

The future of water purification by electrical discharge plasmas

Selma Mededovic Thagard

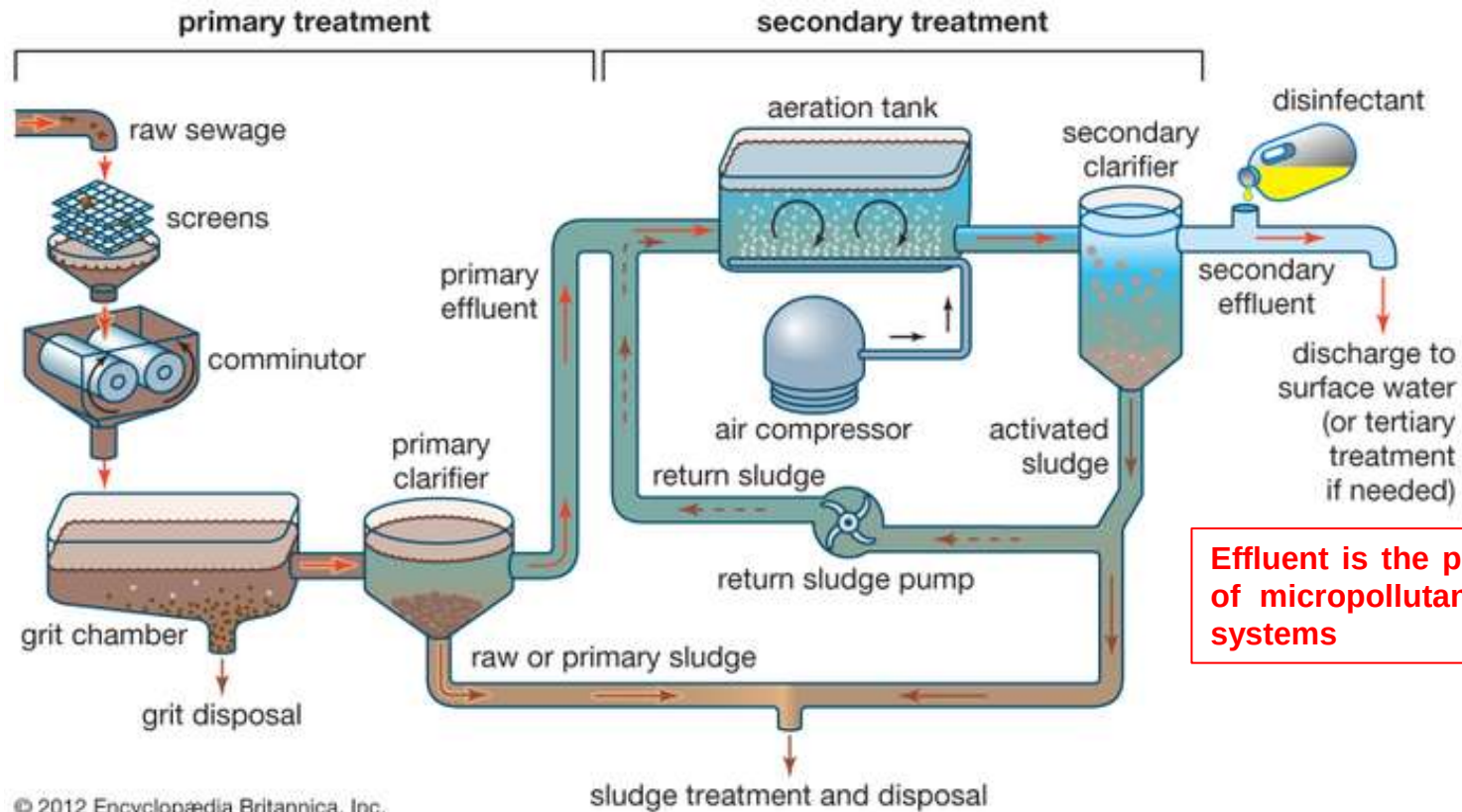
Department of Chemical and Biomolecular Engineering

Clarkson University

Potsdam, NY, United States



Conventional large scale wastewater treatment



- Capacities range between 1 and 100+ million gallon per day

The problem

- Ineffective removal of micropollutants

Solutions:

- Prevention by application of products without micropollutants or only with micropollutants which are easily removed

Near impossible

- Reassessment and optimization of current treatment processes

Economically feasible but ineffective towards persistent micropollutants. The removal of those requires additional secondary or tertiary treatment steps.

- Pretreatment of hospital and industrial effluents

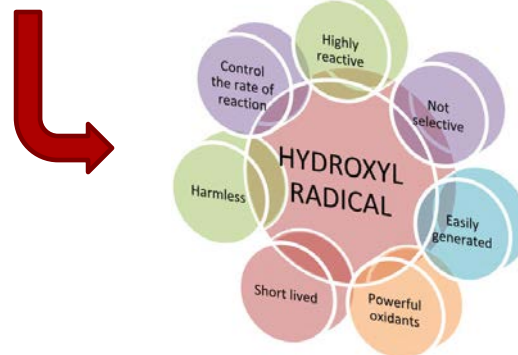
A range of destructive and non-destructive techniques has been investigated.

Existing and emerging water treatment technologies

- **Non-destructive technologies** (membrane filtration, ultraviolet irradiation, biological filtration, and ion exchange)
- **Destructive technologies** (Advanced Oxidation Processes-AOPs)

Oxidation potential (V)

Oxygen (O ₂)	1.23
Hydroperoxyl radical (HO ₂ ·)	1.44
Hydrogen peroxide (H ₂ O ₂)	1.78
Ozone (O ₃)	2.07
Atomic oxygen (O)	2.43
Sulfate radical anion (SO ₄ · ⁻)	2.50
OH Radicals (OH·)	2.80
Fluorine (F ₂)	2.87



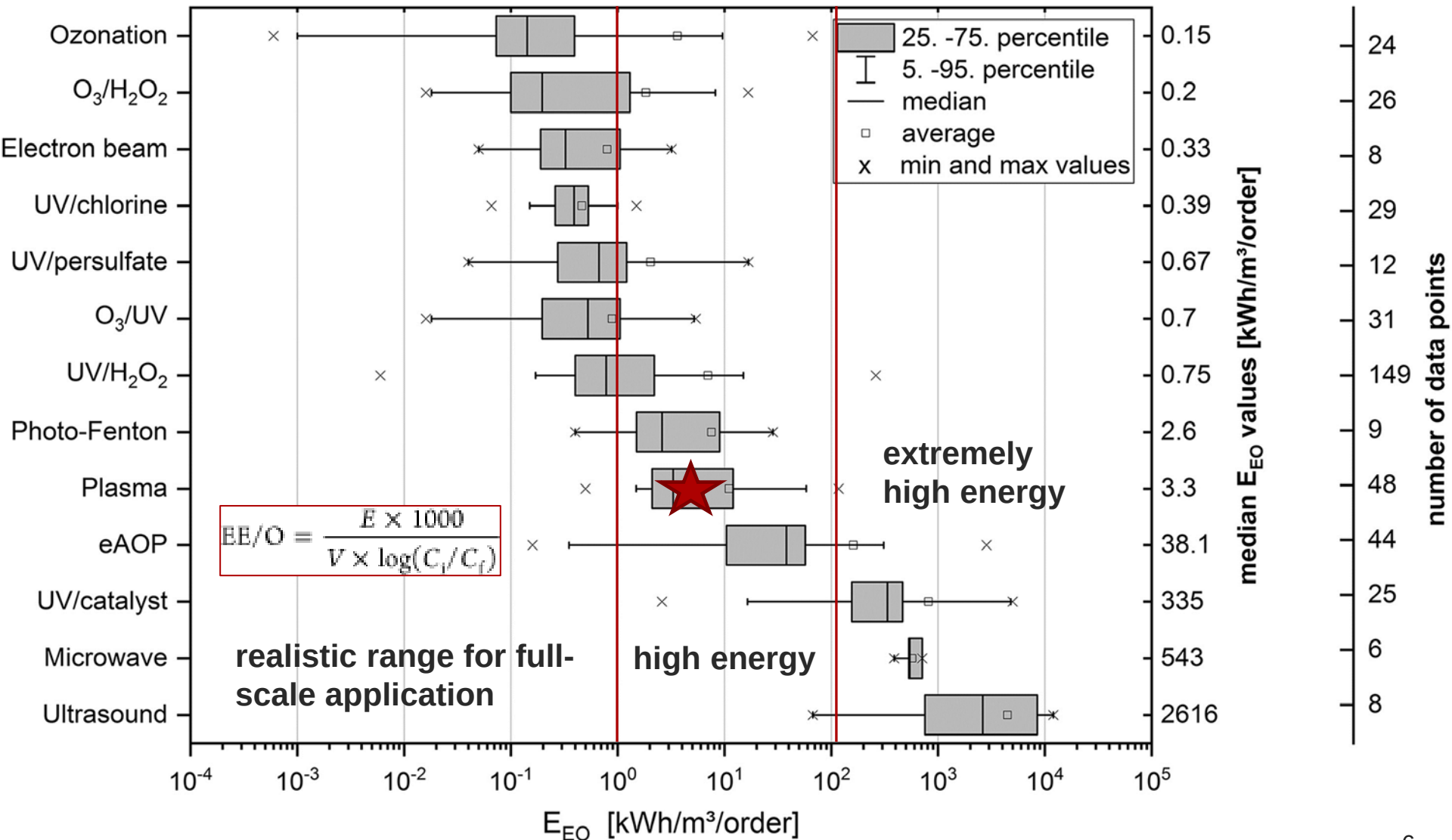
- Pharmaceuticals
- Industrial Chemicals
- Toxic Compounds
- Pesticides
- Personal Care Products
- Endocrine Disrupting Compounds

Ultimately, the optimal water treatment technology achieves regulatory effluent limitations at a reasonable cost.

