



NSTX

LTX

Supported by



U.S. DEPARTMENT OF
ENERGY

Office of
Science

Up Against the Wall: Liquid Lithium for the Chamber Technology Challenge in Fusion Energy

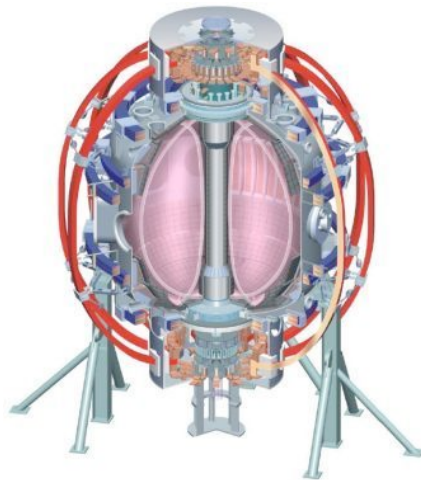
R. Kaita

Princeton Plasma Physics Laboratory

**Michigan Institute for Plasma Science and
Engineering Seminar**

April 28, 2009

College W&M
Colorado Sch Mines
Columbia U
CompX
General Atomics
INEL
Johns Hopkins U
LANL
LLNL
Lodestar
MIT
Nova Photonics
New York U
Old Dominion U
ORNL
PPPL
PSI
Princeton U
Purdue U
SNL
Think Tank, Inc.
UC Davis
UC Irvine
UCLA
UCSD
U Colorado
U Illinois
U Maryland
U Rochester
U Washington
U Wisconsin



Culham Sci Ctr
U St. Andrews
York U
Chubu U
Fukui U
Hiroshima U
Hyogo U
Kyoto U
Kyushu U
Kyushu Tokai U
NIFS
Niigata U
U Tokyo
JAEA
Hebrew U
Ioffe Inst
RRC Kurchatov Inst
TRINITI
KBSI
KAIST
POSTECH
ASIPP
ENEA, Frascati
CEA, Cadarache
IPP, Jülich
IPP, Garching
ASCR, Czech Rep
U Quebec

Outline

- **“First Wall” Problem and Liquid Metal Solution**
- **Spherical Torus Magnetic Confinement Concept**
- **Liquid Lithium Handling for “Free Surface” Studies**
- **High Heat Load Experiments with Electron Beams**
- **Plasma Fueling with Supersonic Gas Injection**
- **Lithium Coatings on Plasma Facing Components**
- **Future Plans and Challenges**

Liquid Metals Provide Possible Solution for “First Wall” Problem in Fusion Reactors

- **Liquid metals can simultaneously provide:**
 - **Elimination of erosion concerns**
 - **Wall is continuously renewed**
 - **Absence of neutron damage**
 - **Substantial reduction in activated waste**
 - **Compatibility with high heat loads**
 - **Potential for handling power densities exceeding 25 MW/m²**

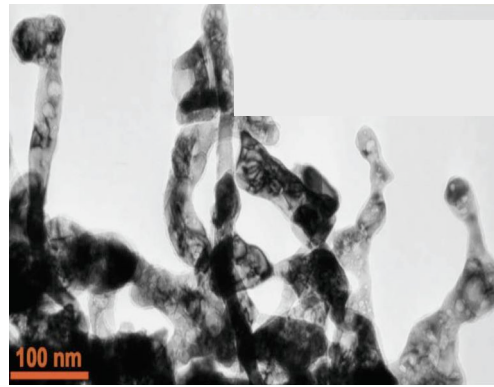
Present Solid Materials Problematic

- Tungsten is only candidate for fusion reactors
 - Tests involving long-term exposure to plasma reveals surface damage

Example: NAGDIS-II: pure He plasma

N. Ohno et al., in IAEA-TM, Vienna, 2006

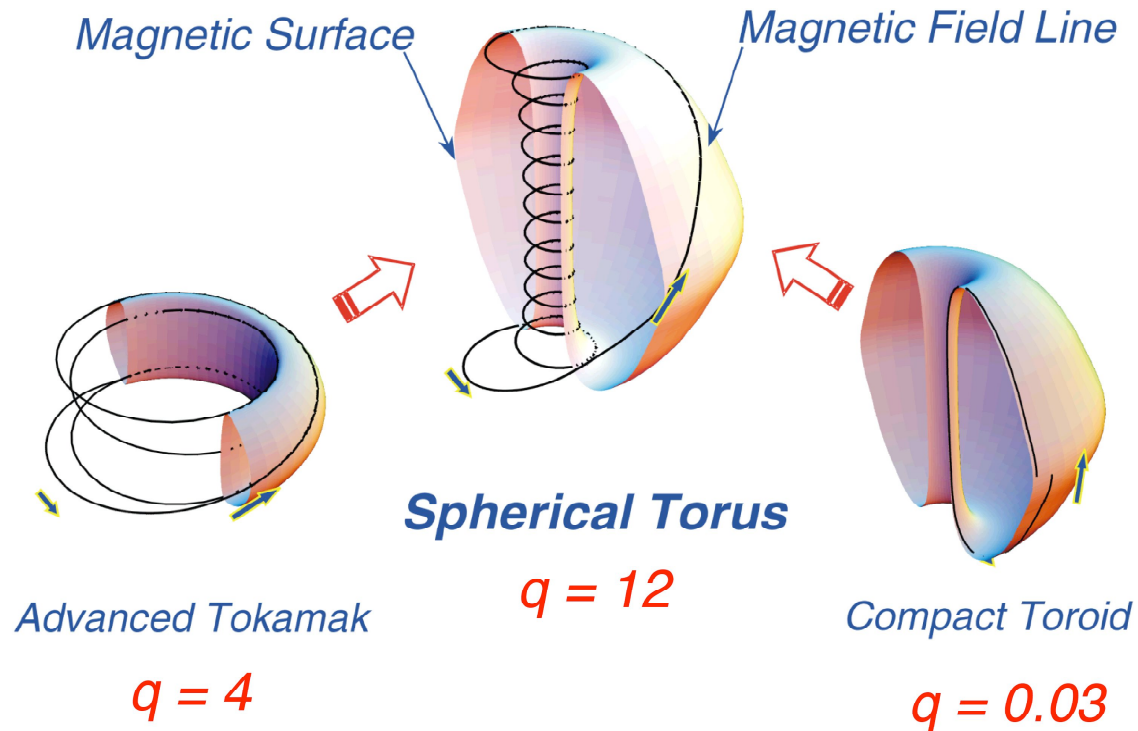
- Bombardment with $3.5 \times 10^{27} \text{ He}^+/\text{m}^2$ at $E_{\text{ion}} = 11 \text{ eV}$ for $t = 36,000 \text{ s}$



100 nm (VPS W on C) (TEM)

- Structures appear on scale of tens of nm and reflect swelling due to “nanobubbles”

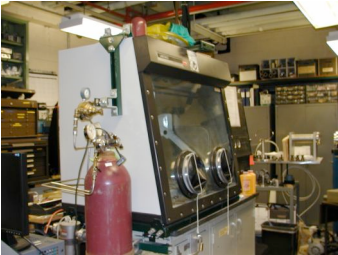
Research on Plasma-Facing Components Focused on Spherical Torus Devices at PPPL



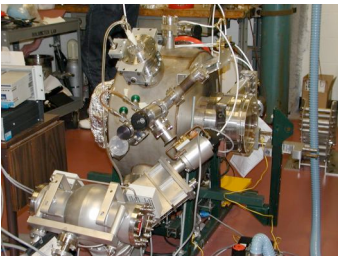
- **Spherical Torus represents “intermediate” confinement scheme**
 - Tokamak: toroidal current dominates
 - Compact toroid: poloidal current dominates
- **Greater field line length on inboard “high field” side improves confinement and stability**
 - Reduces toroidal field required for more efficient magnetic confinement

Lithium Tokamak Experiment and National Spherical Torus Experiment used to develop PFC's for future machines

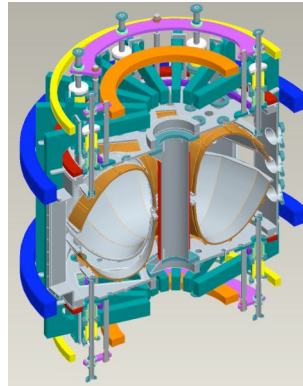
LTX lithium handling facility



LTX PFC test facility



Purdue surface analysis facilities



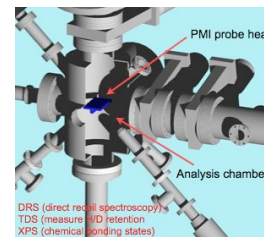
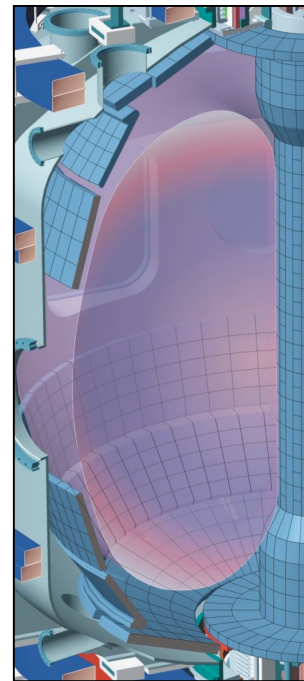
LTX

- Fully-nonrecycling liquid lithium PFC's
- Profile control with core fueling

NSTX

- High performance plasma with lithium PFC's
- High power divertor using liquid lithium

NSTX materials analysis probe



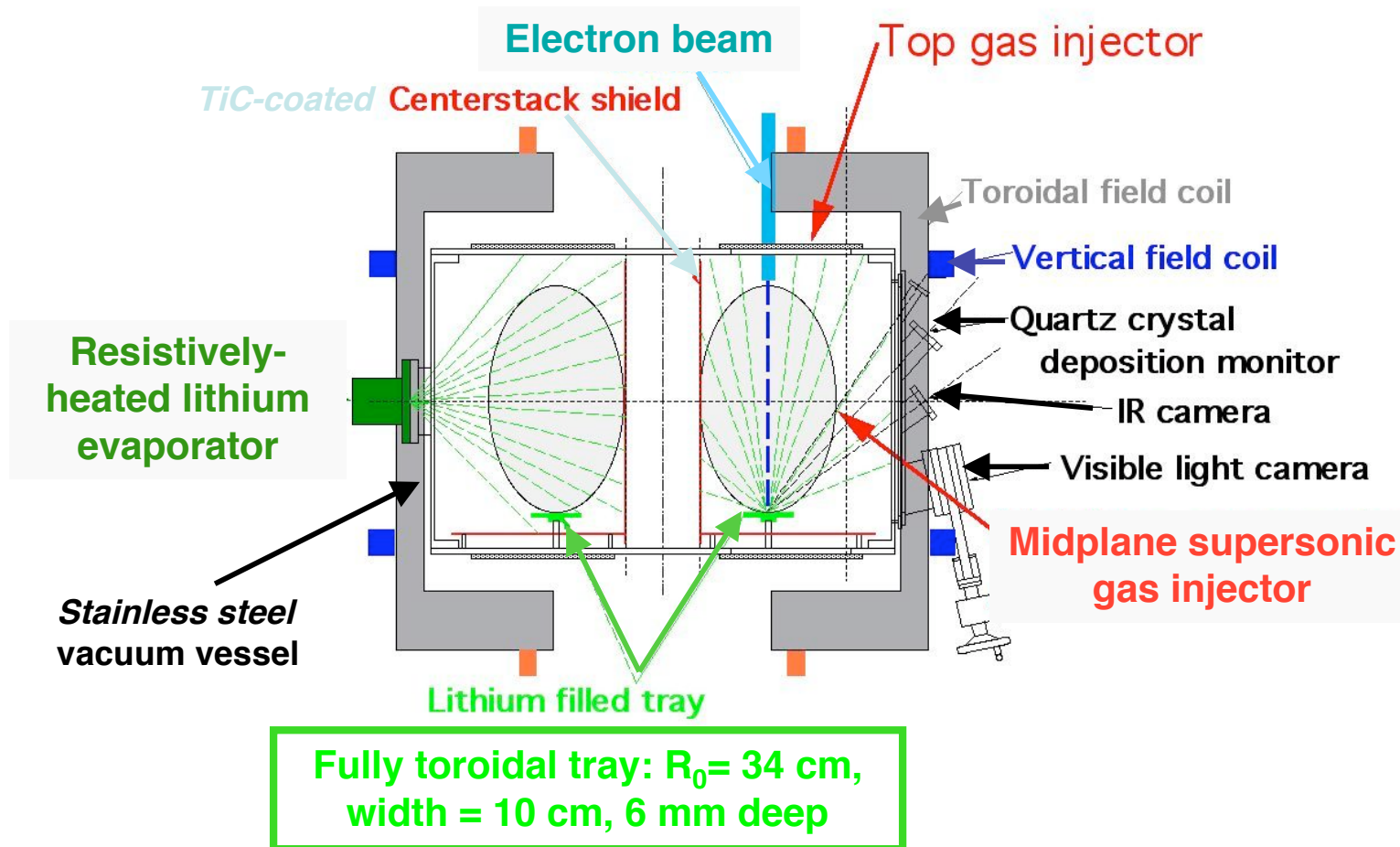
DRS (direct recoil spectroscopy)
TDS (measure WD retention)
XPS (chemical bonding states)

Next Step ST's

Retention of hydrogenic species and impurities

Initial “free-surface” liquid lithium experiments performed on Current Drive Experiment-Upgrade

$R_0=34$ cm, $a = 22$ cm, $I_p \leq 80$ kA, $B_T(0) \leq 2.1$ kG, $T_e(0) \sim 100$ eV, $n_e(0) < 6 \times 10^{19}$ m⁻³



Stainless steel “tray” installed on Current Drive Experiment-Upgrade (CDX-U) to hold lithium



- 34 cm major radius, 10 cm wide, 0.64 cm deep

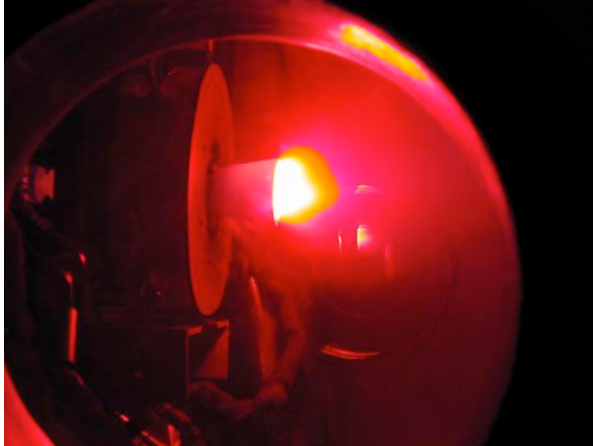
- Fabricated in two halves with a toroidal electrical break

