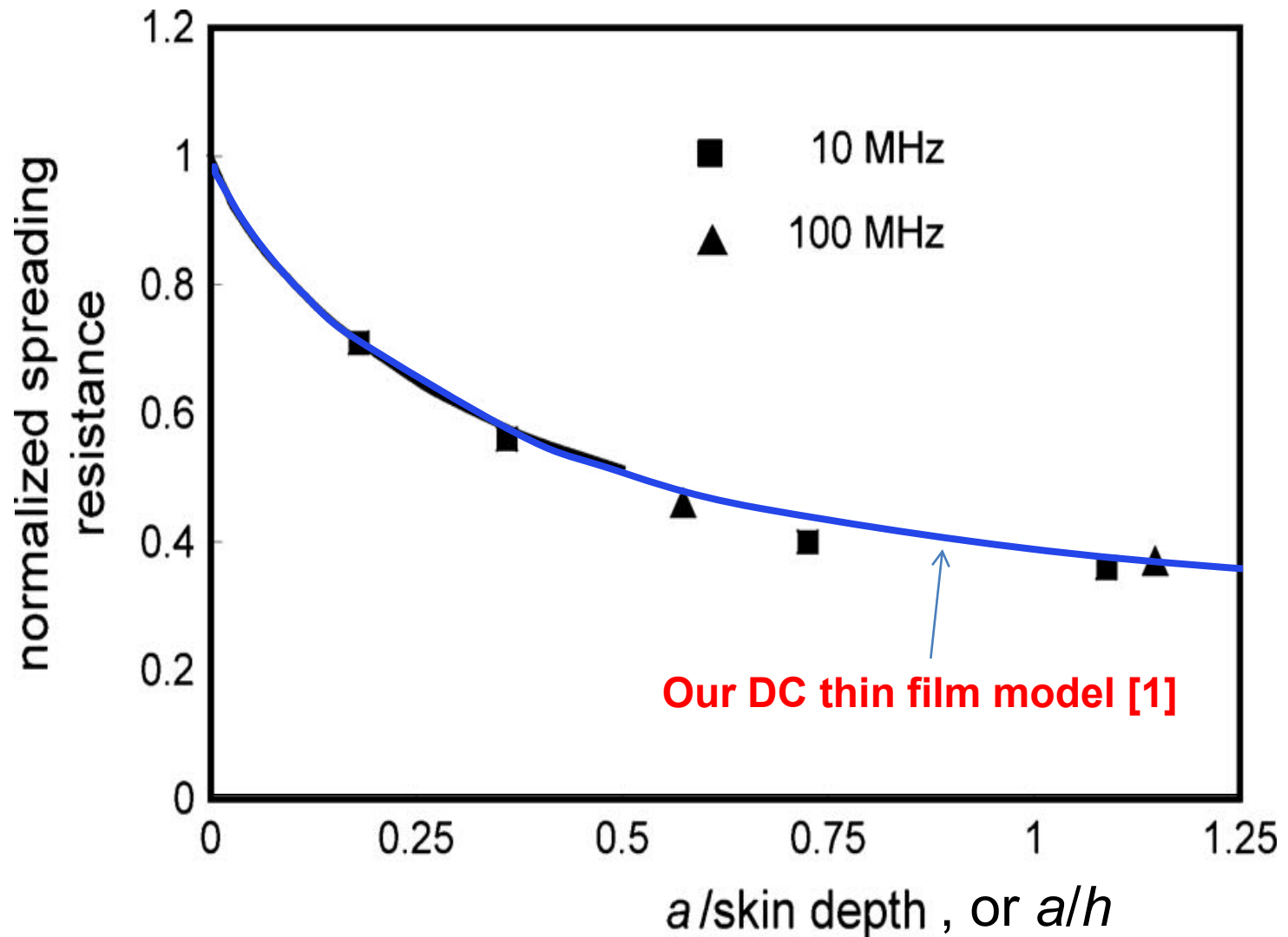
AC bulk constriction resistance for frequencies ranging from dc to 1 GHz*