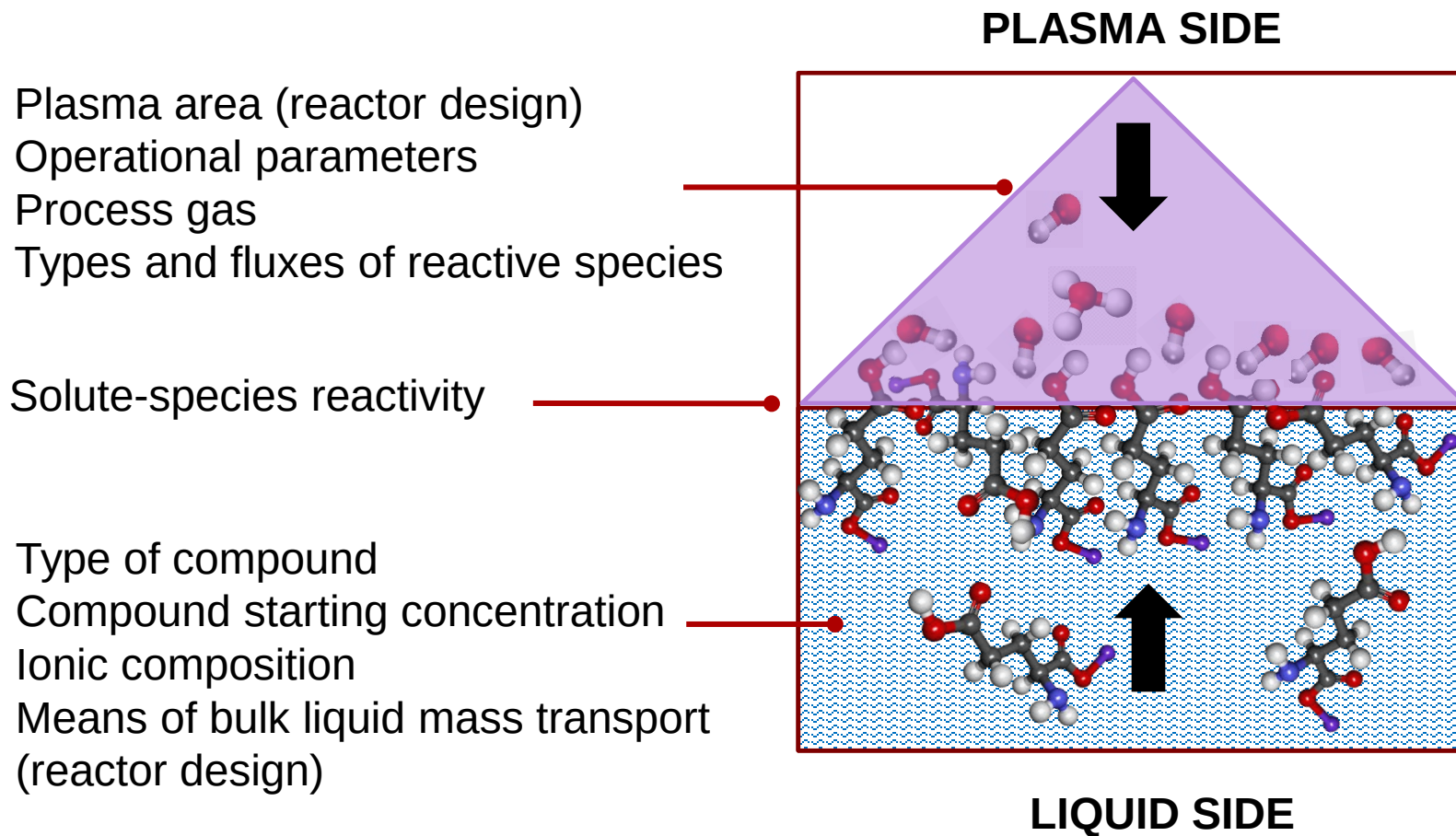
Electrical discharge plasma for water treatment

- Wide variety of reactive oxidative species (OH, H₂O₂, O₃).
 - *Also present for other AOPs*
- Existence of reactive reductive species (e.g., e_{aq}⁻) and ions.
 - *Specific to plasma treatment and advantageous*
- Highly non-selective process.
 - *As is every other AOP*
- Physical effects such as generation of ultraviolet-range radiation (UV), shockwaves capable of inducing cavitation, and in some cases high temperatures capable of thermally decomposing molecules.
 - *No experimental evidence that these processes aid treatment*
- No chemical additives are required.
 - *Many other AOPs also do not require chemicals*

Plasma-based water treatment: comparison with a range of AOPs



The problem (and the solution) is the heterogeneous nature of the plasma

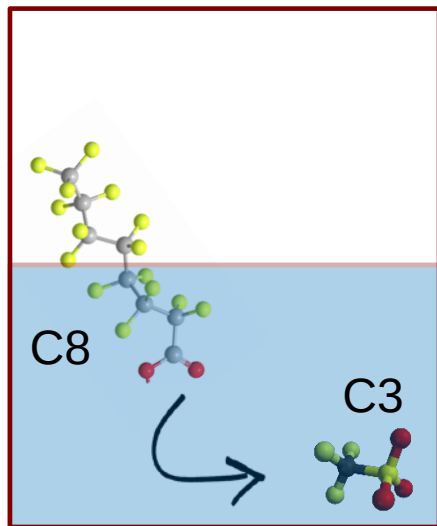


Objective: effectively utilize plasma-generated species by concentrating the contaminants at the plasma-liquid interface over a large surface area.

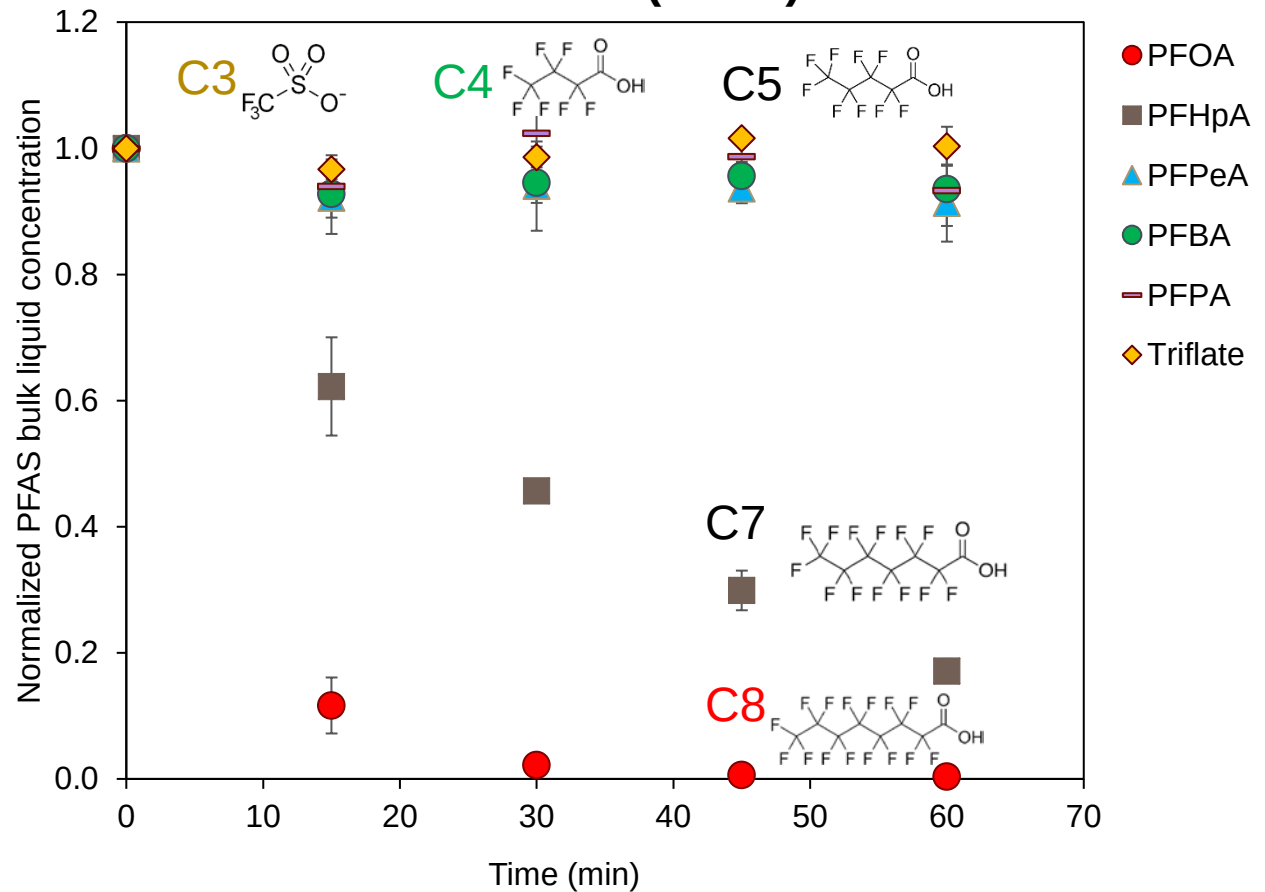
How do properties of compounds effect plasma reactor performance?



Point-ring reactor
with argon
bubbling

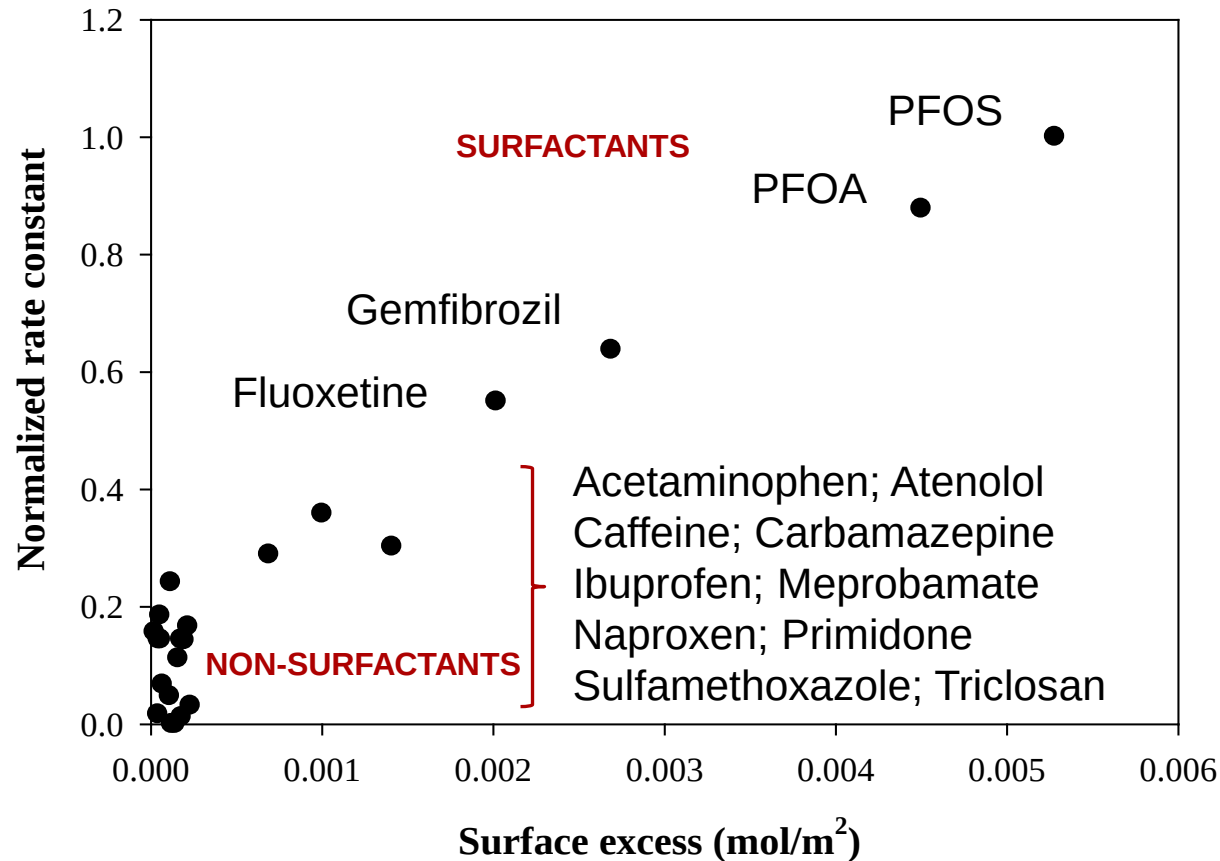


Degradation of Poly- and Perfluoroalkyl substances (PFAS)



Surfactant-like compounds exhibit a strong tendency for the plasma-liquid interface and are rapidly degraded.