- Heaters beneath for temperature control up to 500°C

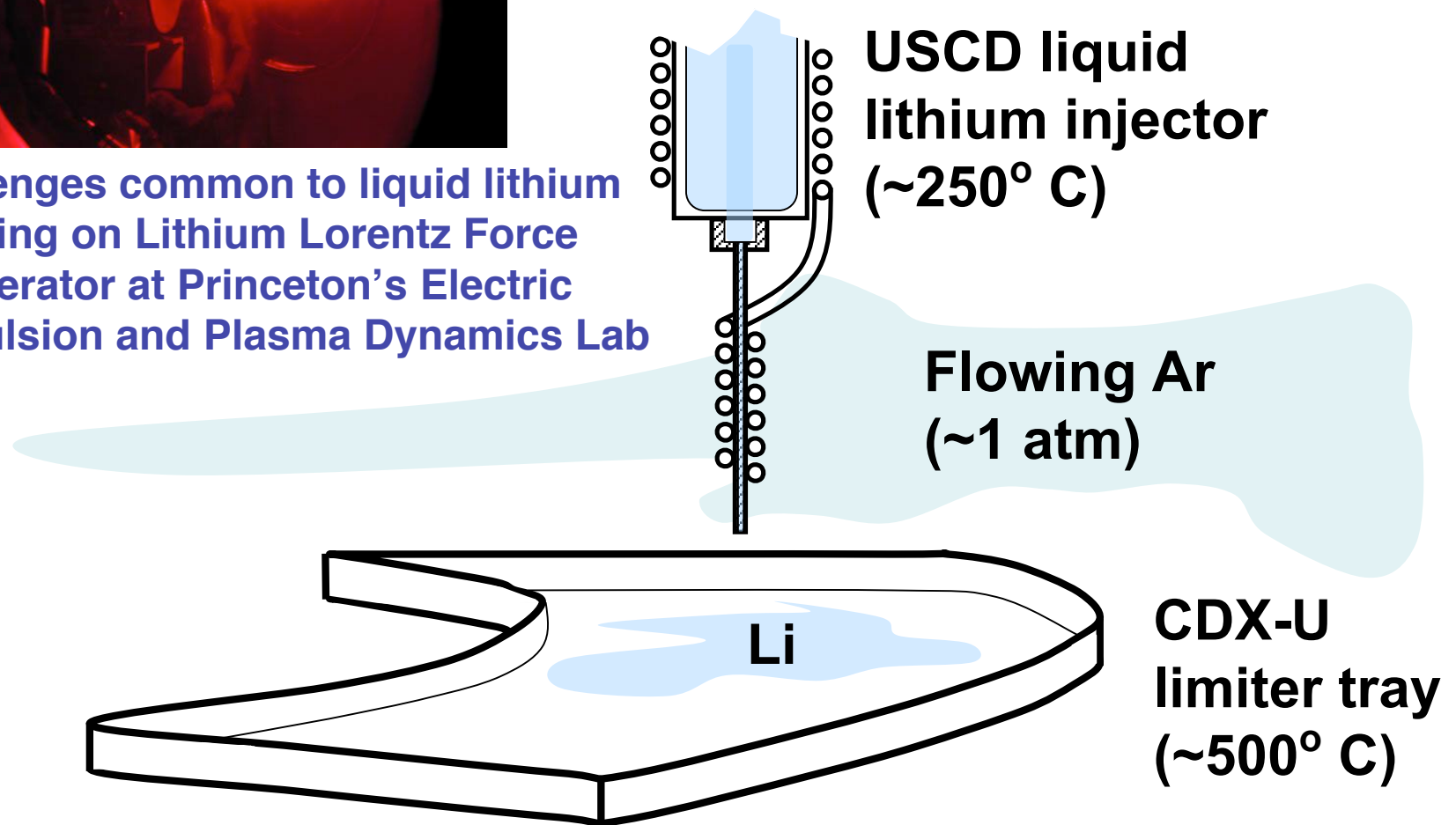
- Heat/lithium shield between tray and lower vacuum flange

- Heat shield on center stack

University of California at San Diego (UCSD) asked to develop liquid lithium loading system required to fill “tray”



- Challenges common to liquid lithium handling on Lithium Lorentz Force Accelerator at Princeton's Electric Propulsion and Plasma Dynamics Lab



Complex arrangement of heated reservoir and transfer tube needed to keep lithium liquid during loading

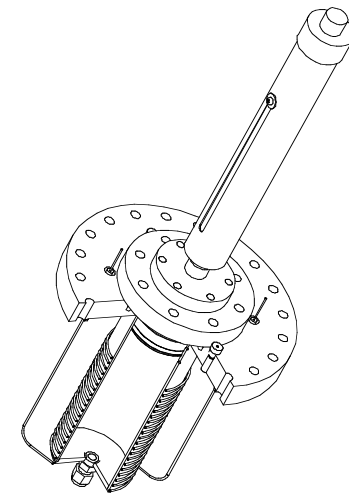
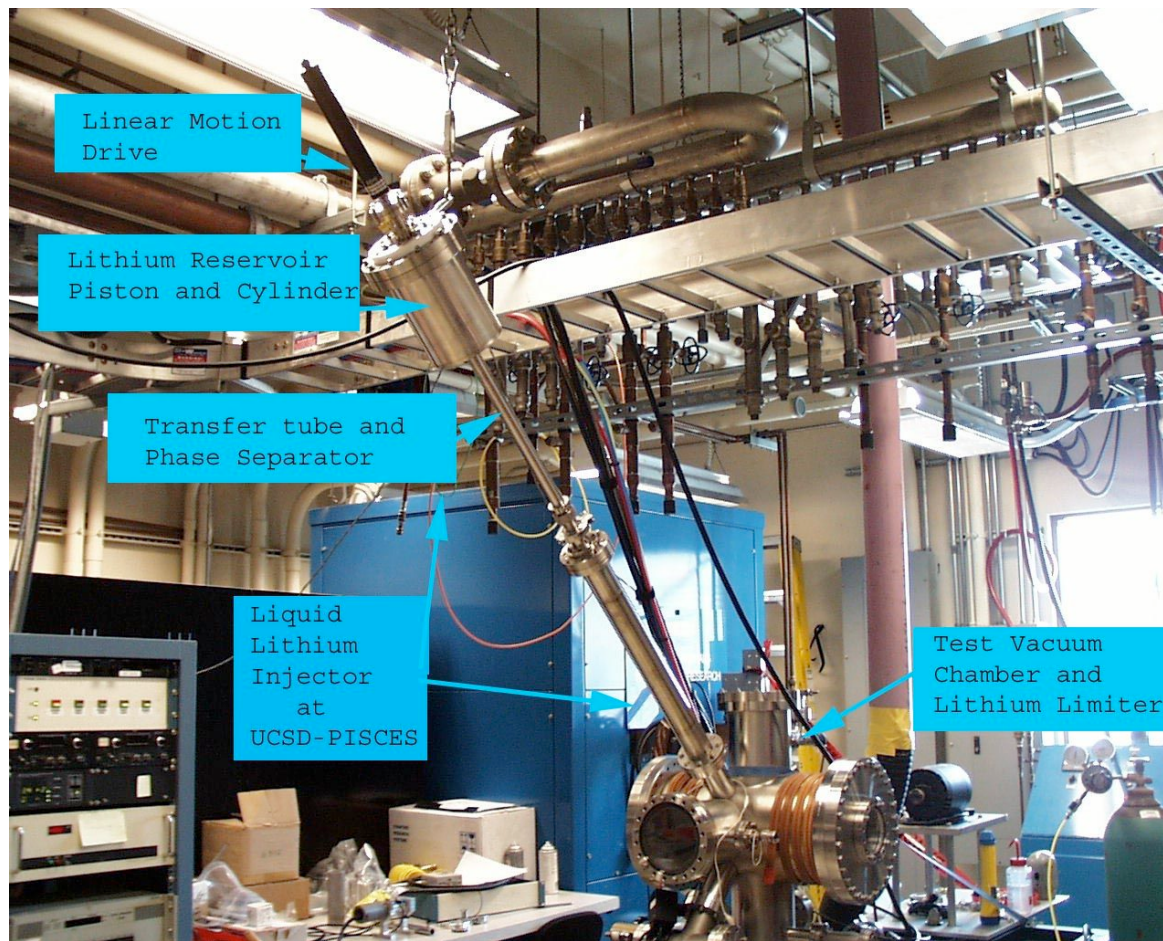
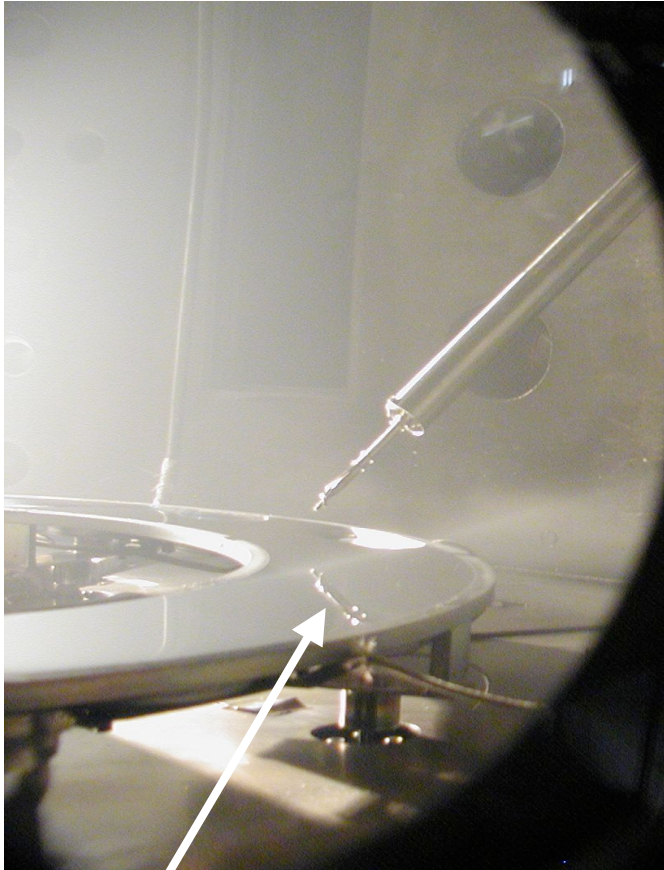


Diagram showing heated liquid lithium reservoir with motion drive and piston

Loader successful in transferring liquid lithium to heated “tray” inside CDX-U vacuum chamber

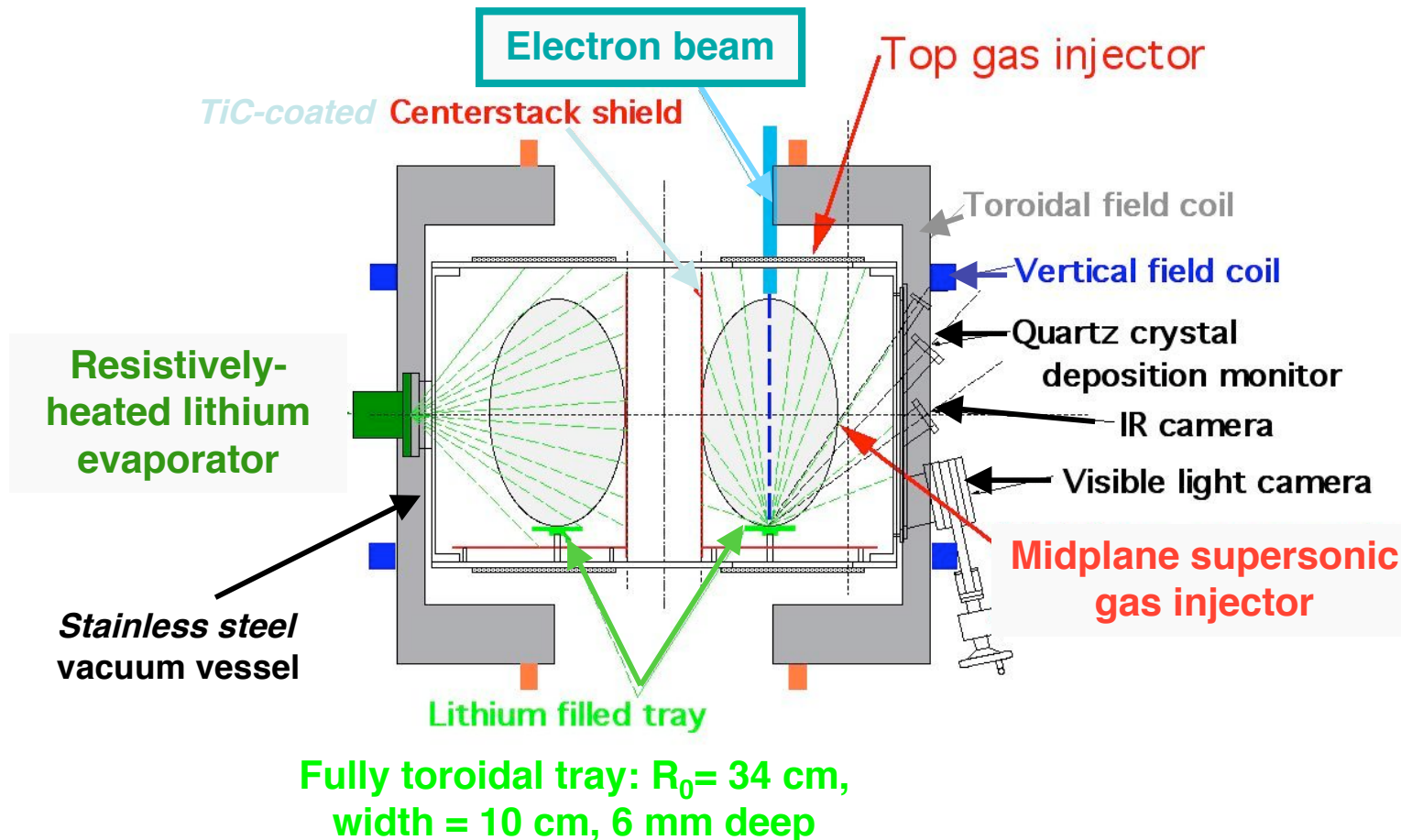


- **Tip of loader reflected on surface of liquid lithium covering tray**



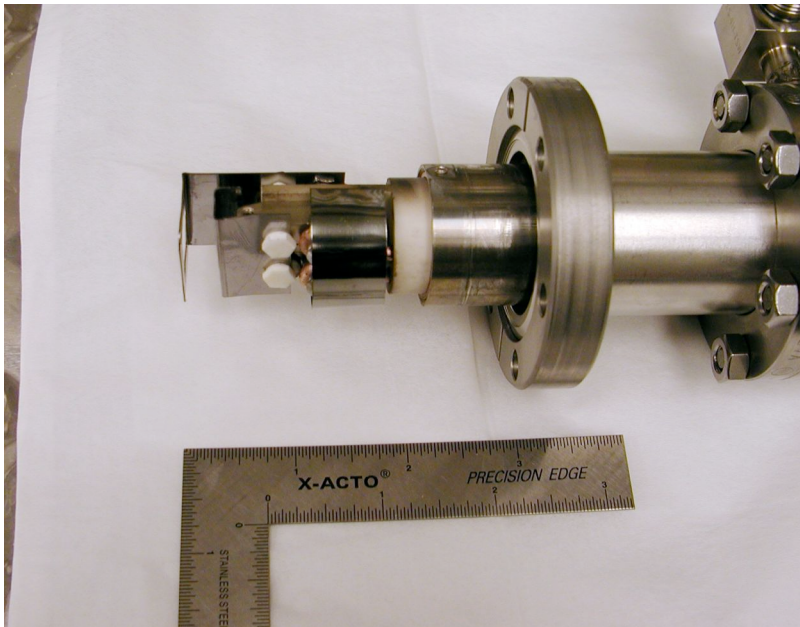
- **Closeup of loader end showing heater extending to tip**

Electron beam installed initially for as method to create lithium-coated PFC's



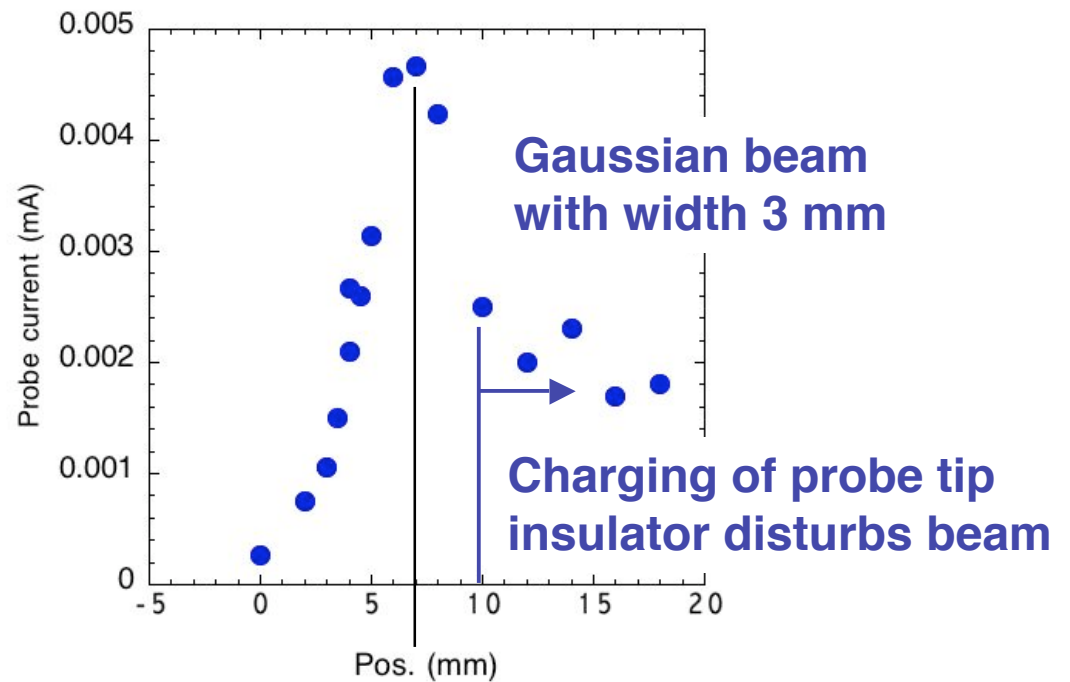
- “Tray” only provides “partial” liquid lithium PFC
- Resistively-heated evaporator and electron beam heating lithium in tray provide greater PFC coverage