AC case



Our DC model



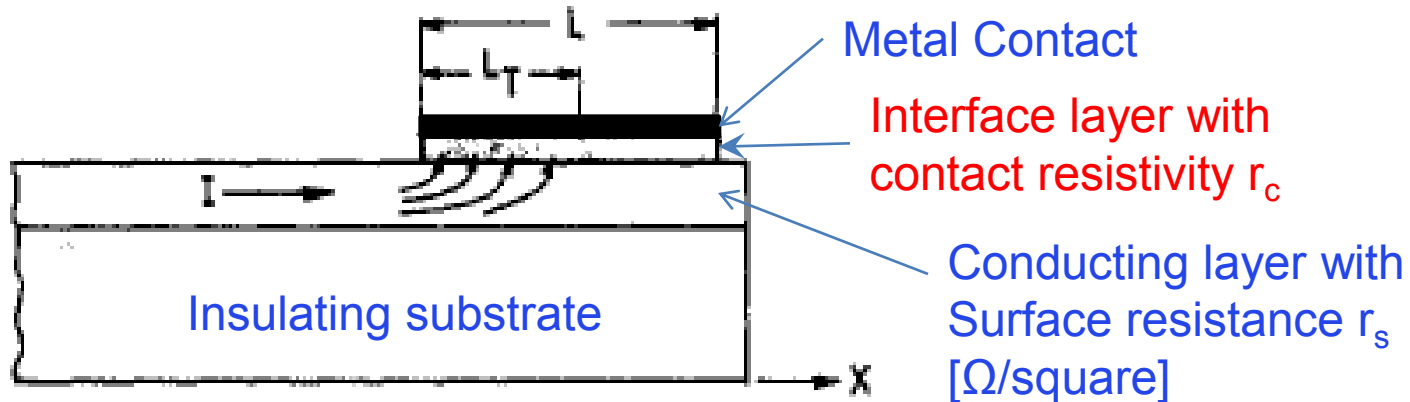
*Lavers and Timsit, *IEEE Trans. Compon. Packag. Technol.*, 25, 446–452, 2002.

[1]Peng Zhang, Y. Y. Lau, and R. S. Timsit, *IEEE Trans. Electron Devices* **59**, 1936 (2012).

Metal-Metal vs Metal-Semiconductor Contacts

Transfer Length, L_T : The length scale over which most of the current from a contact into a semiconductor layer flows

Metal-Semiconductor Contact*



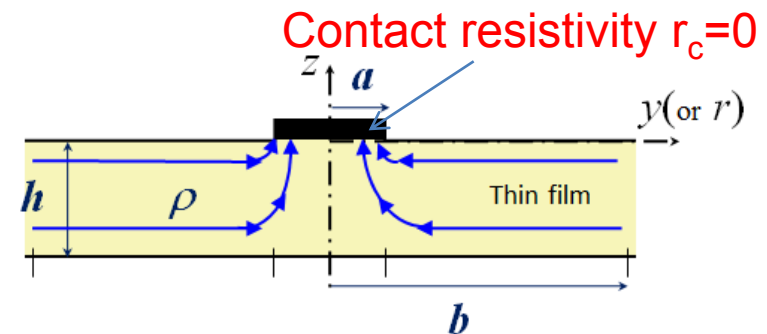
Transmission Line Model*



$$L_T = (r_c/r_s)^{1/2},$$

due ONLY to the semiconductor resistive loss

Metal-Metal Contact model



$L_T \sim 0.44h$, due ONLY to fringe fields



Conclusion

- Made vast generalization in theory of electrical contact, for both bulk and thin-film contacts (applicable to HPM, field emitters, thin-film devices, MEMS, interconnects, etc).
- Thin film contact model is extended to an α -spot of arbitrary geometry.
- The DC thin film contact model turns out to be applicable to the bulk contact resistance, from DC to high frequency (!)
- Transfer length is estimated and compared with Transmission Line Model.



Future Works

- Evaluate ohmic heating at thin-film and bulk contacts based on the newly calculated current flow profile, electro-thermal instability, migration of atoms
- Study RF heating of contacts, with the capacitive and inductive effects of the asperities
- General theory of metal-metal and metal-semiconductor contacts