Plasma reactor performance is closely tied to interfacial compound concentration



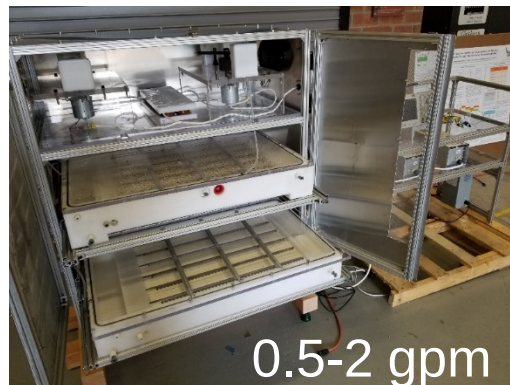
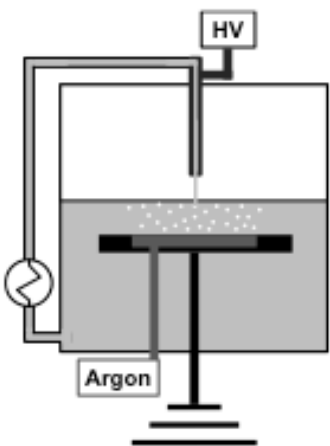
Our current plasma reactor design(s) are superior for the treatment of surfactants (PFAS and dyes) but are unable to competitively treat non-surfactants.

PFOA **PFOS**

- Sources: military training activities (flame retardants) and manufacturing (non-stick cookware, water resistant clothing, fast food wrappers).
- EPA's health advisory level for PFOA+PFOS in drinking water is at 70 ng/L.
- \$12B market
- Plasma is **the most promising treatment technology for the destruction of these compounds.**



Plasma reactor scaleup for PFAS degradation



The key reactor design elements:

BULK LIQUID MASS TRANSPORT – Bubbling using argon is very effective and the gas can be recycled.

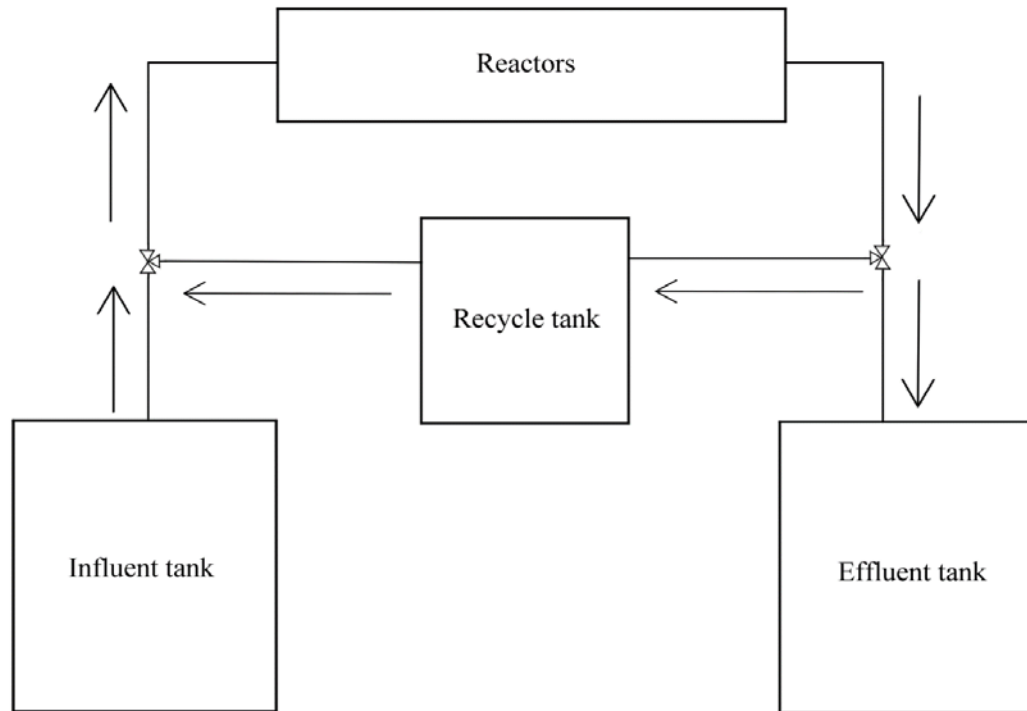
PLASMA AREA – Plasma-generated species must contact the entirety of the gas-liquid interface to maximize the treatment efficacy.

Plasma reactor field demonstration

- ~ 2 years effort
- Mobile skid layout, electrical drawings and process flow diagrams
- Trailer integrated system testing at Clarkson before the field demonstration using a generator
- Installation of grounding rods
- Electromagnetic interference testing of plasma reactors
- Equipment and safety training courses
- Development of operation and maintenance manuals
- Base permits, water discharge permits...
- 100s of gallons of water successfully treated over a two-week period at various flowrates up to 2 gpm

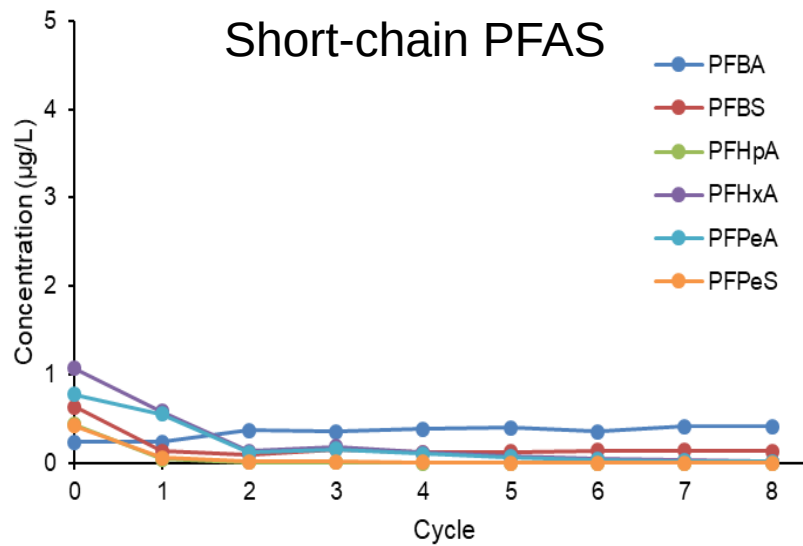
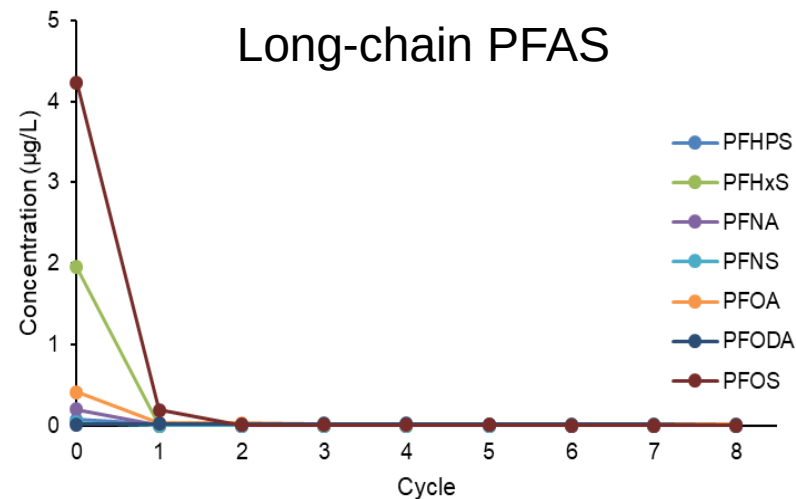
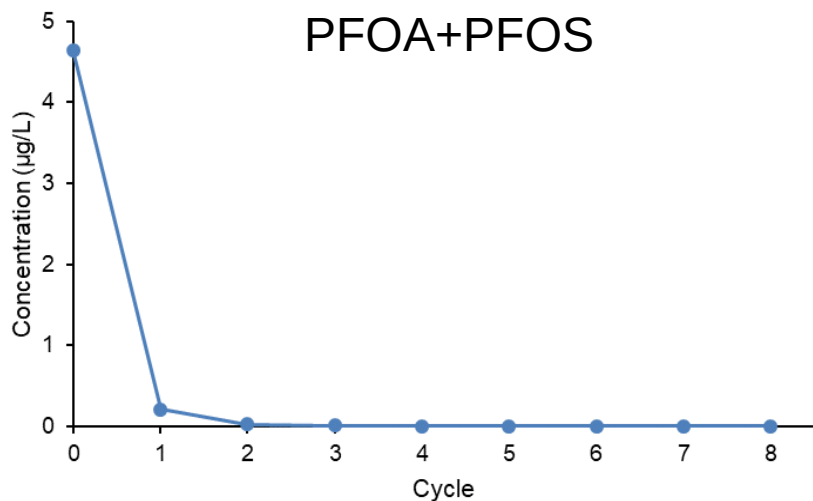