Commercial electron beam (e-beam) used to provide intense local heating of lithium

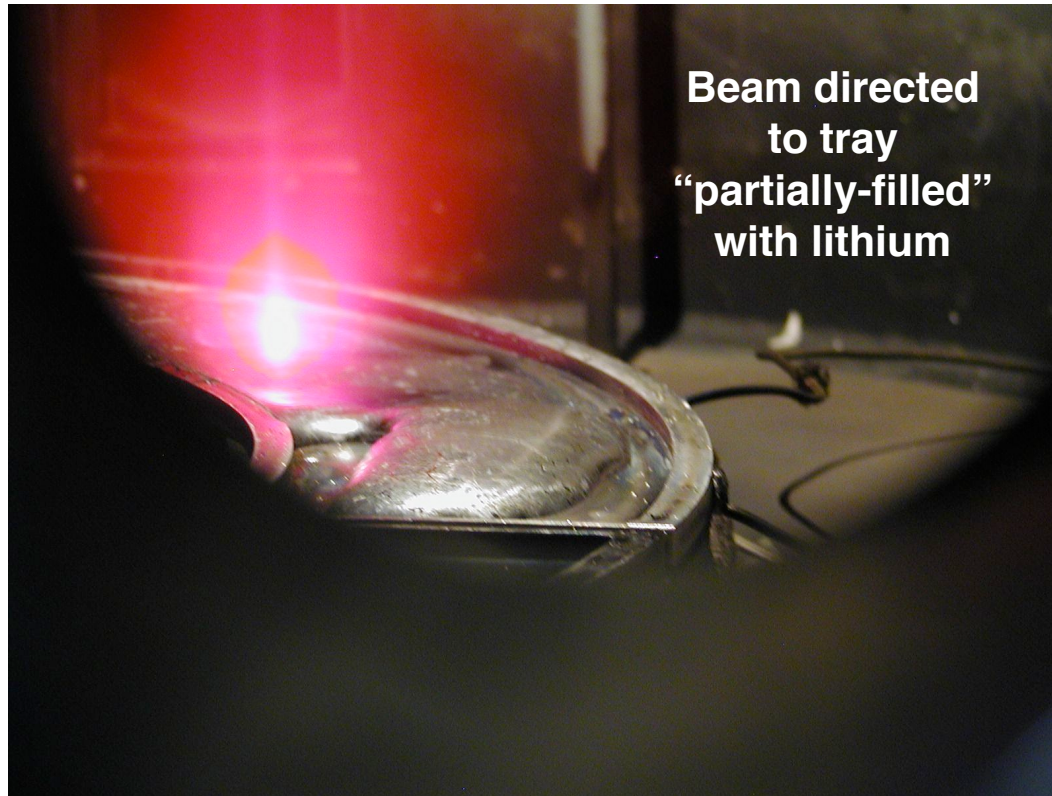


**Modified commercial
electron beam head**

Measured electron beam profile

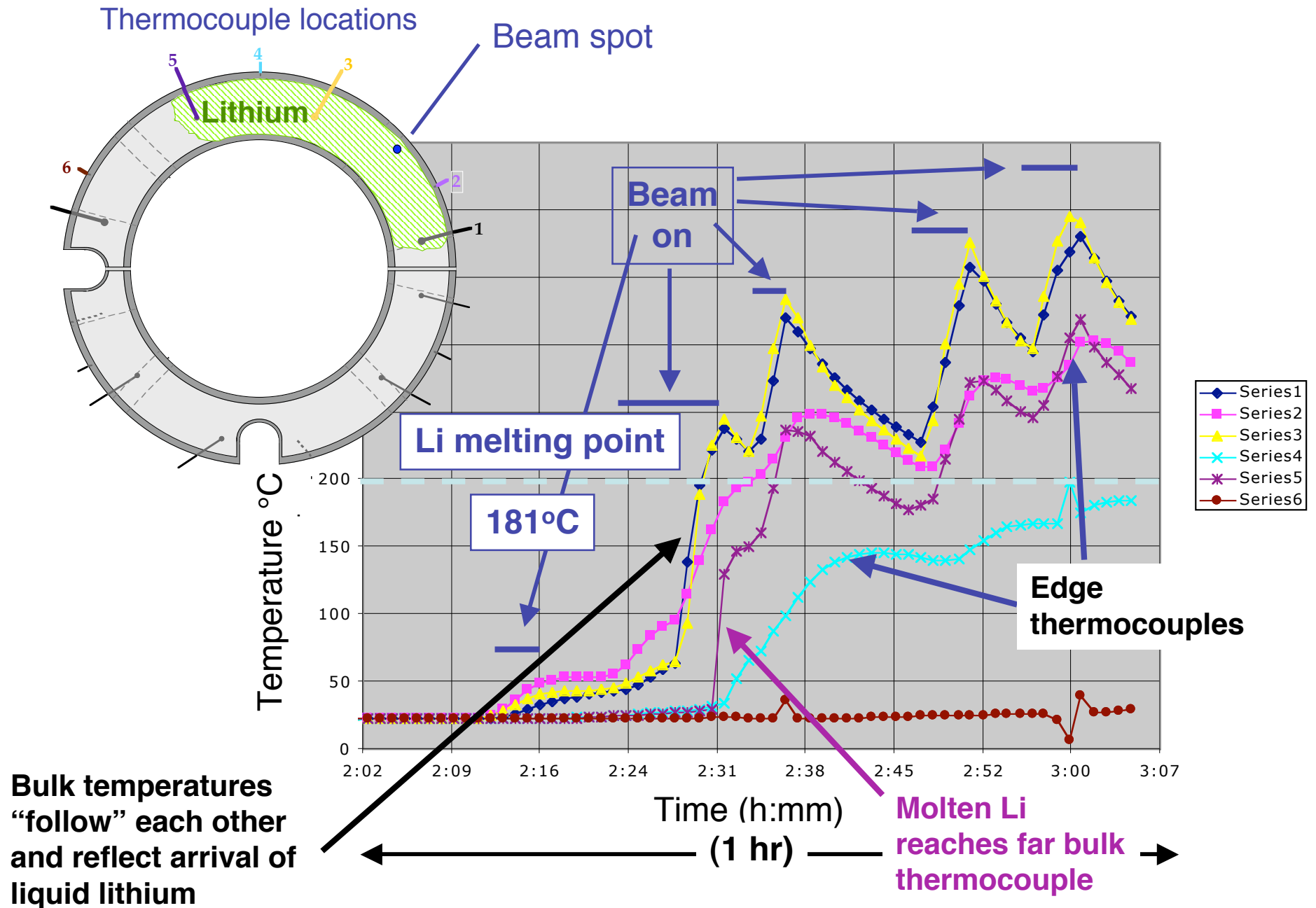


Tokamak poloidal field coils used to provide vertical “guide” field to direct e-beam to lithium

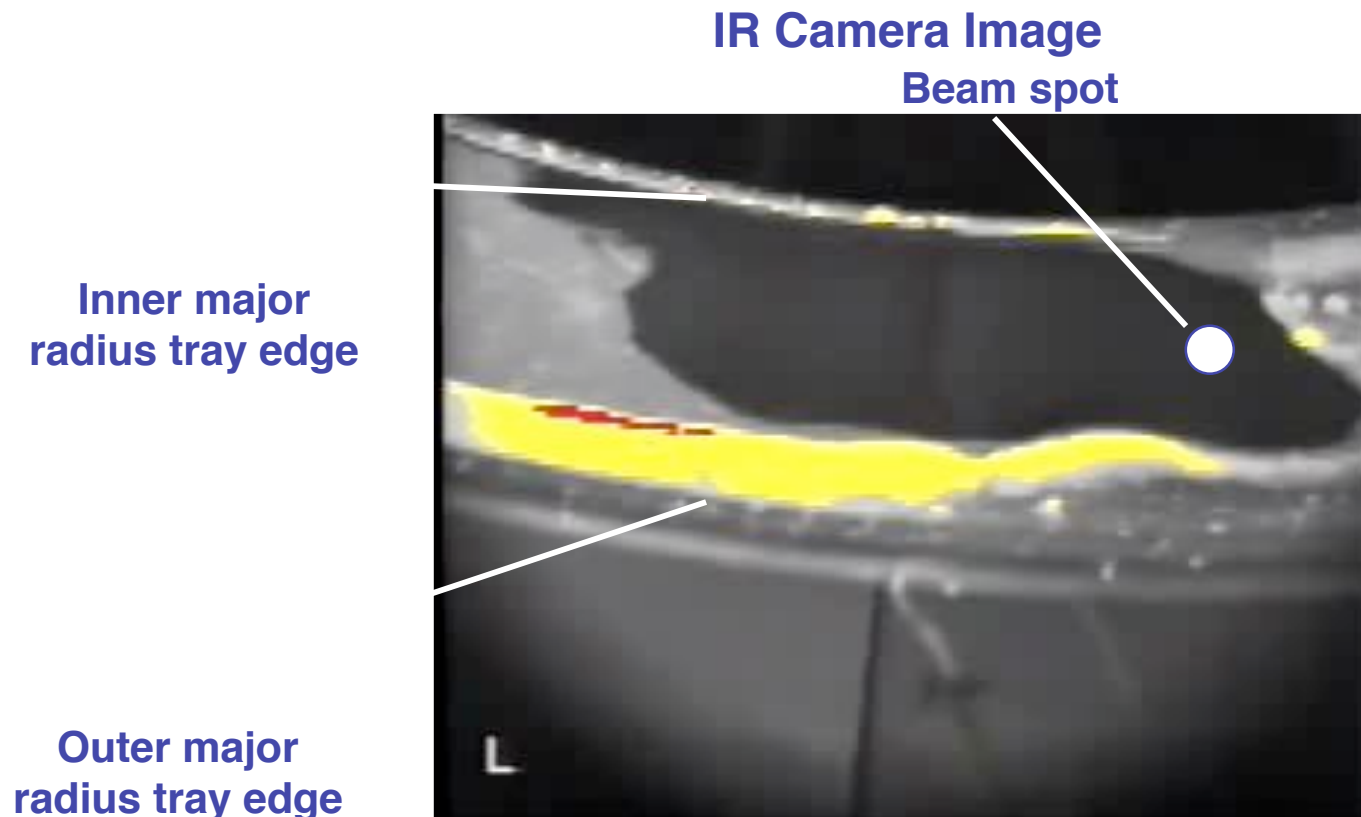


- 100 nm lithium wall coatings at maximum evaporation rate of 600 mg/minute
 - CDX-U magnetic fields guide 4 kV, 0.3 - 0.4 A beam for 300 - 400 seconds
 - Lithium area in tray $\sim 600 \text{ cm}^2 \gg$ beam spot for power density up to 60 MW/m²

All lithium liquefied before evaporation occurs



Localized heat deposition affects surface tension and “Marangoni effect” can induce lithium flows



- Yellow denotes $+55^{\circ}\text{C}$, red denotes $+110^{\circ}\text{C}$
- Area under beam should go to 1400°C in 0.1 sec with conduction only
 - No “hot spot” appears however
 - Shows ability of lithium to dissipate high beam power densities

Marangoni convection can lead to high fluid velocities and efficient heat transfer

Dependence of surface tension on temperature imposes boundary condition:

$$\text{Viscosity} \quad \left. \nu \vec{V}_n' \right|_{\text{surface}} = \frac{\text{Derivative of surface tension} \quad d\sigma(T)}{dT} \nabla_s T$$

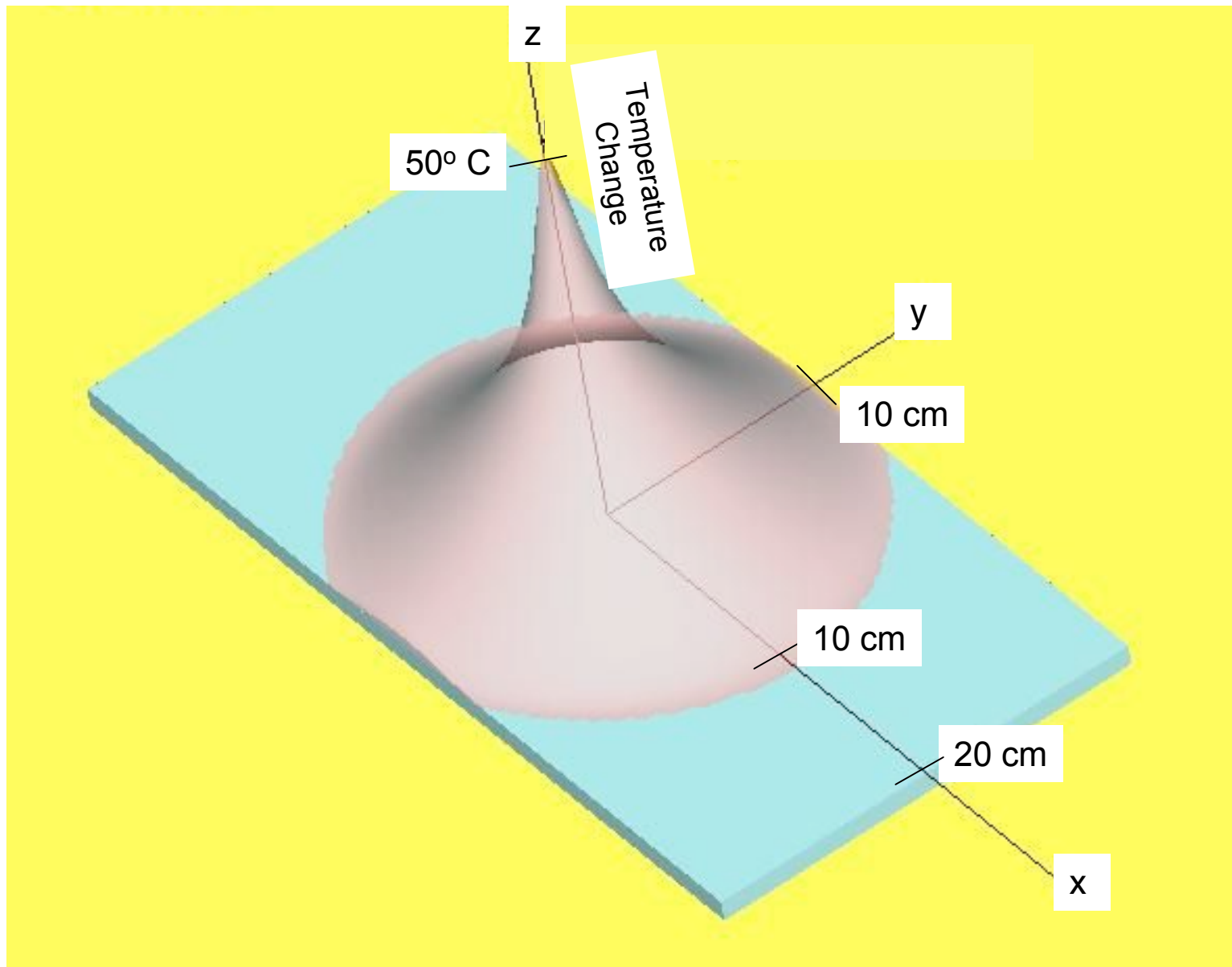
Derivative of fluid velocity normal to surface

Solve for fluid velocity in terms of viscous boundary layer d:

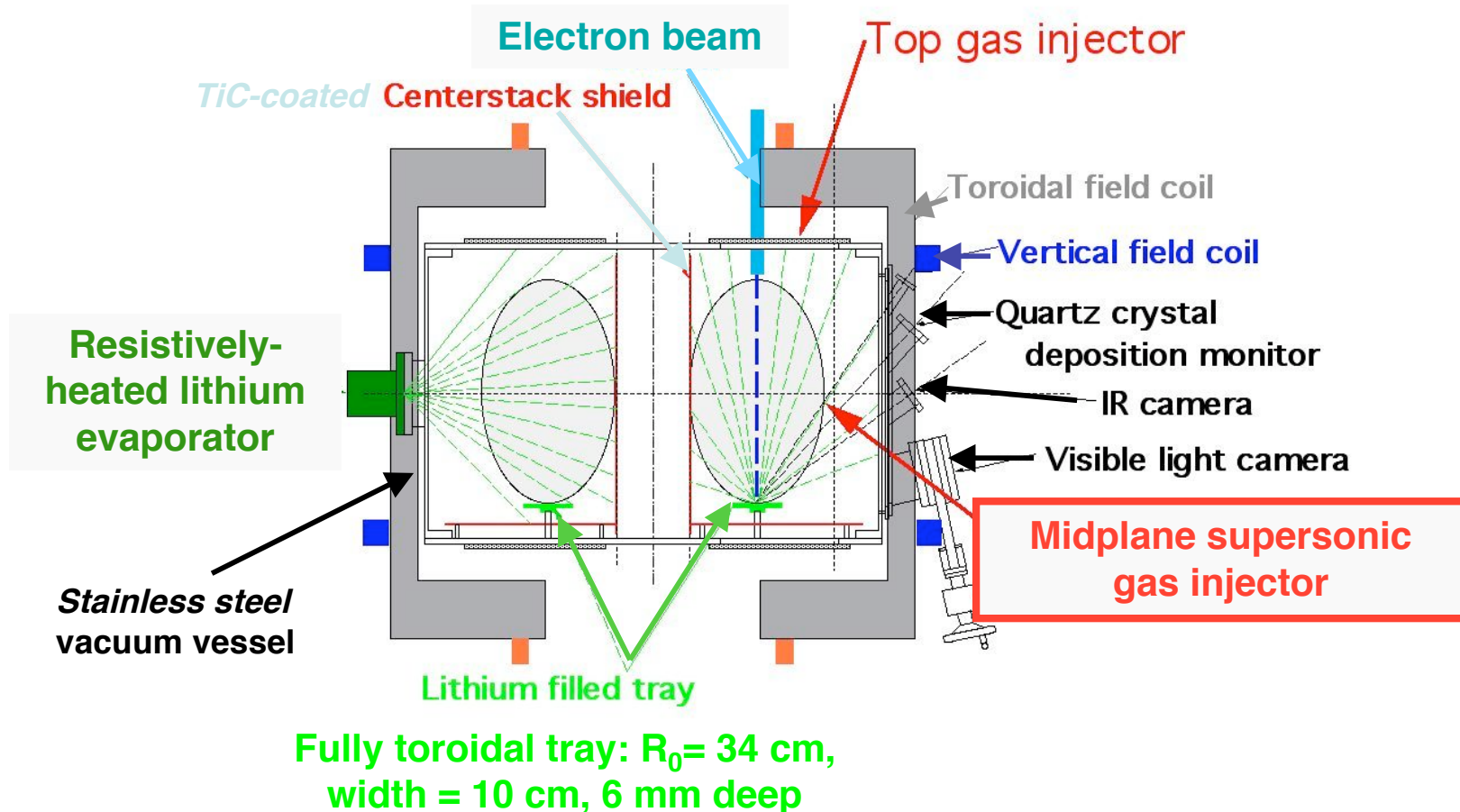
$$\vec{V} = \frac{1}{\nu} \frac{d\sigma(T)}{dT} \nabla_s T d$$

- Using values for lithium leads to velocity of 10 m/s
- Leads to efficient heat transfer from e-beam spot

Calculations show modest temperature rise over broad area instead of highly localized heating

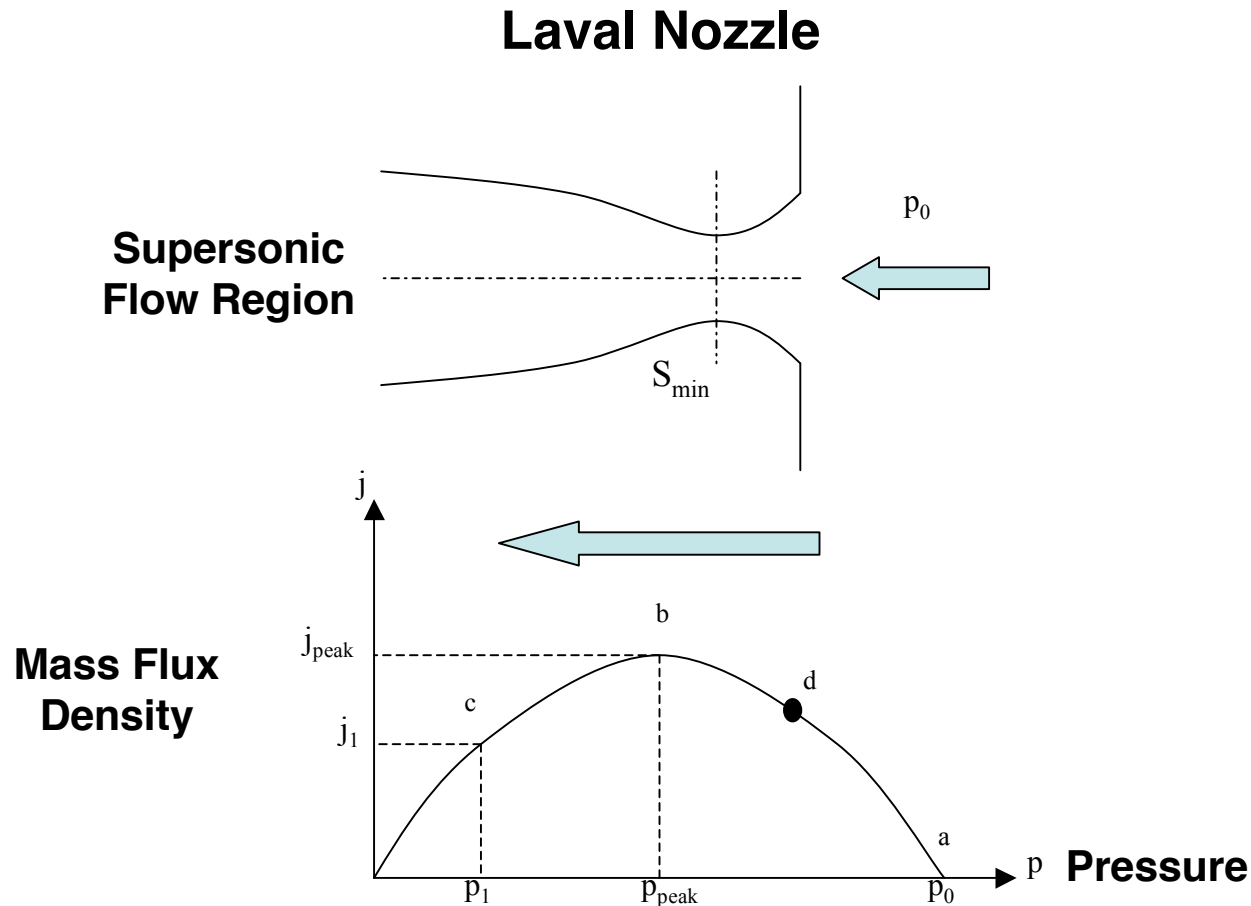


Ability of lithium PFC to “pump” hydrogen “working gas” required new fueling methods



- “Top” gas injector consists of simple tube attached to vacuum chamber
 - Distance from plasma limits fueling efficiency
 - Separation of gas valve from end of tube leads to slow time response

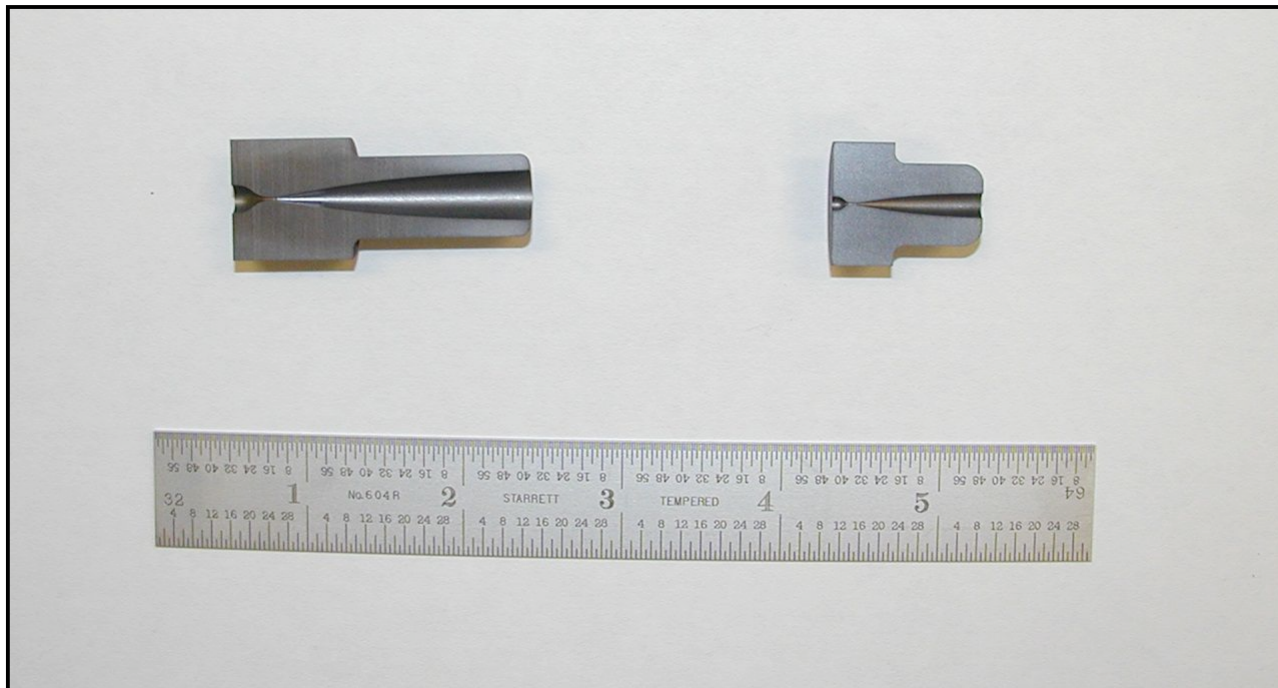
Supersonic gas injector (SGI) implemented to improve fueling



- Principle well-established for large nozzles in aerospace applications
 - Situation not clear for small-scale nozzles needed for plasma fueling

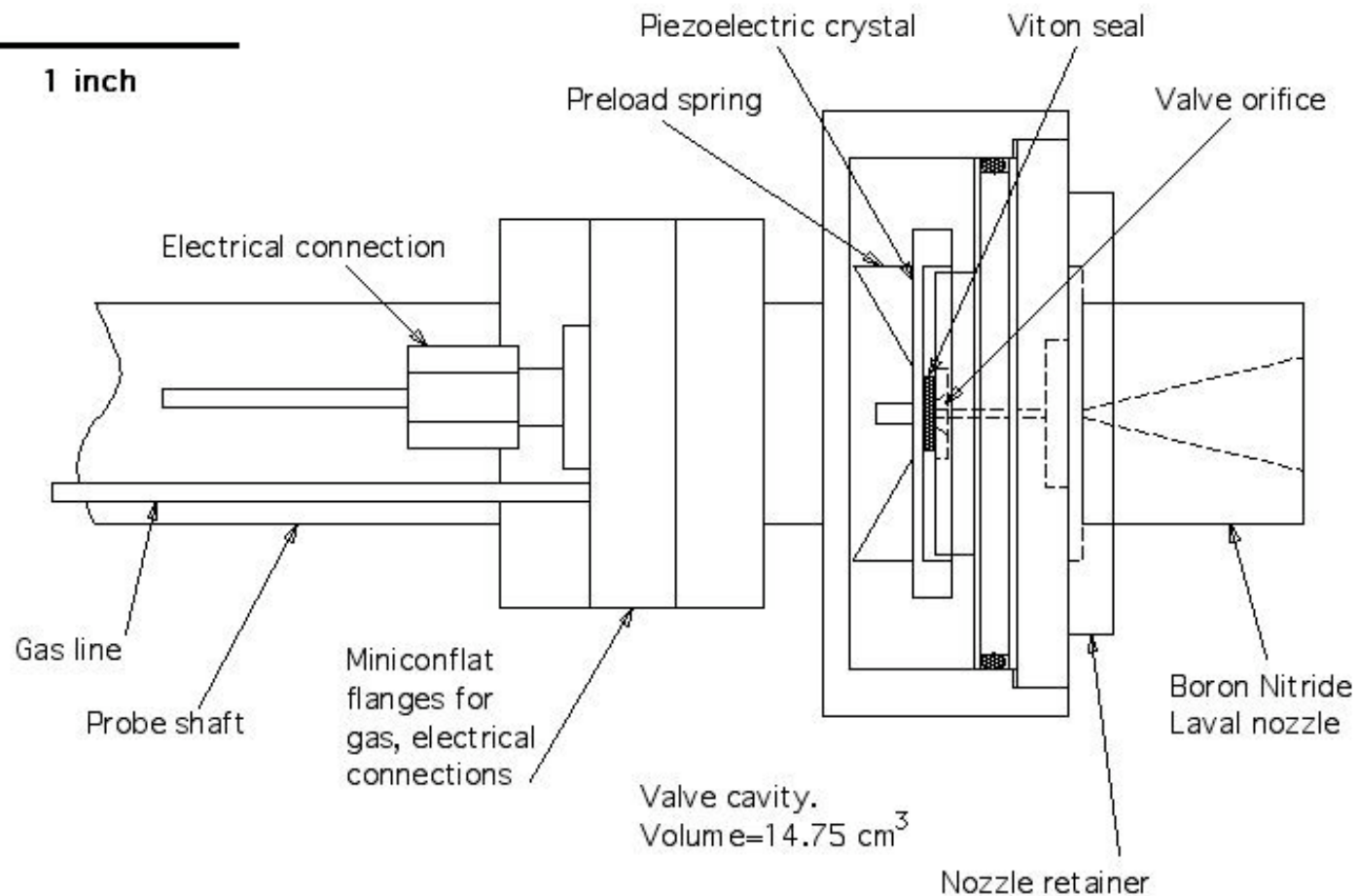
First attempt involved only scaling down design for Mach 8 nozzles

- Original design included 0.6 inch throat diameter [Ph. D. Thesis Princeton University Department of Mechanical and Aerospace Engineering, 1997]
- New graphite nozzles built with 0.02 and 0.01 inch throat diameters