Plasma reactor field demonstration

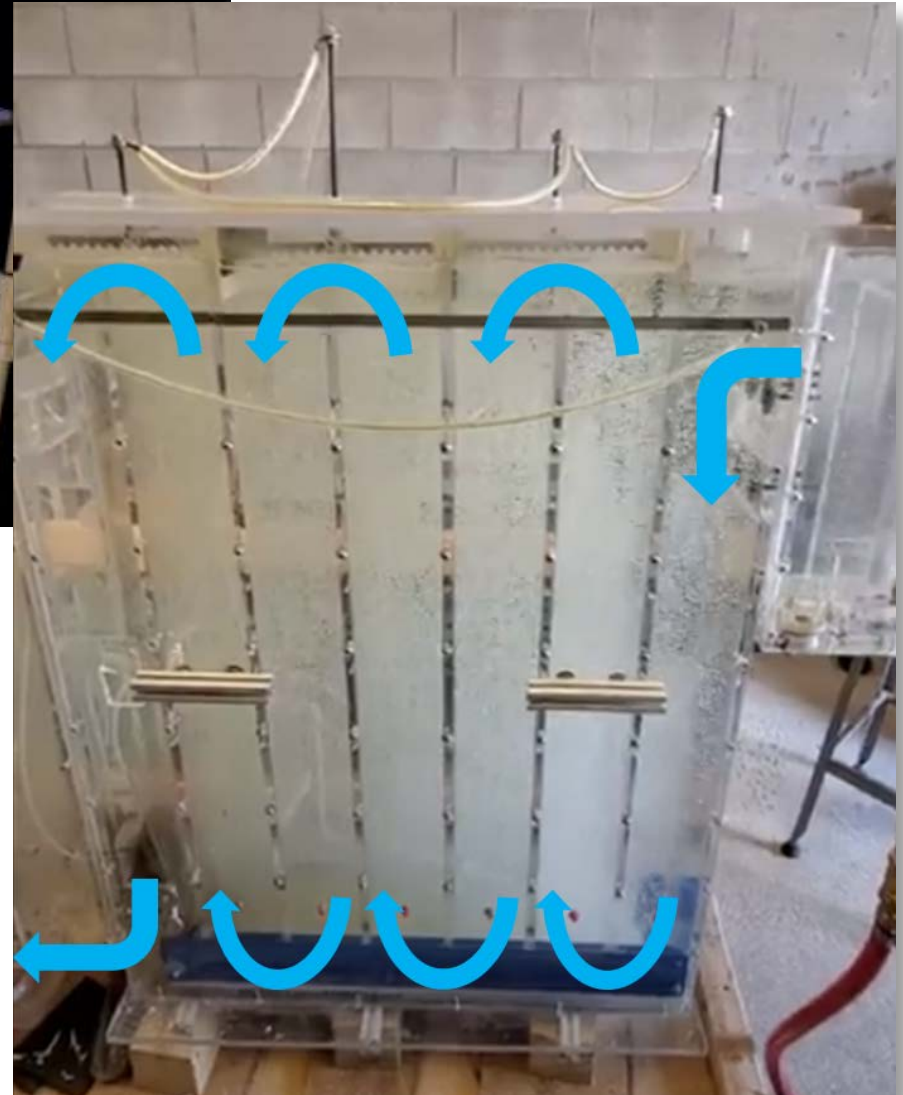


One cycle (18 gallon of water) is defined as a single pass through the reactor from the influent tank.

Field treatment results at 1.5 GPM



System throughput increase: 10 gpm



The performance of the 10 gpm system supersedes that of the 2 gpm system due to bulk liquid transport optimization.

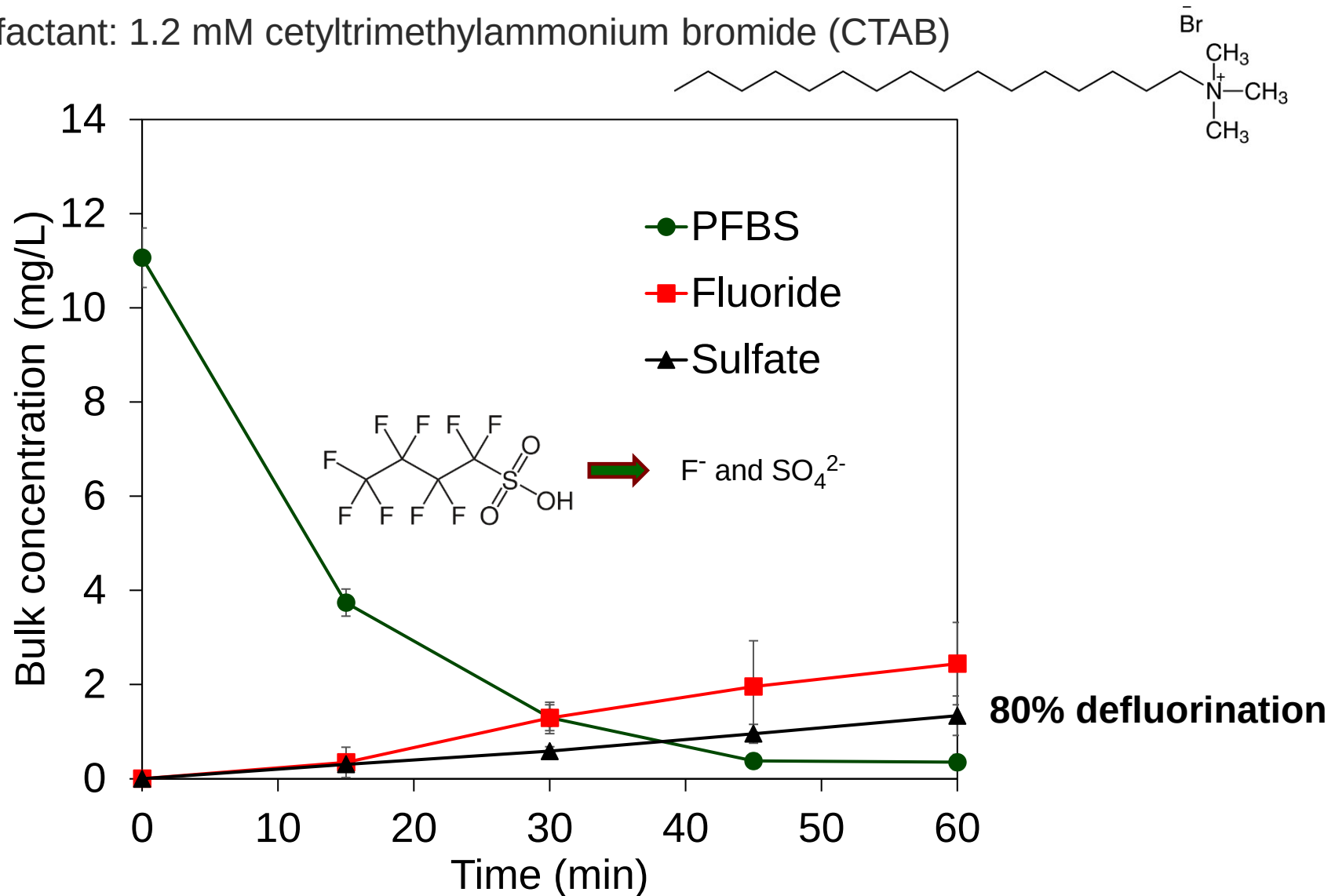
Degradation of PFBS (perfluorobutane sulfonate) by a point-ring plasma reactor



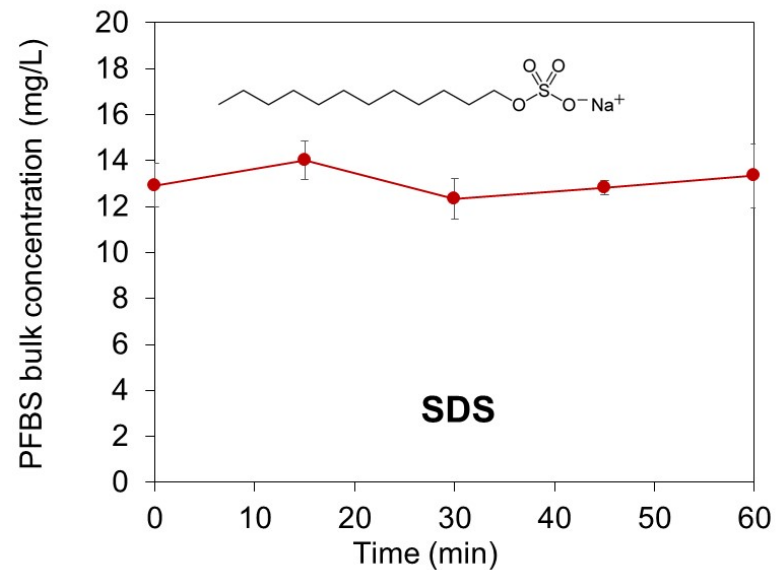
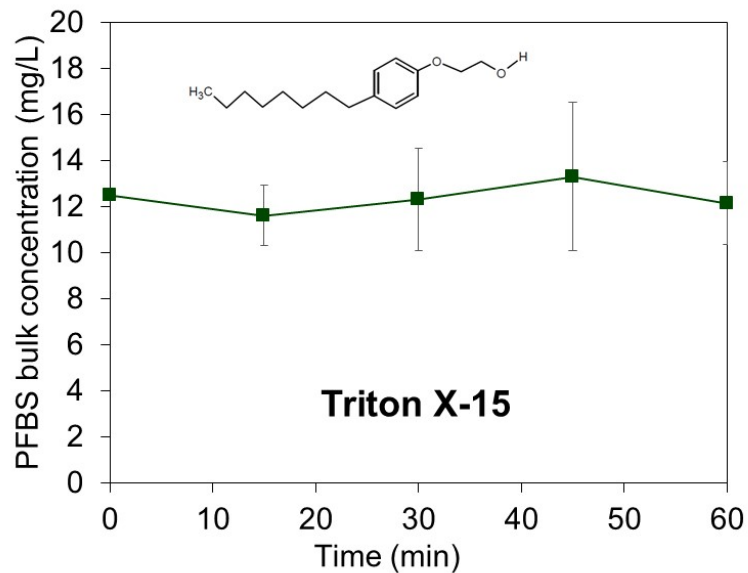
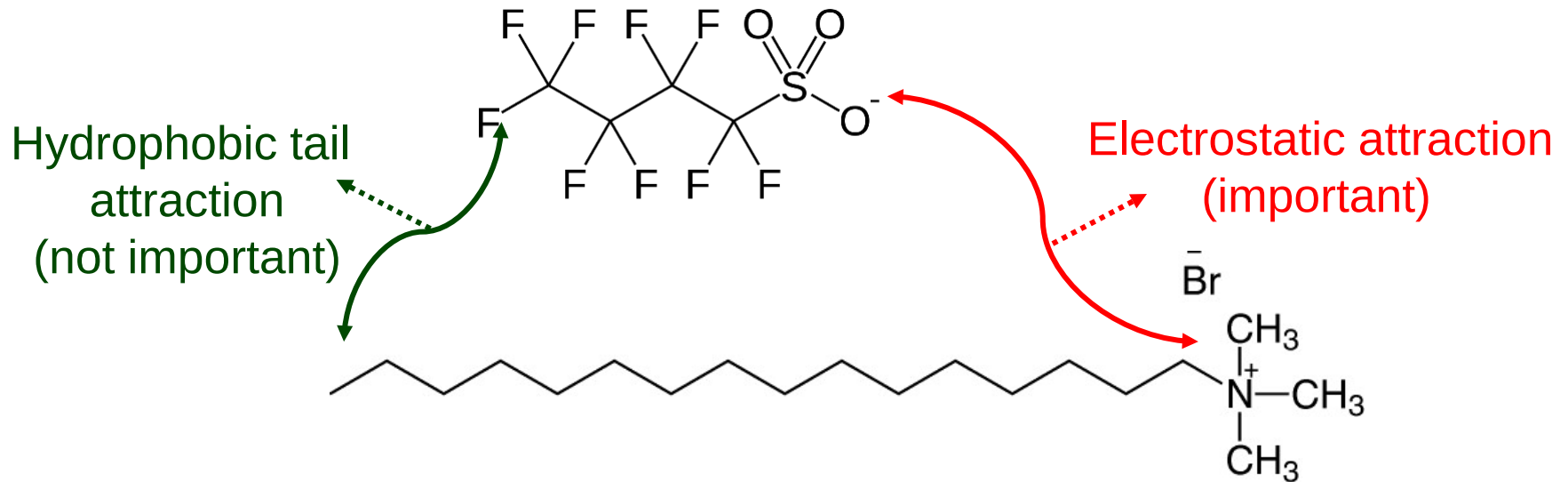
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- The graph displays the change in PFBS bulk concentration over time. The y-axis represents PFBS bulk concentration in mg/L, ranging from 0 to 18. The x-axis represents time in minutes, ranging from 0 to 60. A green line connects the data points, which show a slight decrease in concentration over time. Vertical error bars are present for the data points at 15, 30, 45, and 60 minutes.
- | Time (min) | PFBS bulk concentration (mg/L) |
|------------|--------------------------------|
| 0 | ~14.8 |
| 15 | ~12.7 ± 2.5 |
| 30 | ~12.3 ± 1.5 |
| 45 | ~12.1 ± 1.2 |
| 60 | ~12.0 |
- Chemical structure of PFBS (Perfluorobutanesulfonic acid) is shown below the graph:
- FSC(F)(F)C(F)(F)C(F)(F)S(=O)(=O)O

Minimizing bulk liquid mass transport limitations increases the removal rate of PFBS

Surfactant: 1.2 mM cetyltrimethylammonium bromide (CTAB)

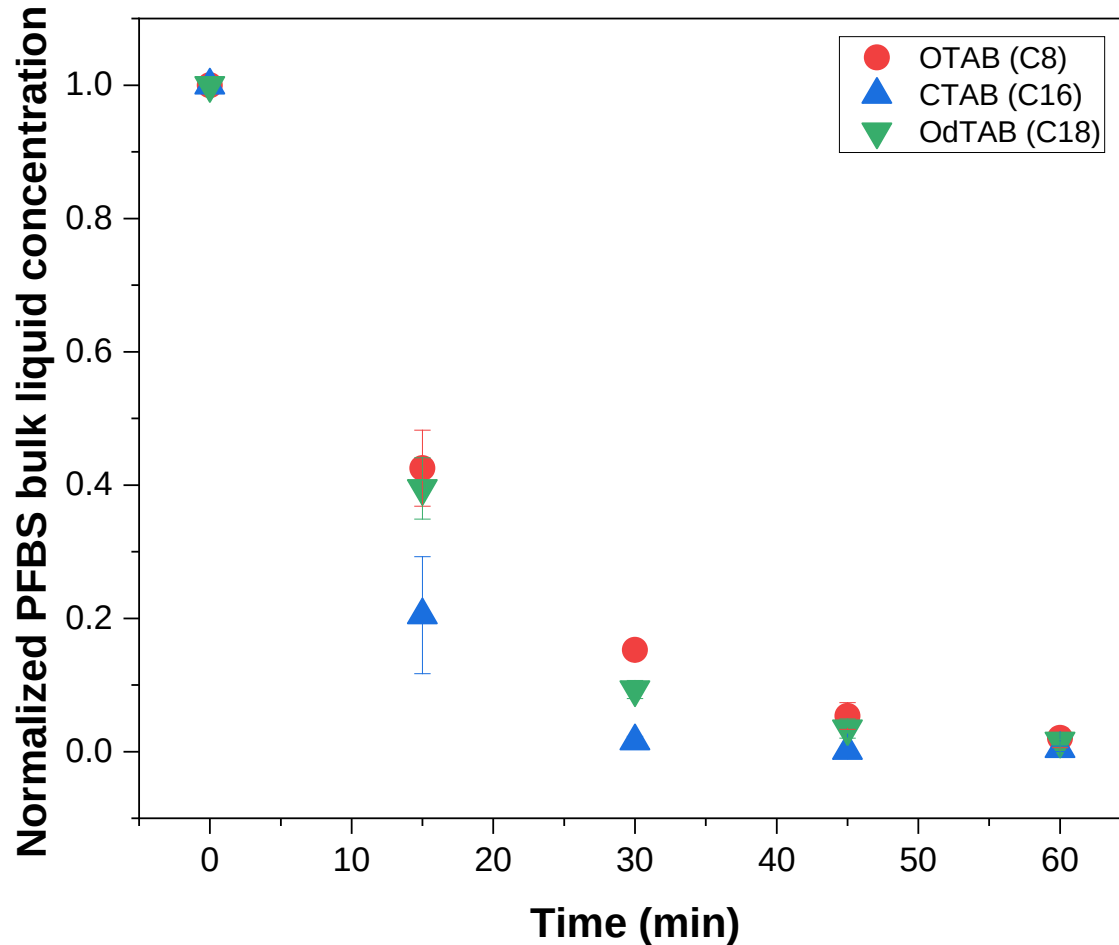


PFBS-CTAB interaction



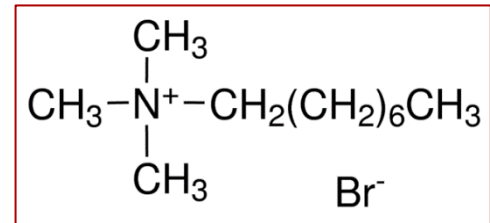
PFBS at the interface

Surfactant (0.2 mM) added every 15 mins

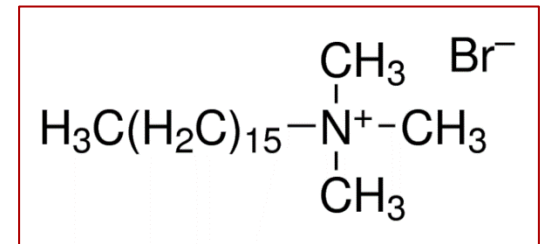


The mechanism of degradation (defluorination) is unknown.

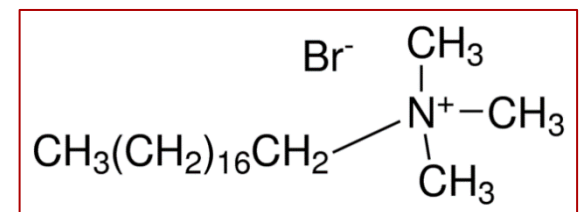
Octyltrimethylammonium bromide (C₈ - OTAB)



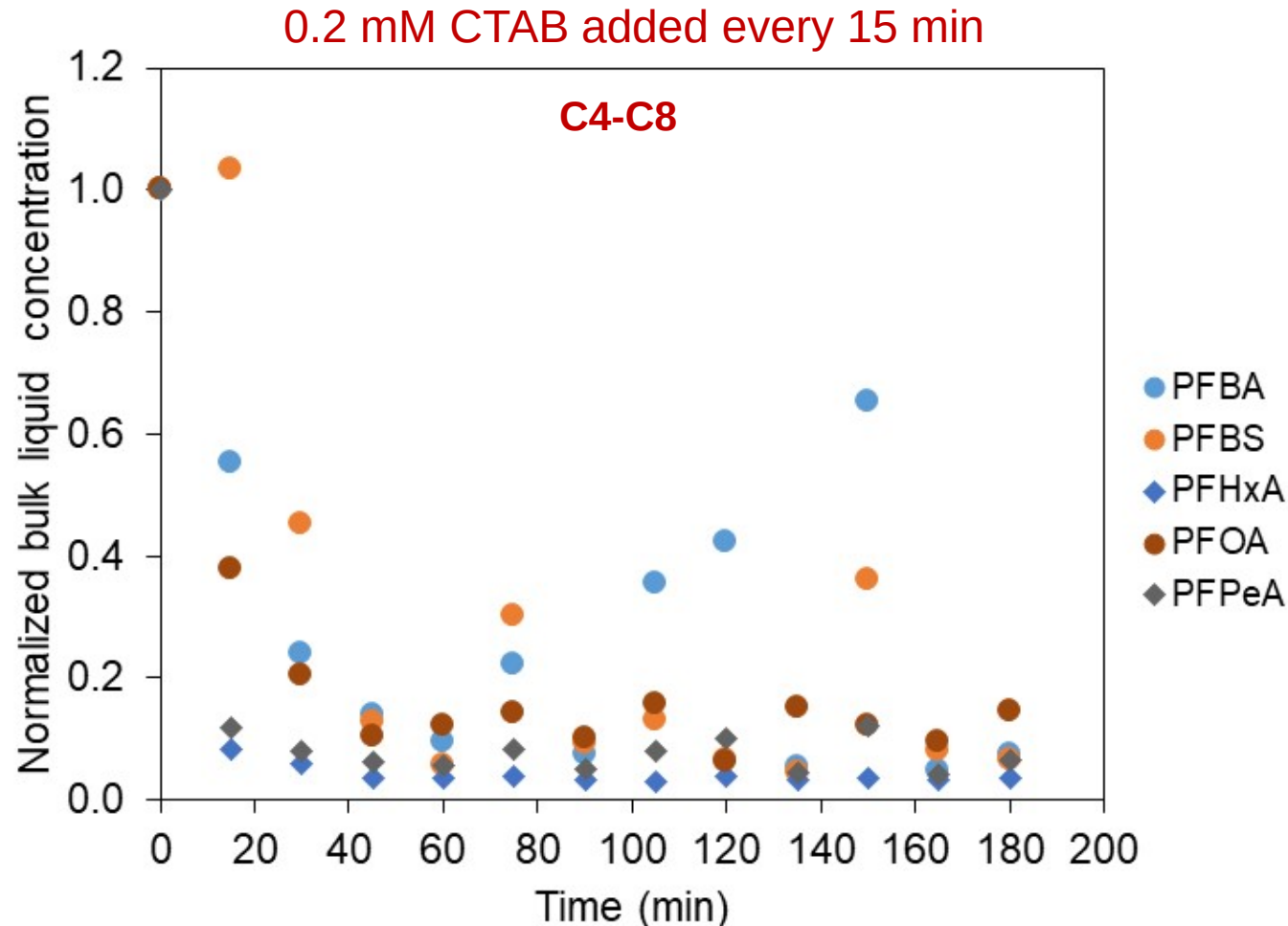
Hexadecyltrimethylammonium bromide (C₁₆ - CTAB)



Trimethyloctadecylammonium bromide (C₁₈ - OdTAB)



FAB wastewater reverse osmosis PFAS concentrate treatment in the presence of CTAB



- > 97% degradation of C4-C8 compounds
- C9-C16 compounds removed to below detection limits
- ~70% defluorination

Plasma treatment of Ion Exchange (IX) brine

Mobile plasma IX brine treatment system

- **Regenerant brine:** complex and highly concentrated mixture of PFAS, methanol (between 5% and 20%), NaCl (6-7%), and a range of co-contaminants.
- Solution electrical conductivity ~60 mS/cm.