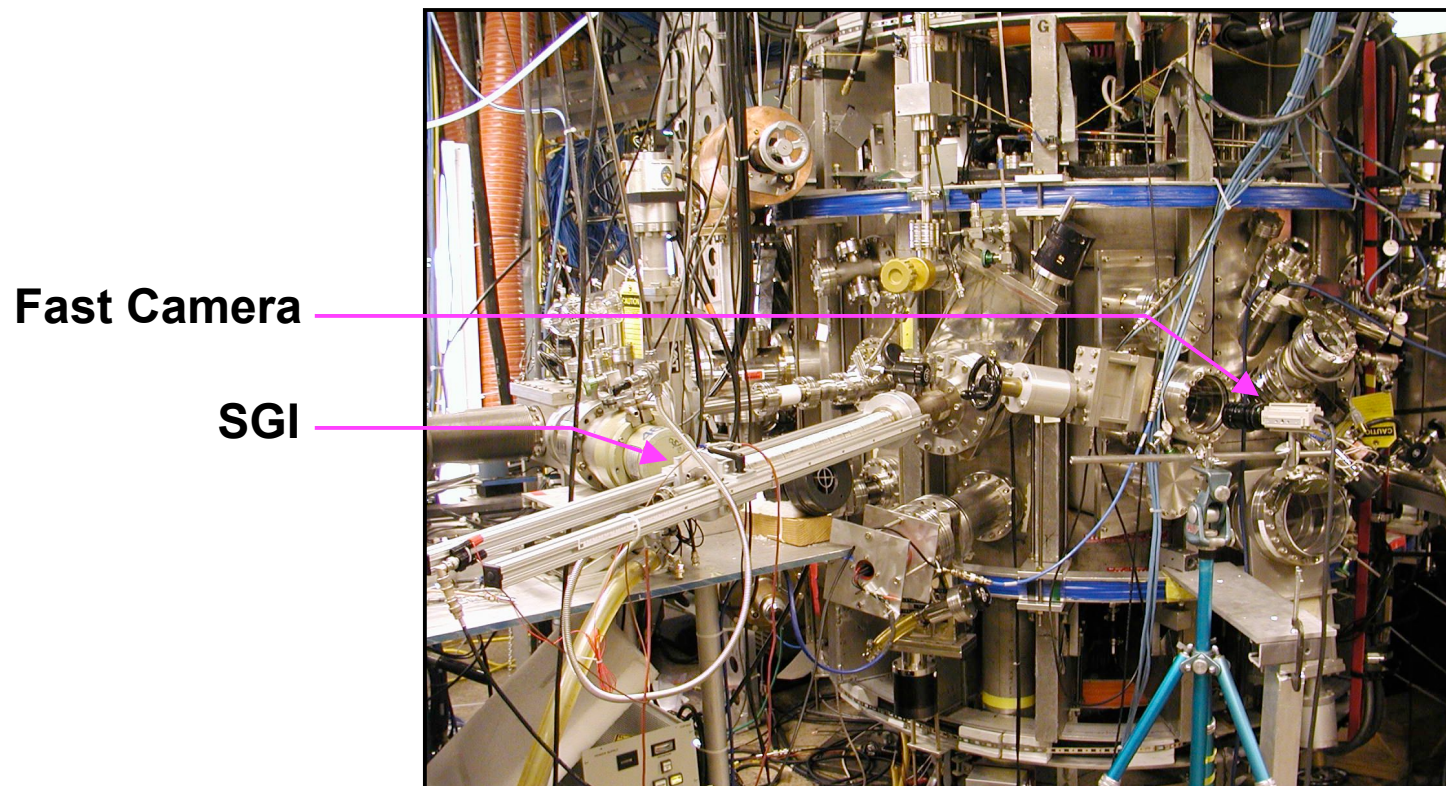
Close coupling of valve to nozzle permits fast time response

Assembly drawing - modified PV-10 piezoelectric valve with mount and Laval nozzle

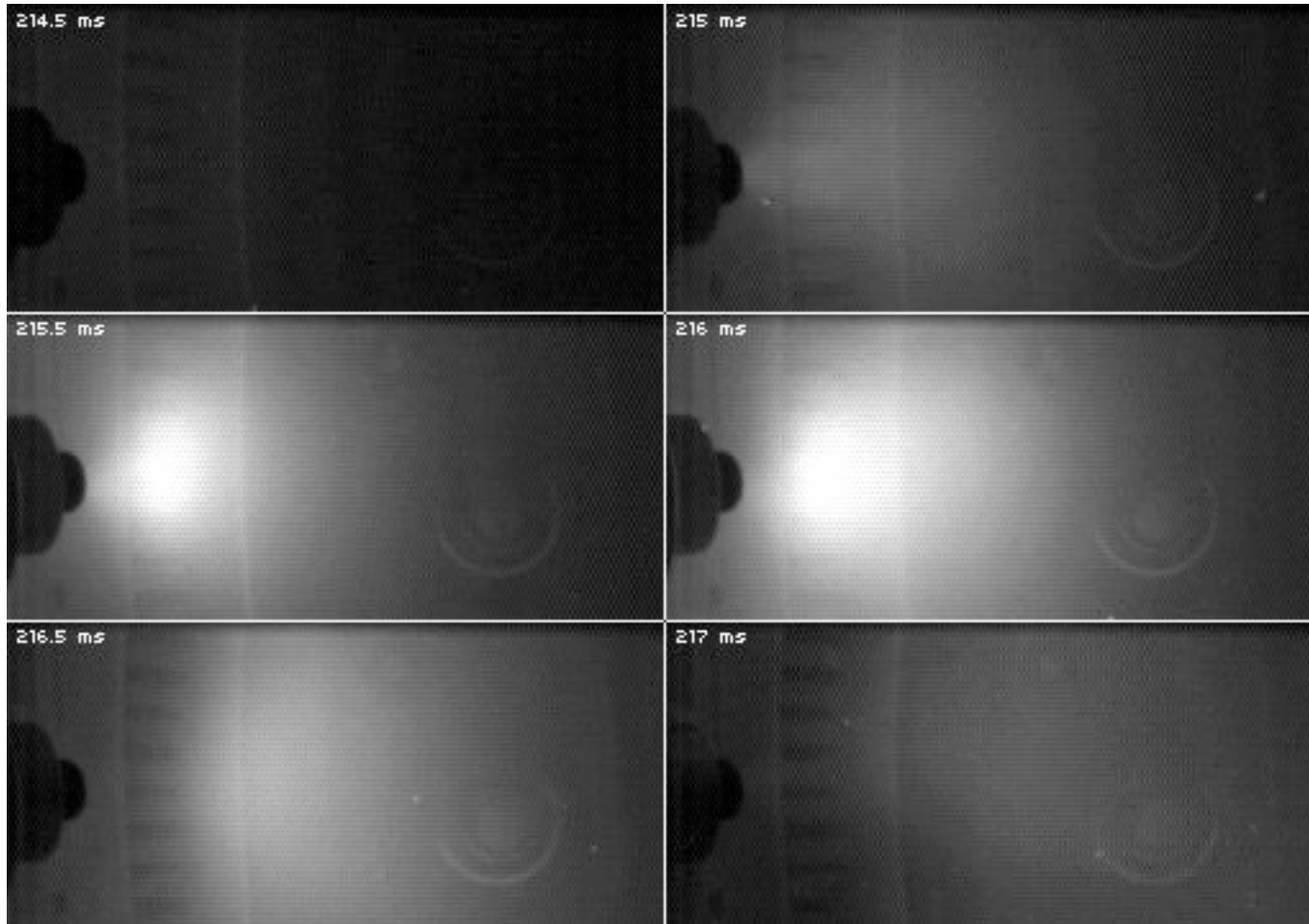


SGI installed on CDX-U with position adjustment capability

- SGI mounted radially
- Fast visible camera installed with tangential view
 - Used to image gas plume from SGI



Gas injection from SGI imaged



Lithium PFC's expected to reduce recycling

- **“Conventional” PFC**
 - Hydrogenic “working gas” not retained in PFC
 - Influx of gas back into plasma becomes major fueling source (“high recycling”)
 - Results in long effective particle confinement time
- **Lithium PFC**
 - High chemical reactivity with hydrogen isotopes means “working gas” is trapped in PFC
 - PFC is no longer major fueling source (“low recycling”)
 - Results in short effective particle confinement time

Density measurements during SGI fueling used to determine effect of lithium PFC's on recycling

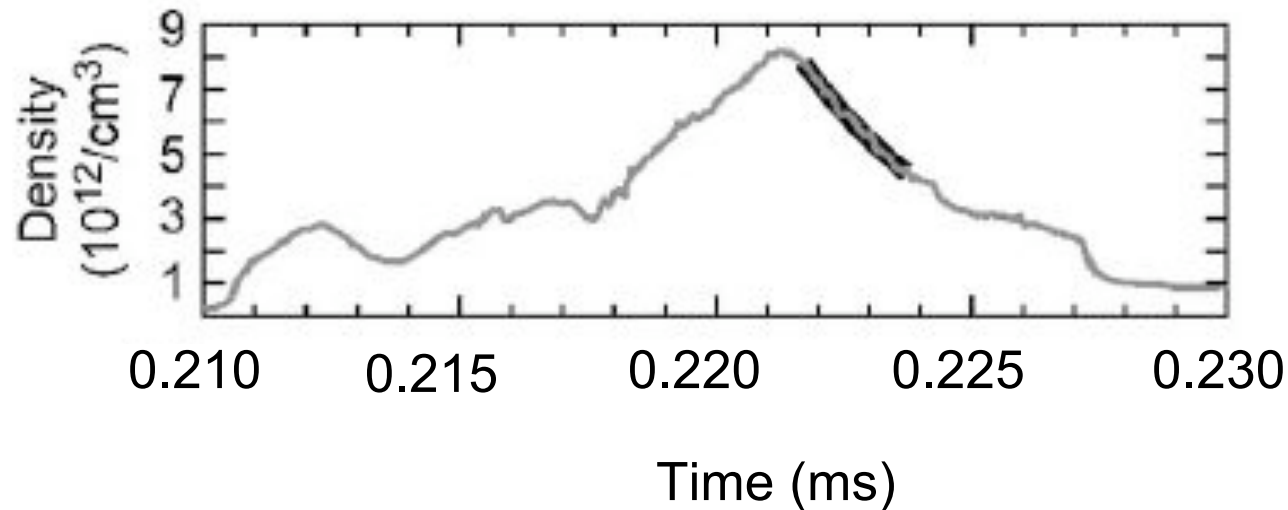
- Define “effective” particle confinement time as function of recycling coefficient R
 - High recycling means high effective particle confinement time

$$\tau_p^* = \frac{\tau_p}{1 - R}$$

- Time behavior of density then gives indication of R
 - Finite decay when SGI terminates means low recycling
 - PFC does not provide significant fueling

$$N_e = N_e(0) \exp\left(-\frac{t}{\tau_p^*}\right)$$

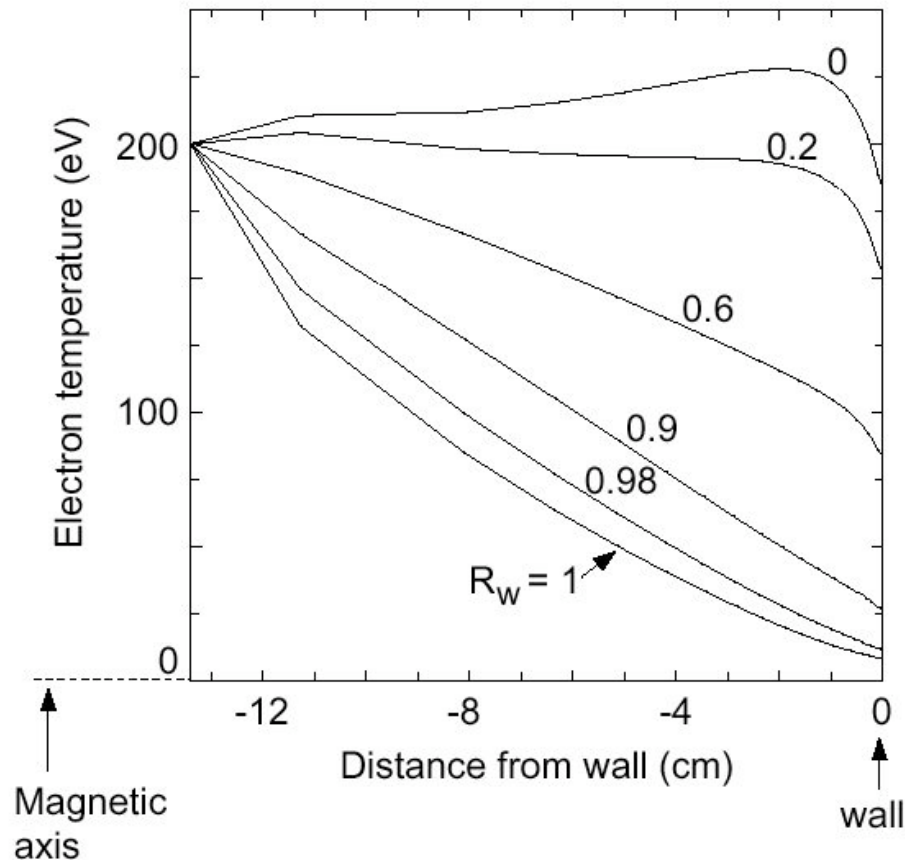
Measurements in plasmas with lithium PFC's indicate lowered recycling



- **Gas puff ends at 220 ms**
 - **Decay indicates dependence of density on external fueling**

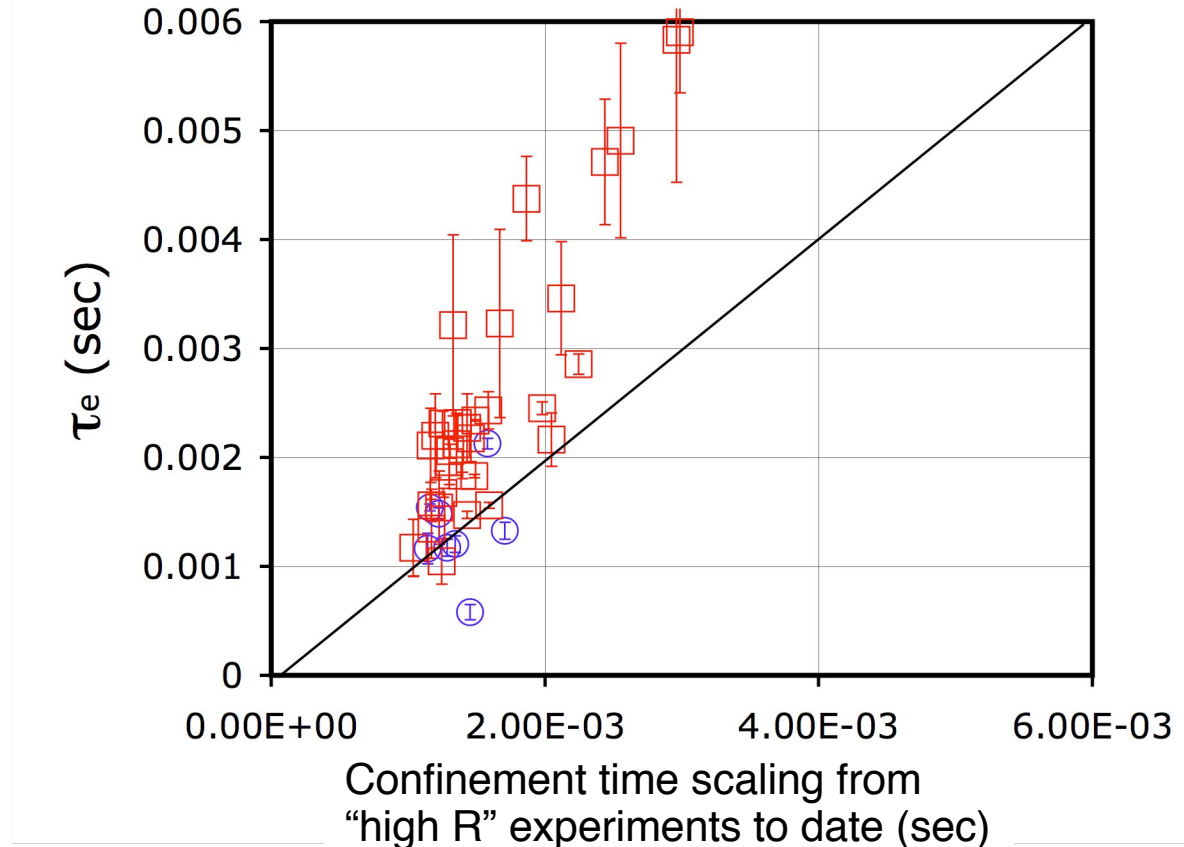
Salient prediction of low R is reduced transport due to “flattened” electron temperature profile

- Low R means suppression of cold gas flow back into plasma
 - Temperature gradients reduced across plasma
 - Lowered internal ∇T_e drive for turbulence-driven electron transport



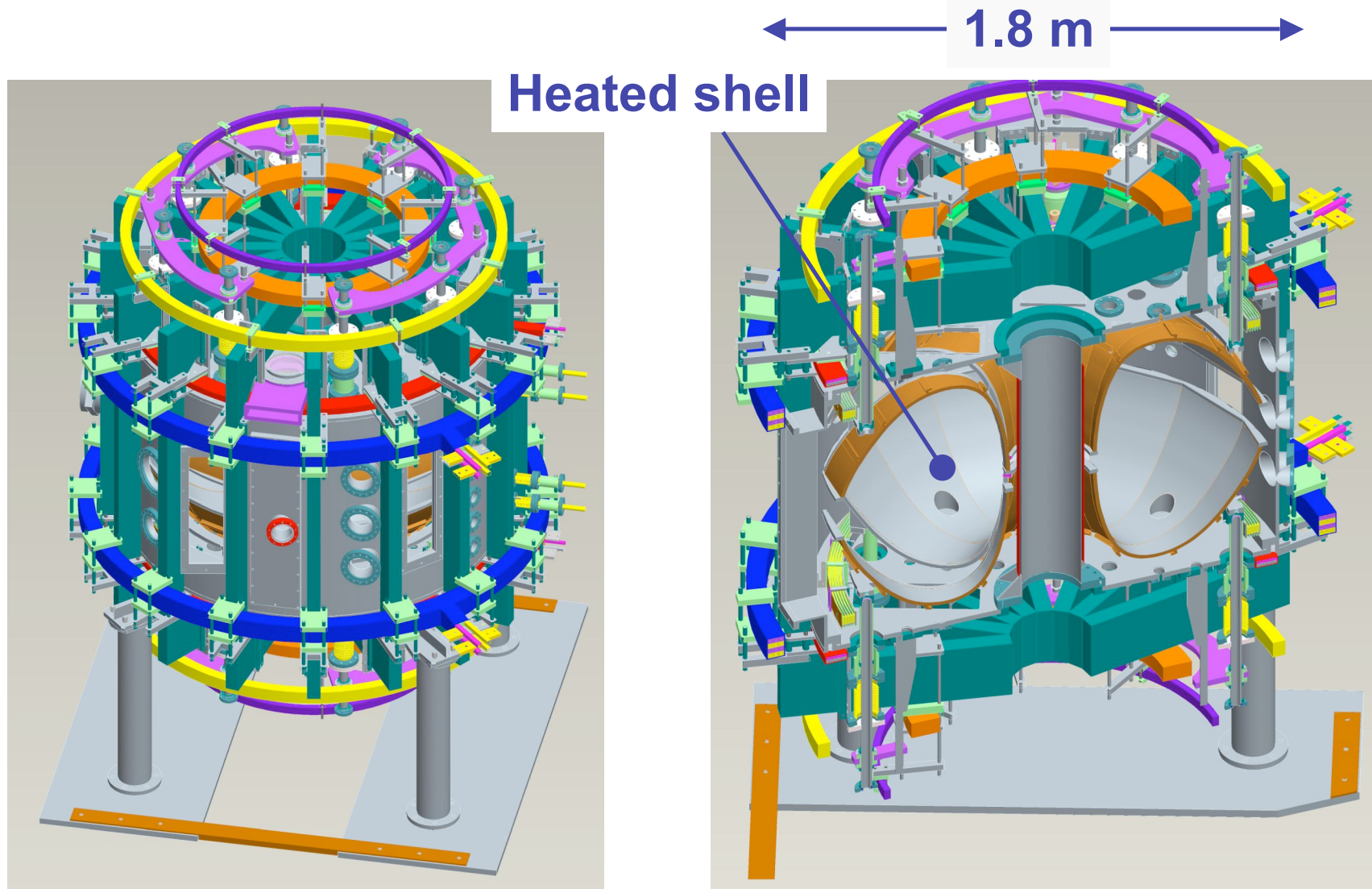
Demonstrated as R is varied in transport modeling from Lawrence Livermore National Laboratory

Results from CDX-U with “partial” lithium PFC’s exceed predictions from past experiments



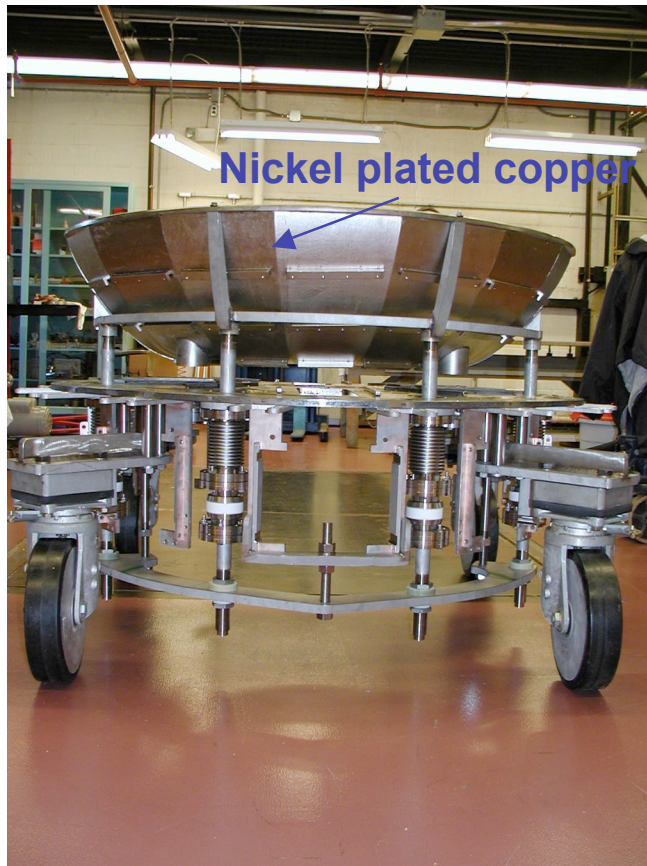
- **Lithium PFC’s improved confinement in CDX-U by 6 times or more**
 - **Exceeds scaling by factor of 2-3**
 - **Largest increase in ohmic tokamak confinement ever observed**

CDX-U performance motivated upgrade to LTX with lithium “shell” that nearly encloses plasma

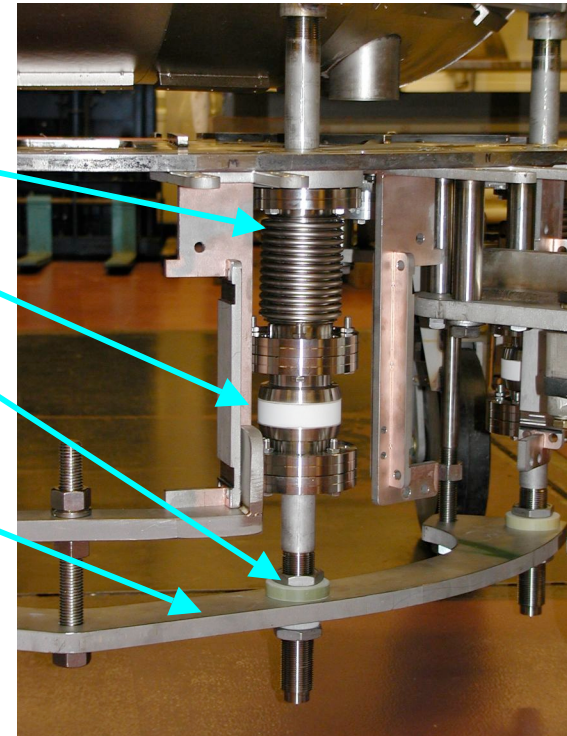


Lithium Tokamak Experiment (LTX)

Requirements for thermal and mechanical isolation create engineering challenges

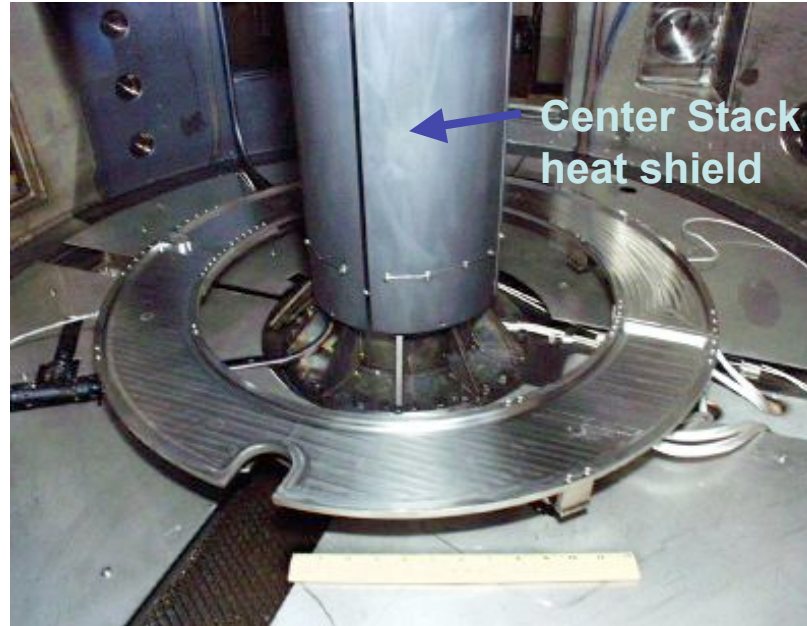
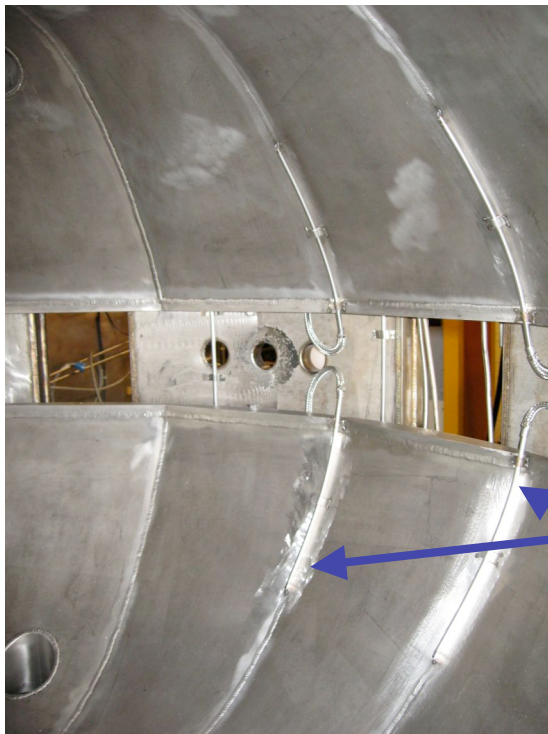