High PFAS
concentration plasma
reactor
(~100 mg/L), 35 gal

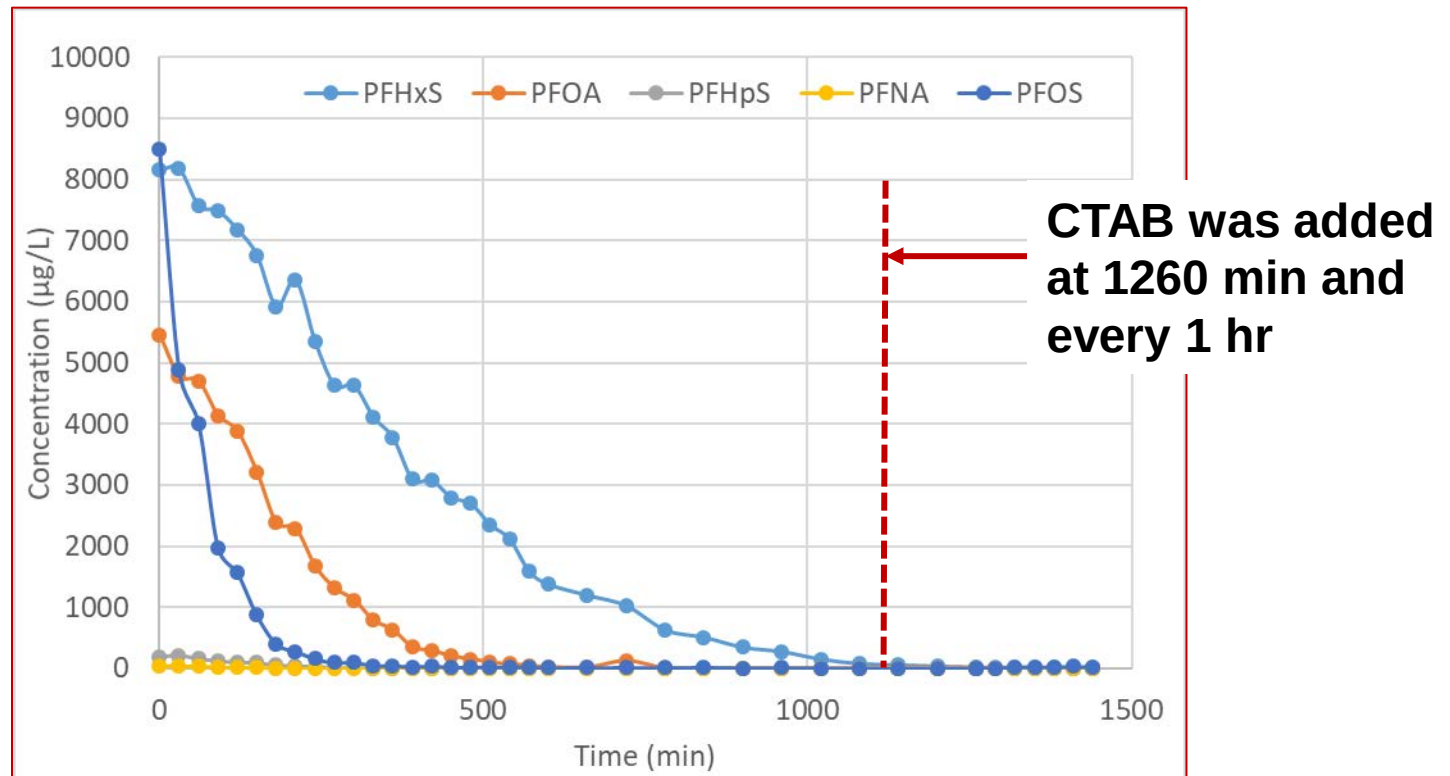


Low PFAS
concentration plasma
reactor
(~1 µg/L), 35 gal



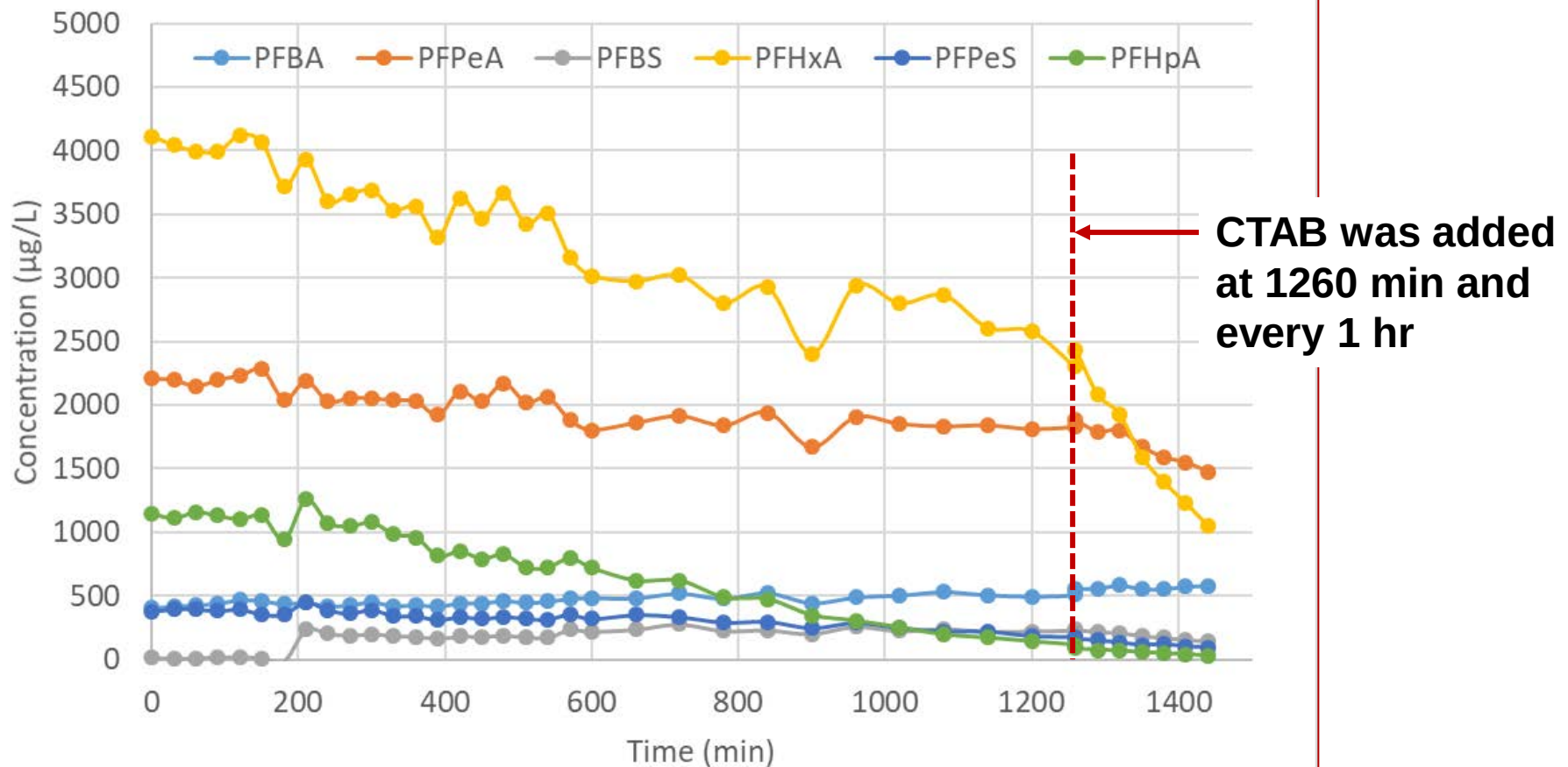
PFAS removal in high concentration plasma reactor

Long-chain PFAS



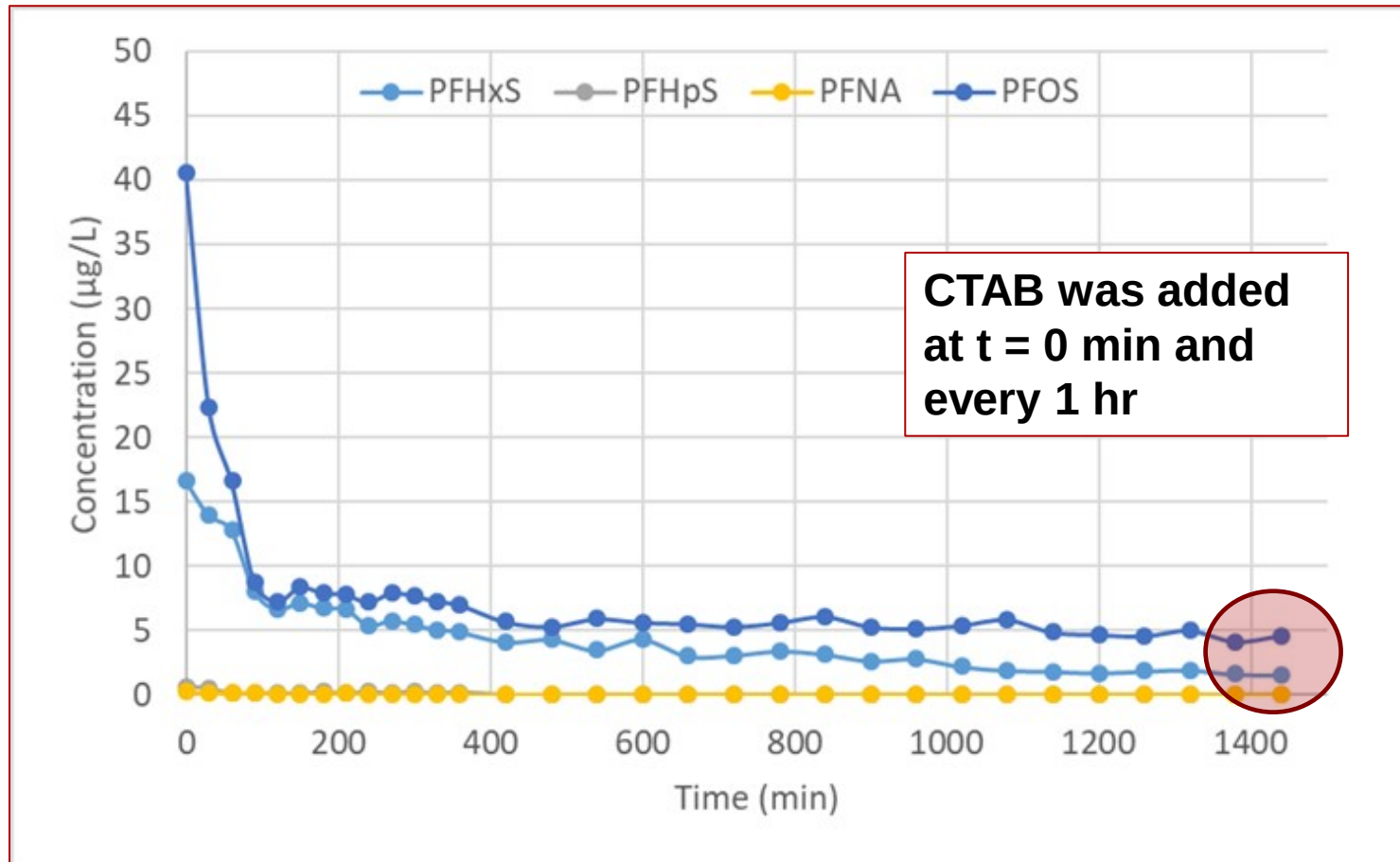
PFAS removal in high concentration plasma reactor