Bellows
Ceramic break
G10 bushing
External
mechanical
support structure

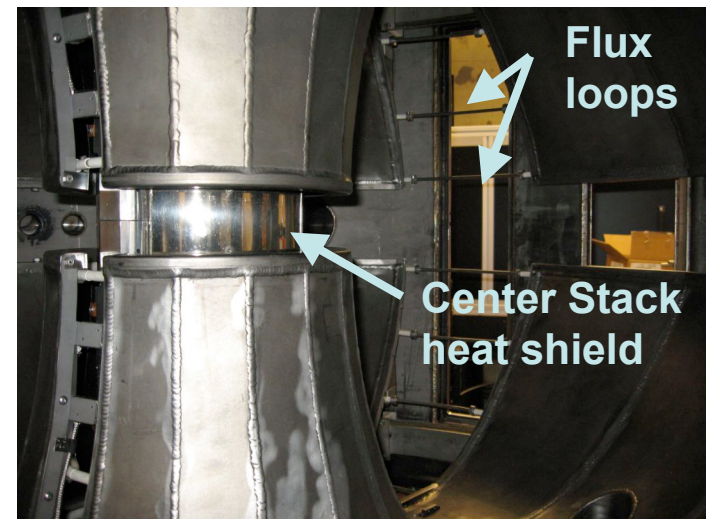


Heaters keep LTX shell above lithium melting point to provide liquid lithium PFC

LTX shell replaces CDX-U tray



Center Stack heat shield

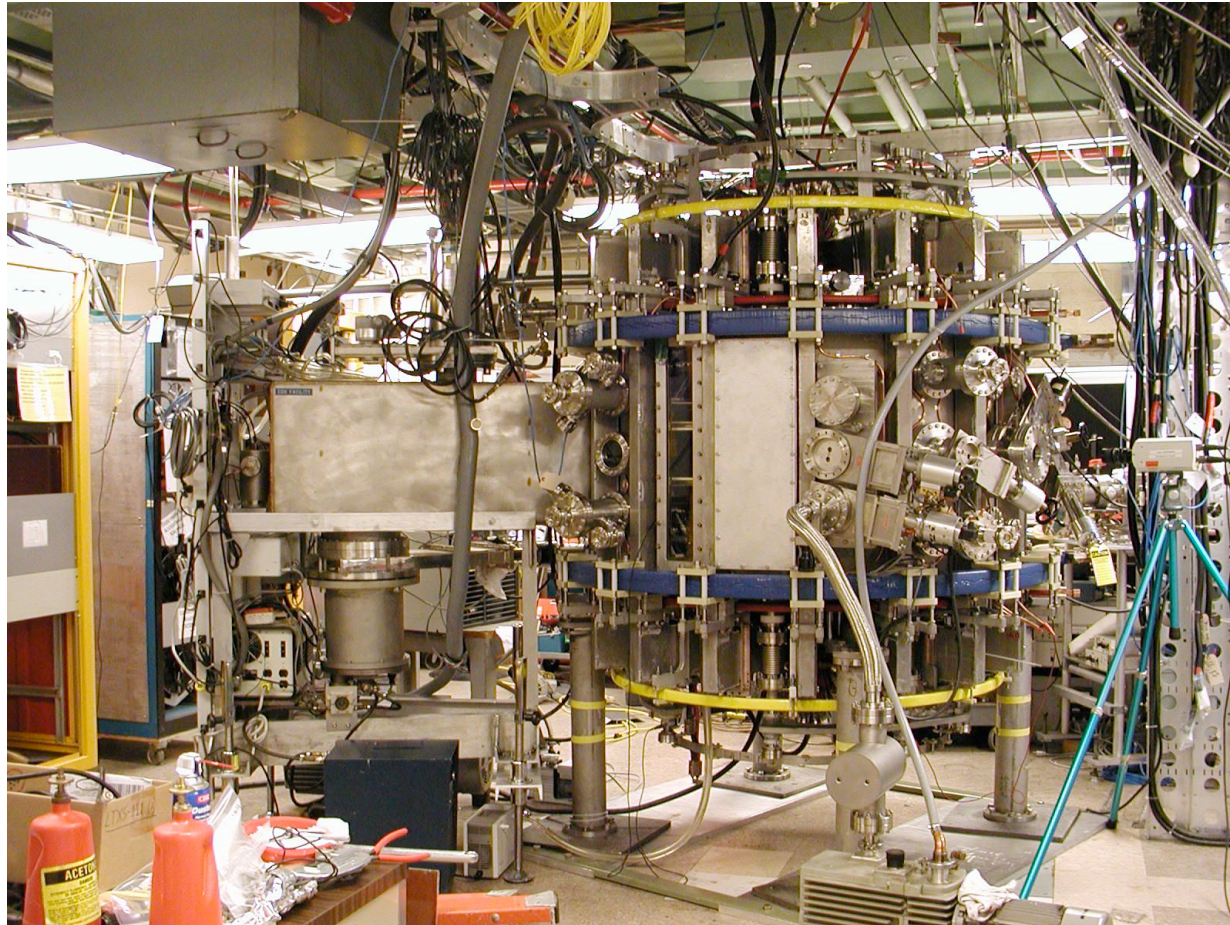


Flux loops

Center Stack heat shield

Protective tubes for magnetic field pickup ("Mirnov") coils

LTX complete and experiments beginning



- **First plasma achieved on 3 October 2008**
- **Diagnostics being installed**

Size and complexity of NSTX requires more measured approach to lithium PFC's

Device Parameters

$R = 85 \text{ cm}$

$a = 65 \text{ cm}$

$\kappa = 1.7 - 2.7$

$\delta = 0.3 - 0.8$

$B_T = 5.5 \text{ kG}$

$\tau_{TF} (3.5 \text{ kG}) \sim 3 \text{ sec}$
 $\sim 6 \tau_{\text{skin}}$

$I_p = 1.5 \text{ MA}$

$V_p = 14 \text{ m}^3$

$E_p \sim 430 \text{ kJ}$

$P_{\text{NBI}} = 7.4 \text{ MW}$

$P_{\text{HHFW}} = 6 \text{ MW}$

350°C bakeout

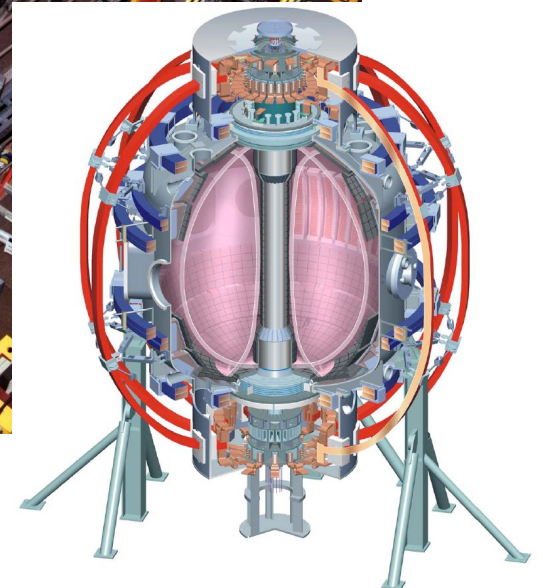
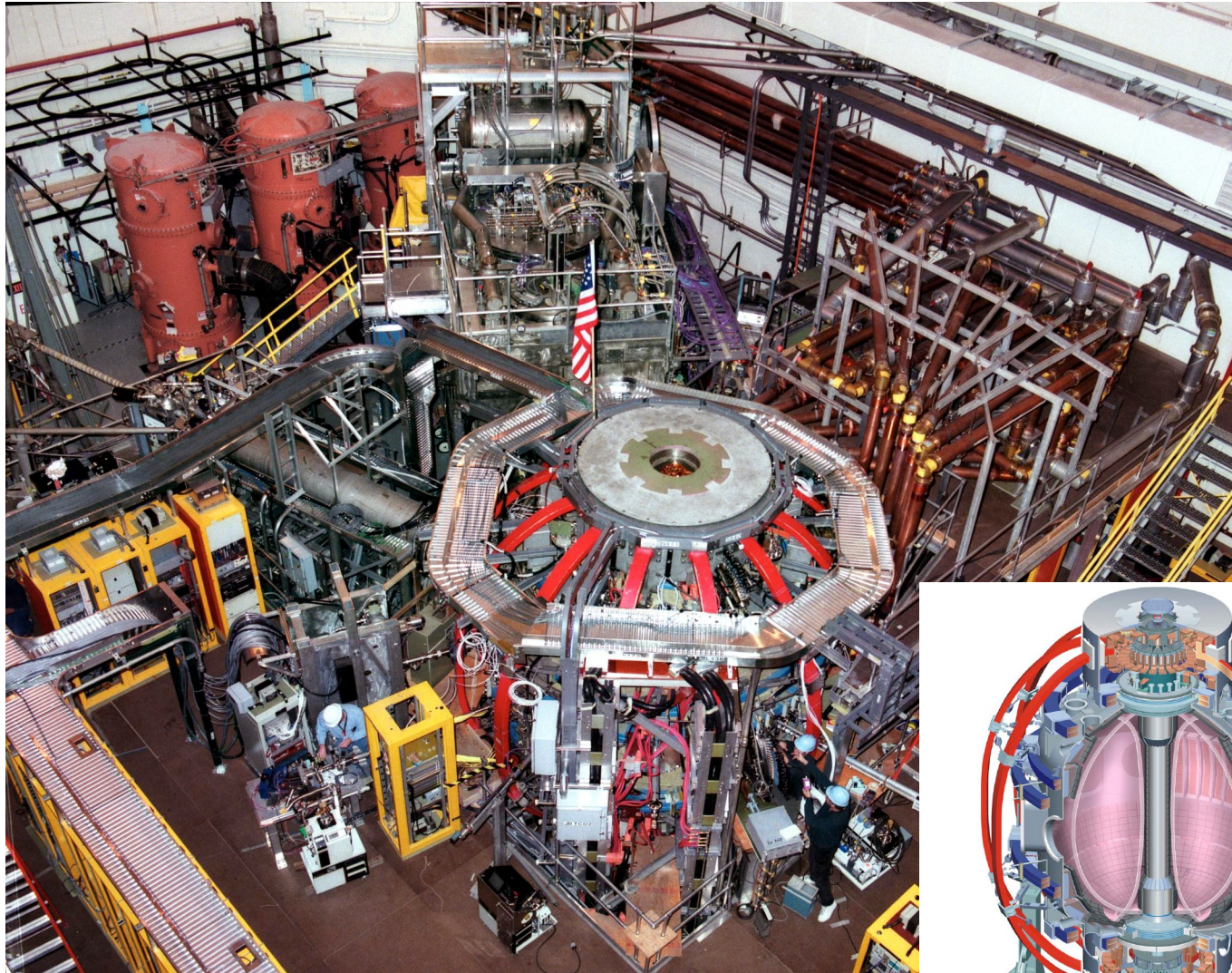
Passive Plates

RWM Coils

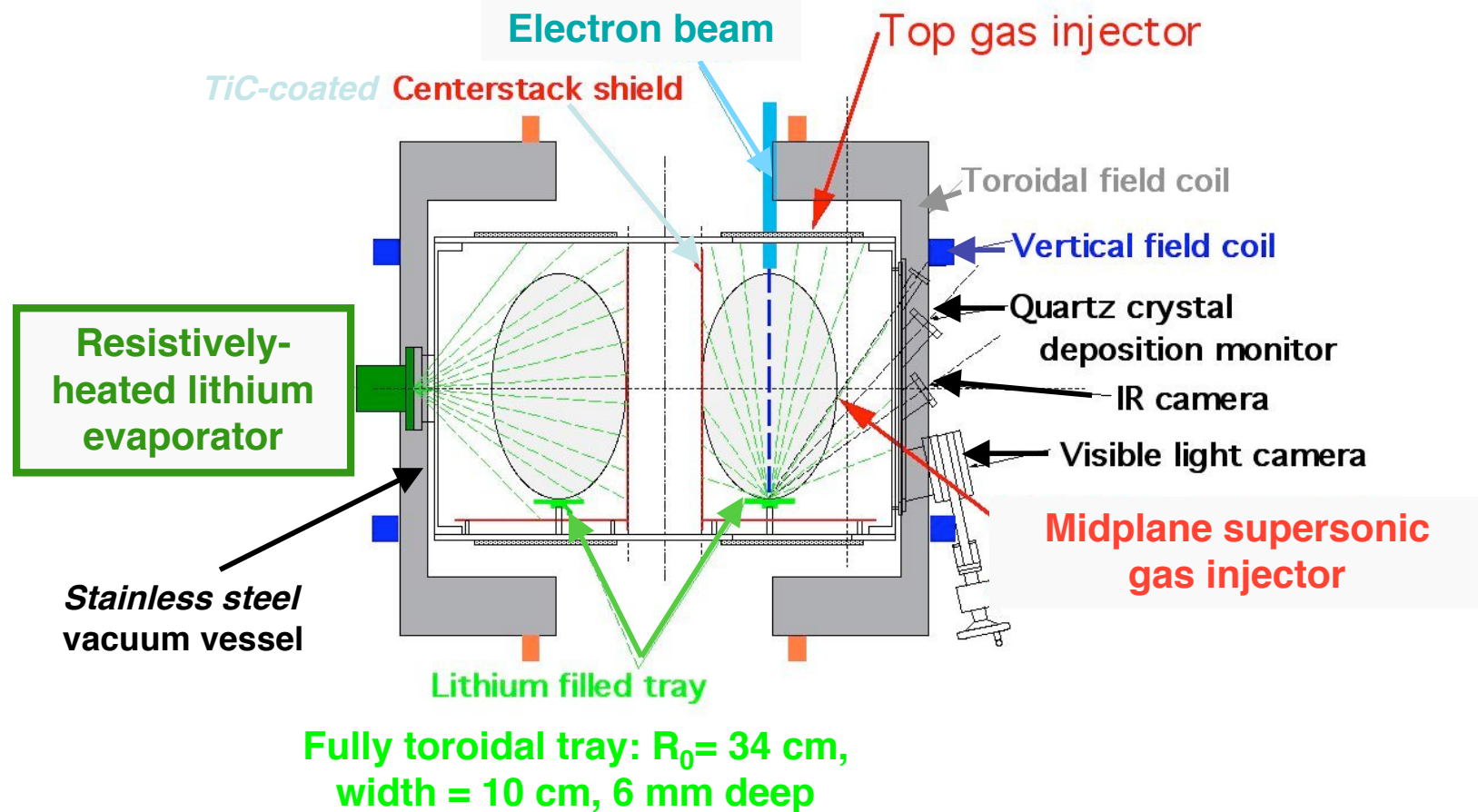
$I_{\text{CHI}} \sim 400 \text{ kA}$

60 cm dia. ports

Wide tang. access

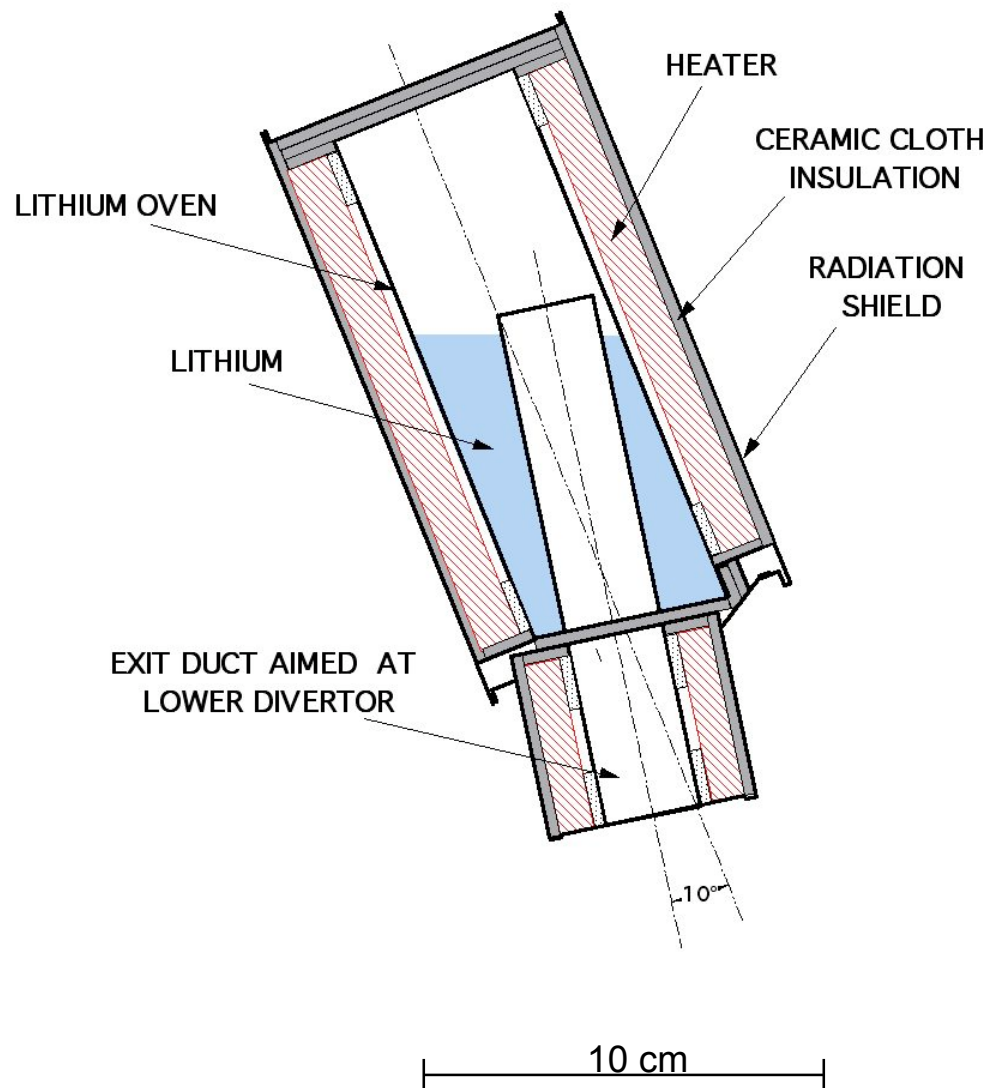


Lithium PFC research in NSTX begun with coatings prior to liquid surface implementation



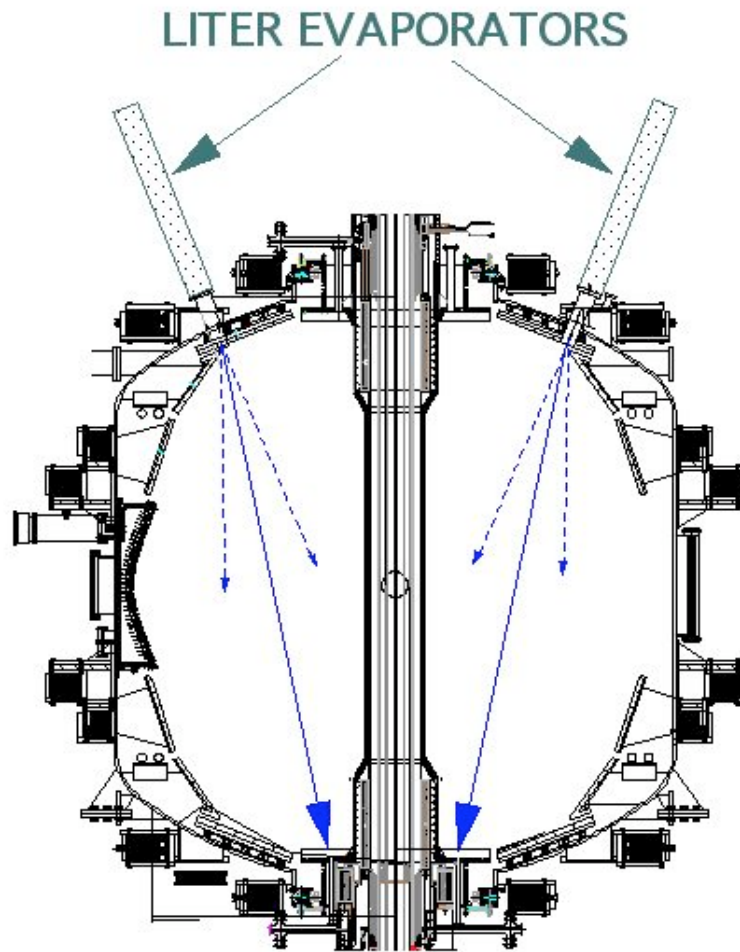
- Use evaporator similar to type developed on CDX-U

NSTX LITHium EvaporatoR (LITER) consists of heated reservoir inside stainless steel oven