Short-chain PFAS



PFAS removal in low concentration plasma reactor

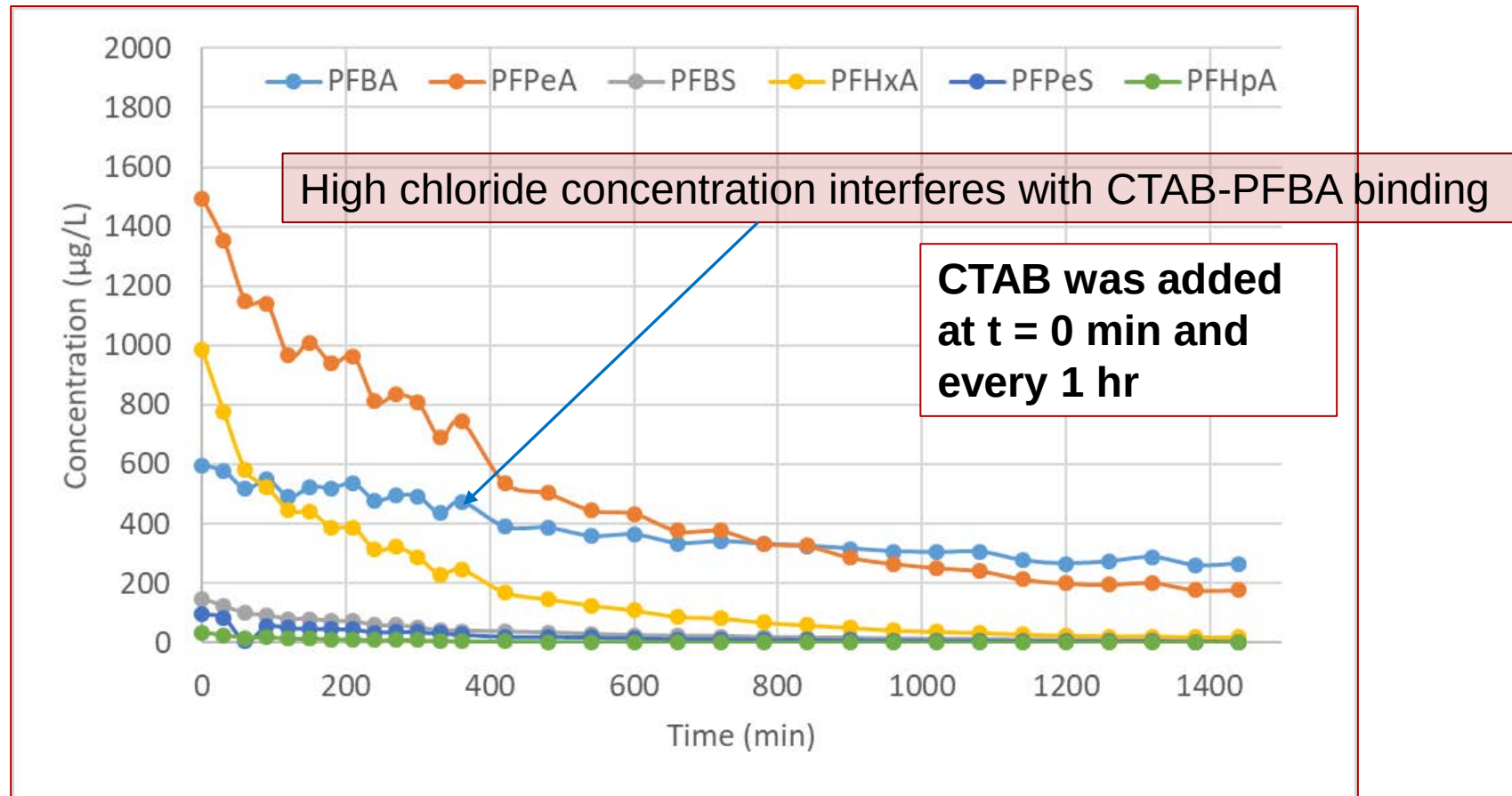
Long-chain PFAS



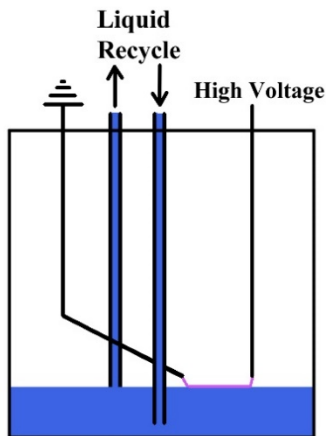
PFAS adsorption-desorption

PFAS removal in low concentration plasma reactor

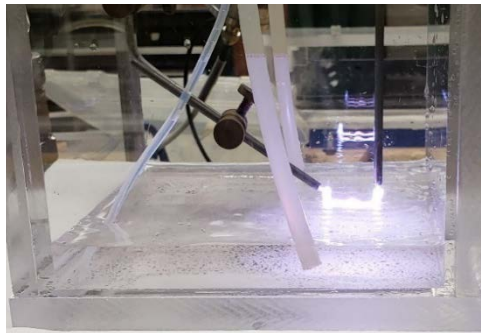
Short-chain PFAS



Inorganic salt effects in highly electrically conductive solutions

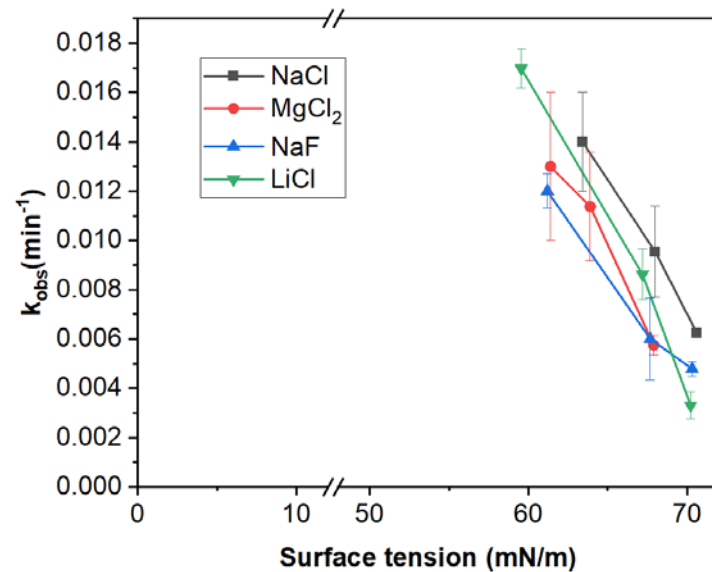
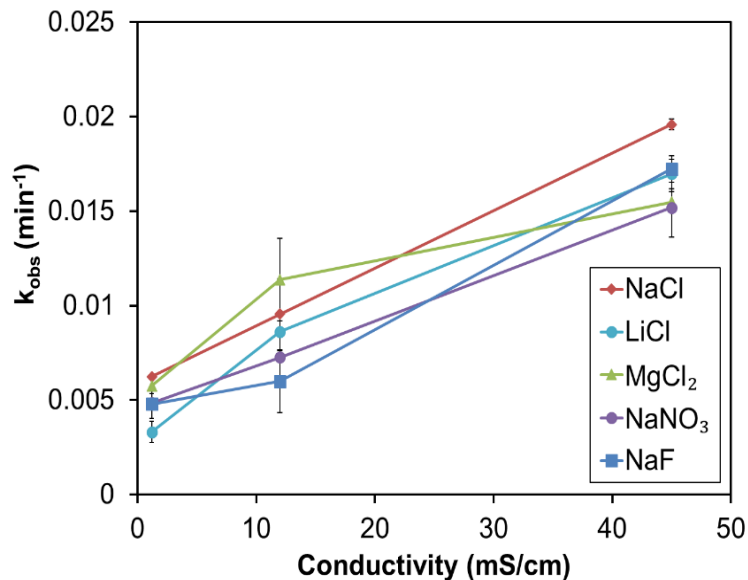


Constant plasma area

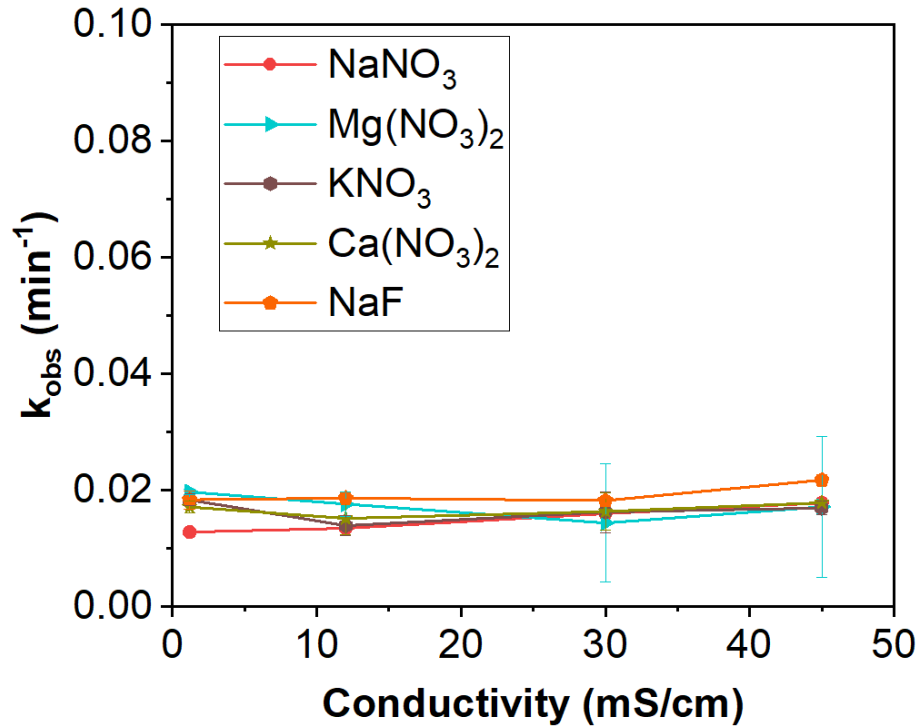


Removal of PFOA and Rhodamine B investigated as a function of solution conductivity up to 45 mS/cm