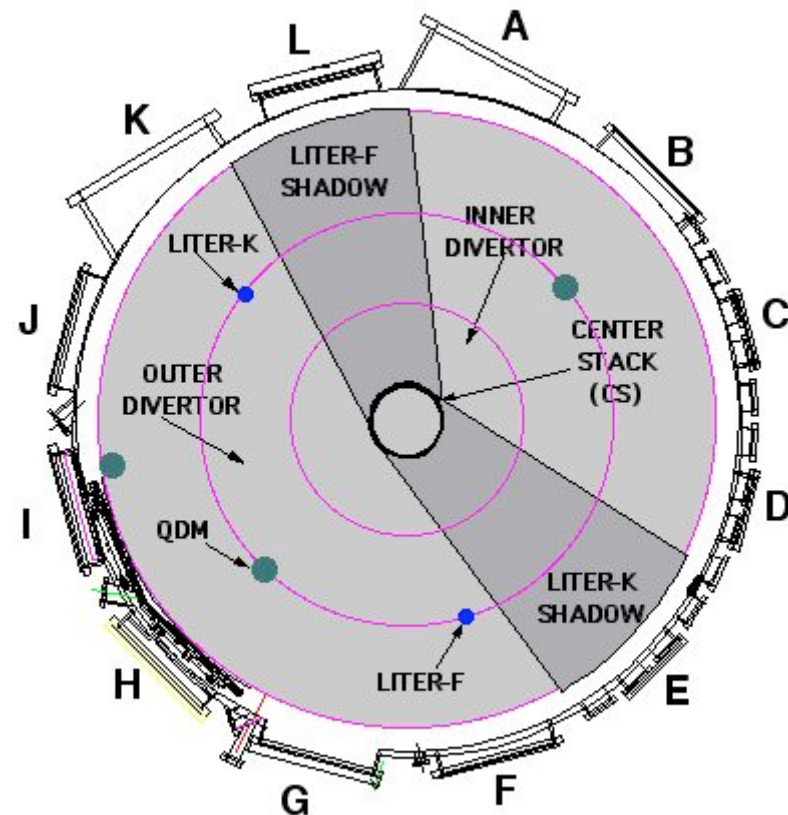


- Capacity: 90 g Li
- Oven Temp: 600-680°C
- Rate: 1mg/min - 80mg/min

Two LITERs oriented for coating NSTX divertor region with lithium



- LITER central aiming axis to graphite divertor and gaussian angle at $1/e$ (dashed)

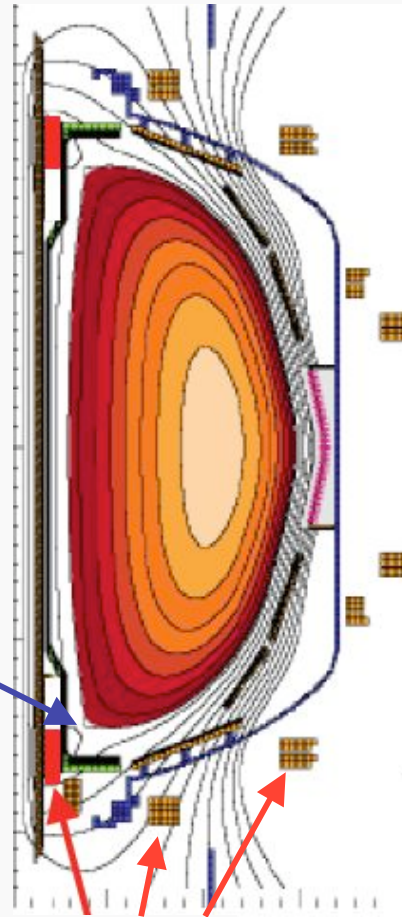


- Toroidal locations of LITER and Quartz Deposition Monitors (QDM)

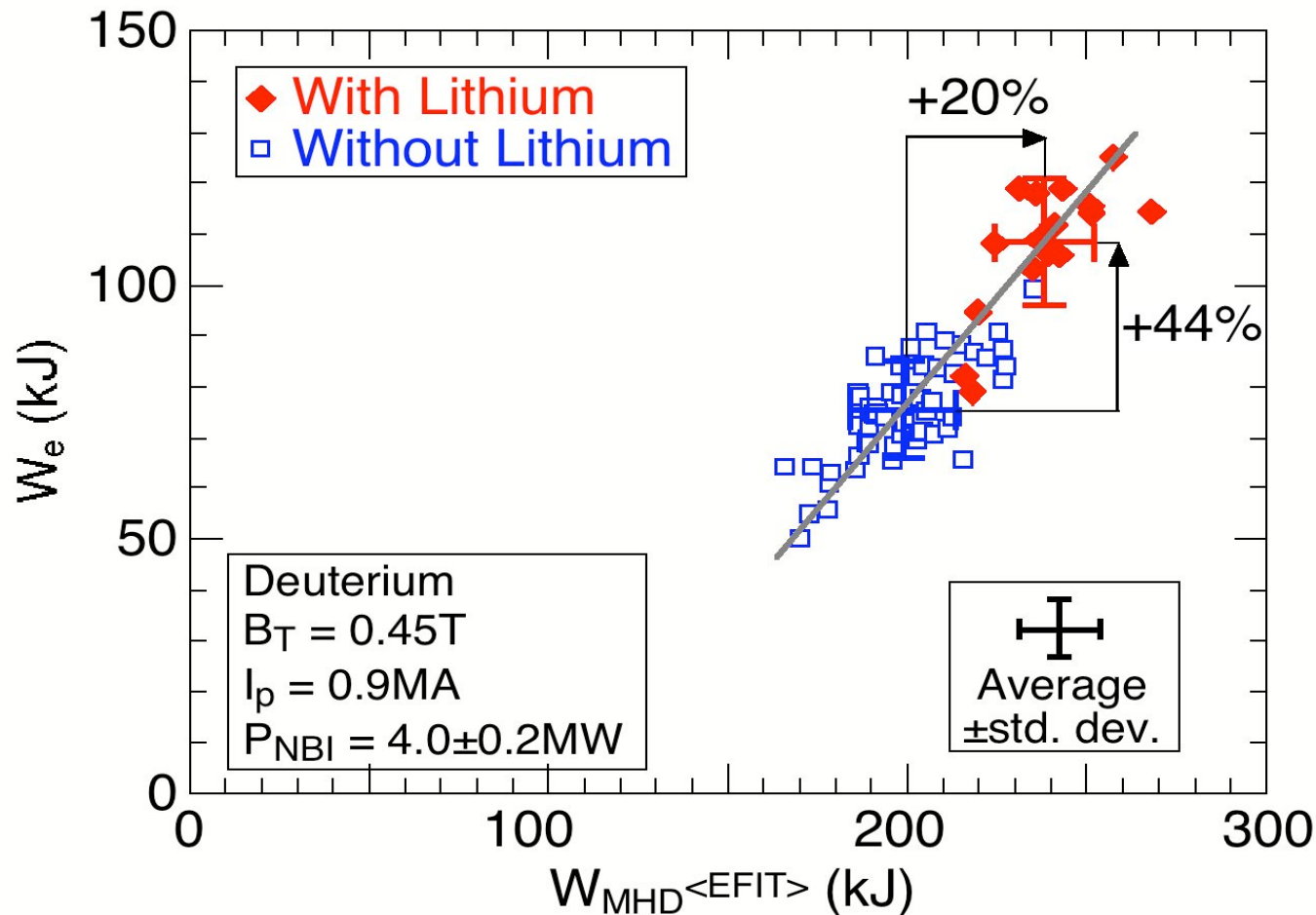
High recycling observed in NSTX divertor region

- Divertor region

- Poloidal field coils



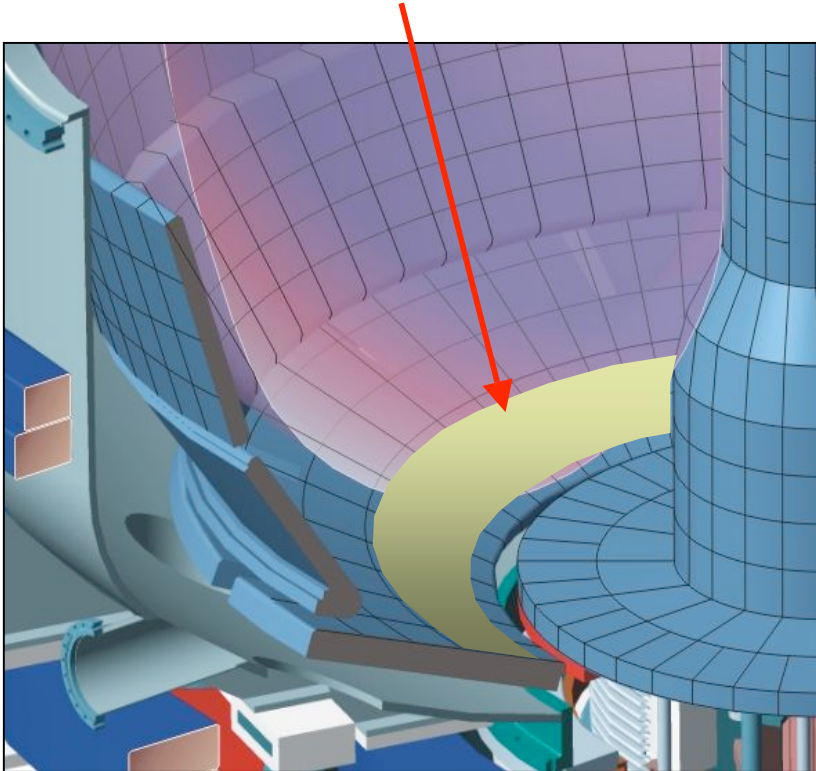
Lithium coatings improve plasma performance in NSTX



- Increase in total stored energy primarily attributable to rise in electron stored energy

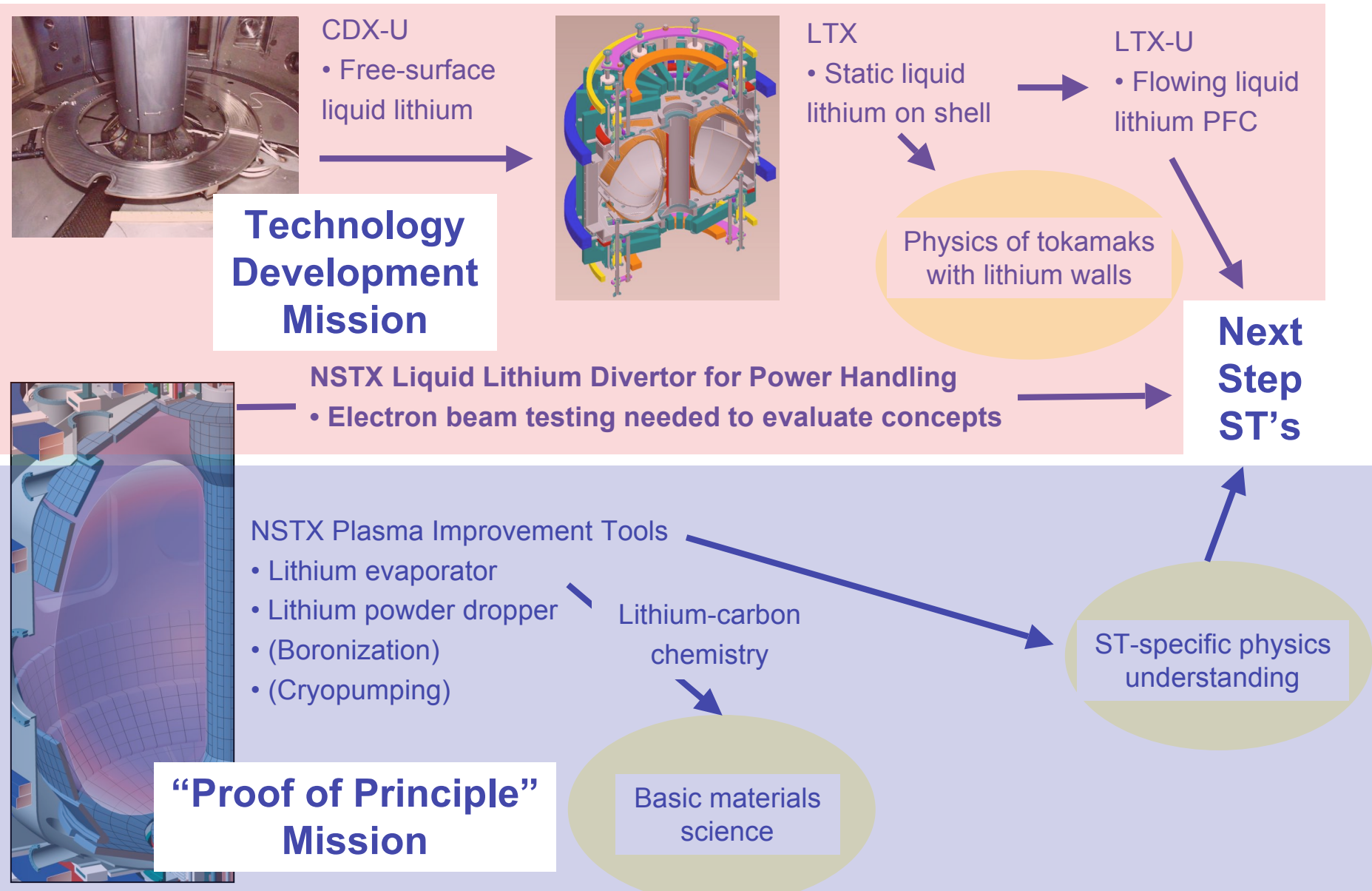
Next step is to replace section of divertor region with fully-toroidal liquid lithium surface

Liquid Lithium Divertor (LLD) to be installed on lower divertor in 2009



- Lithium in porous molybdenum surface to be kept liquid by heated copper substrate
- Objective is to determine if liquid lithium can sustain deuterium pumping beyond capability of solid lithium coatings

Lithium research at PPPL includes complementary technology and ST concept improvement missions



Contributors on LTX and Acknowledgements*

**L. Berzak 1), D. Boyle 1), R. Doerner 2), T. Gray 1), E. Granstedt 1),
C. Jacobson 1), T. Kozub 1), H. Kugel 1), B. LeBlanc 1), D. Lundberg 1),
T. Lynch 2), R. Maingi 3), R. Majeski 1), D. Mansfield 1), J. Spaleta 1),
V. Soukhanovskii 4), T. Strickler 1), J. Timberlake 1), J. Yoo 1), and
L. Zakharov 1)**

1) Princeton Plasma Physics Laboratory, Princeton, NJ 08543 USA

2) University of California at San Diego, La Jolla, CA 92093 USA

3) Oak Ridge National Laboratory, Oak Ridge, TN 37831 USA

4) Lawrence Livermore National Laboratory, Livermore, CA 94551 USA

***Work supported in part by US DOE Contracts DE-
AC02-76CH03073**

Contributors on NSTX and Acknowledgements*

H. Kugel 1), J-W. Ahn 2), J. P. Allain 7), M. G. Bell 1), R. Bell 1), J. Boedo 2), C. Bush 3), R. Ellis 1), D. Gates 1), S. Gerhardt 1) T. Gray 1), J. Kallman 1), S. Kaye 1), B. LeBlanc 1), R. Maingi 3), R. Majeski 1), D. Mansfield 1), J. Menard 1), D. Mueller 1), M. Ono 1), S. Paul 1), R. Raman 4), A. L. Roquemore 1), P. W. Ross 1), S. Sabbagh 5), H. Schneider 1), C. H. Skinner 1), V. Soukhanovskii 6), T. Stevenson 1), D. Stotler 1), J. Timberlake 1), W. R. Wampler 8), J. Wang 9), J. Wilgen 3), and L. Zakharov 1)

1) Princeton Plasma Physics Laboratory, Princeton, NJ 08543 USA

2) University of California at San Diego, La Jolla, CA 92093 USA

3) Oak Ridge National Laboratory, Oak Ridge, TN 37831 USA

4) University of Washington, Seattle, WA 98195 USA

5) Columbia University, New York, NY 10027 USA

6) Lawrence Livermore National Laboratory, Livermore, CA 94551 USA

7) Purdue University, School of Nuclear Engineering, West Lafayette, IN 47907 USA

8) Sandia National Laboratories, Albuquerque, NM 87185 USA

9) Los Alamos National Laboratory, Los Alamos, NM 97545 USA

***Work supported in part by US DOE Contracts DE-AC02-76CH03073, DE-AC04-94AL85000, DE-AC52-07NA27344, and DE-AC05-00OR22725**