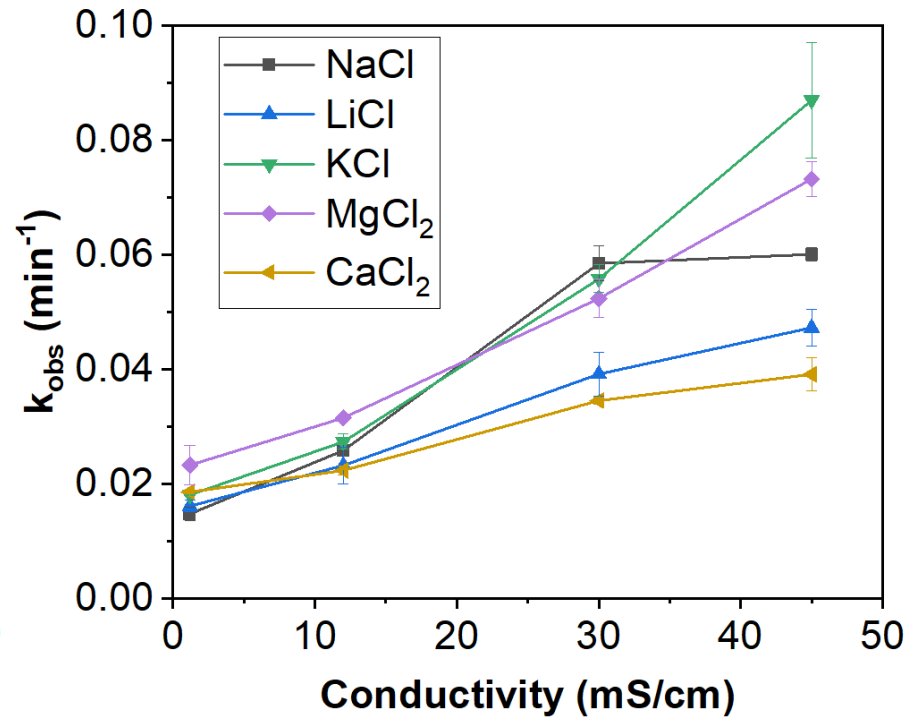
Degradation of PFOA



Rhodamine B degradation

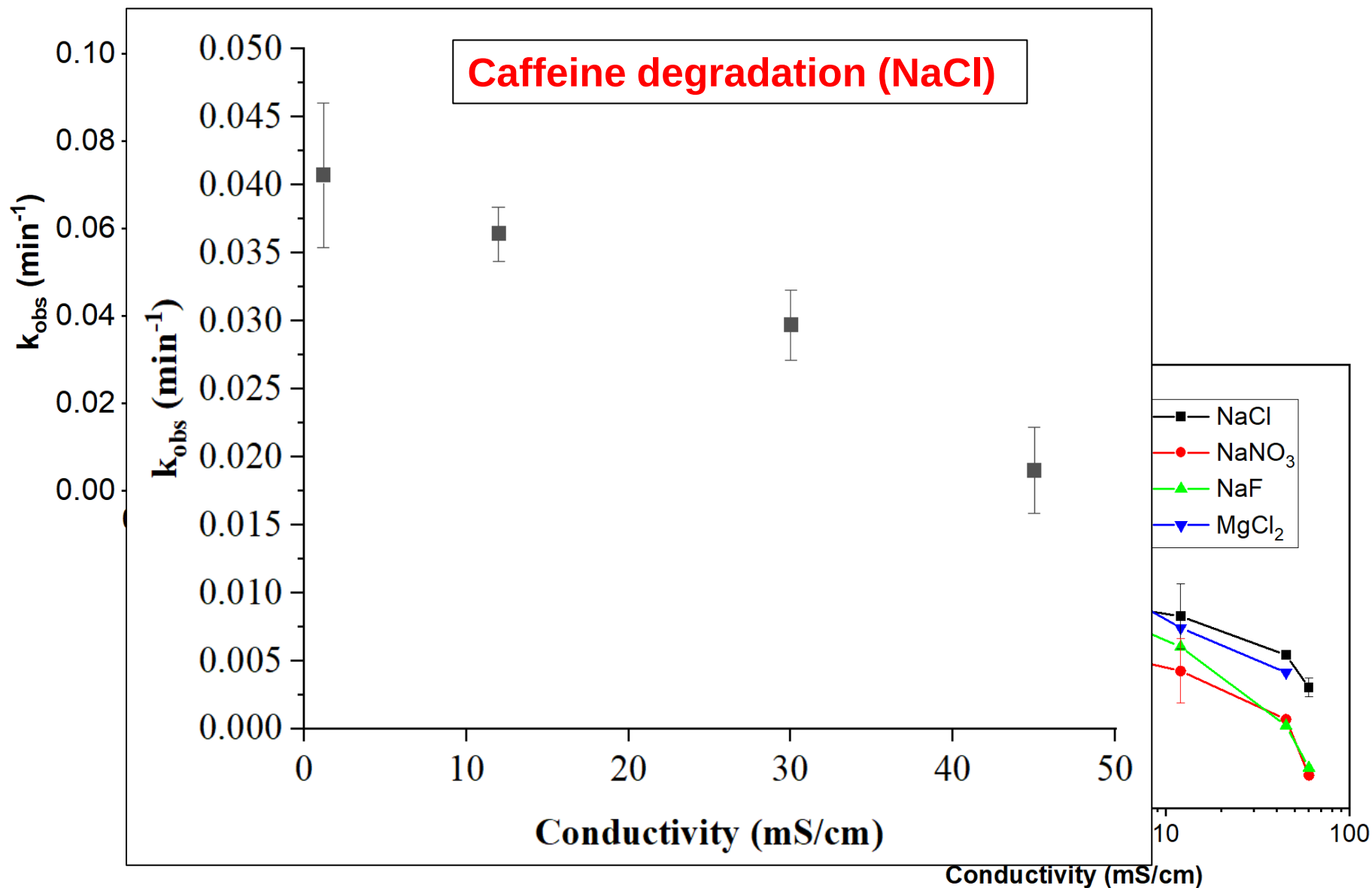


Non-chlorine salts

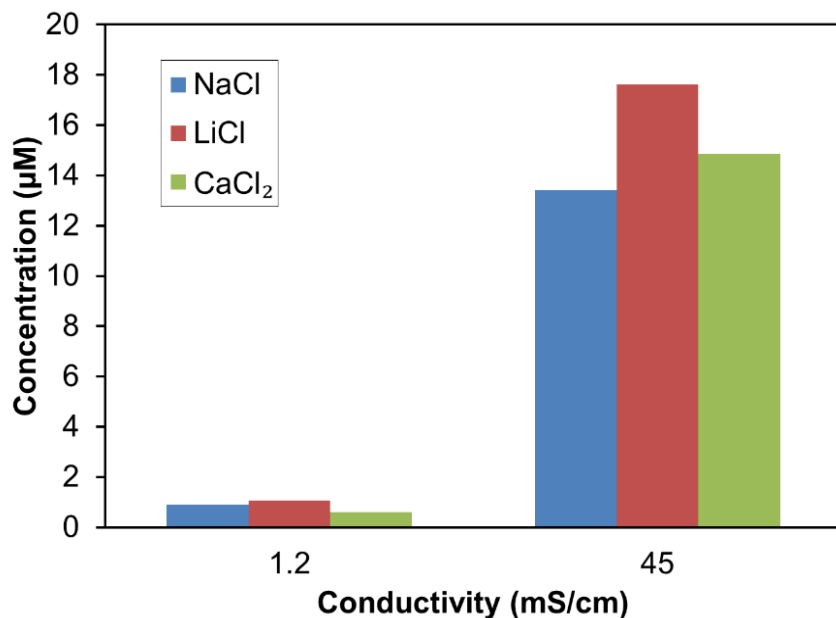


Chlorine salts

Rhodamine B degradation: non-chlorine salts

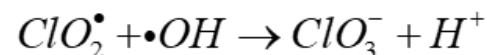
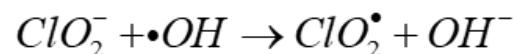
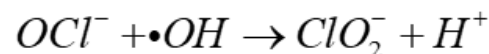
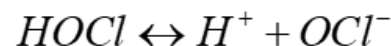
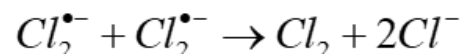
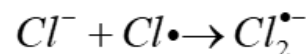
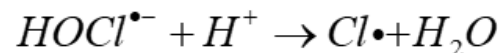
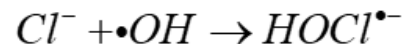


Chlorine chemistry

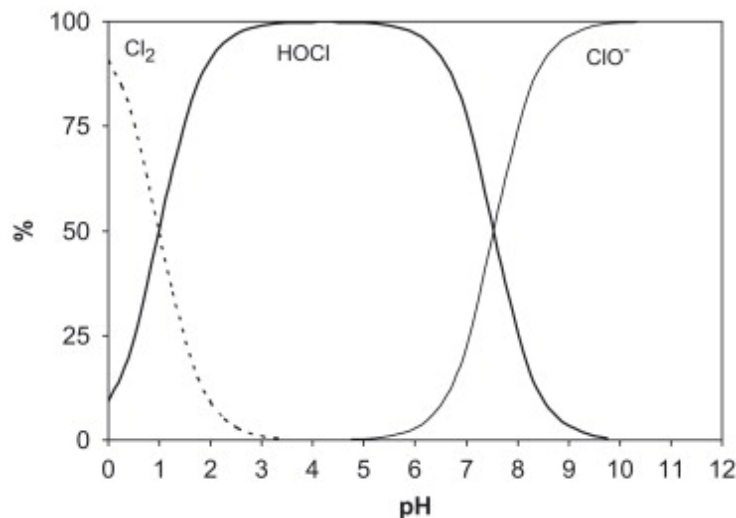


Concentration of chlorate (ClO_3^-) formed at 1.2 mS/cm and 45 mS/cm for three chlorine salts

Perchlorate (ClO_4^-) has not been detected



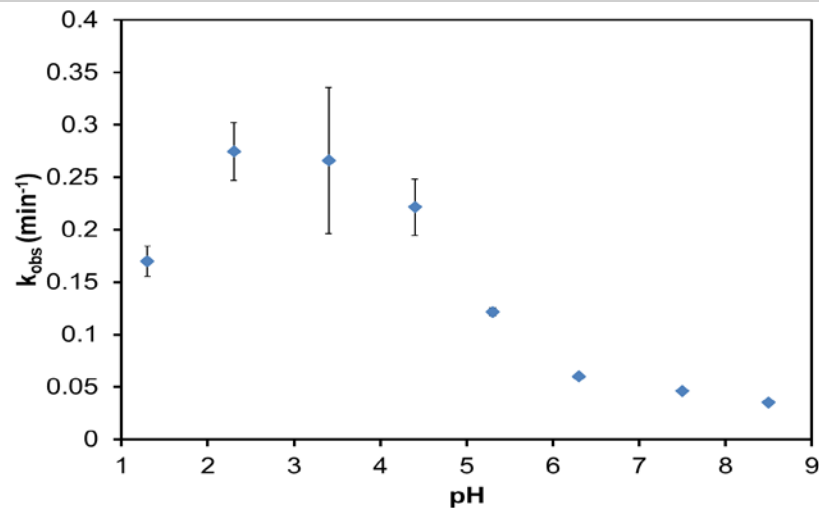
Rhodamine B degradation: HOCl



Hypochlorous acid (HOCl) is stable but deprotonates above a pH of ~ 7 to form the relatively inert ClO^- which does not react with RhB.

Chlorine pH-dependent speciation profile

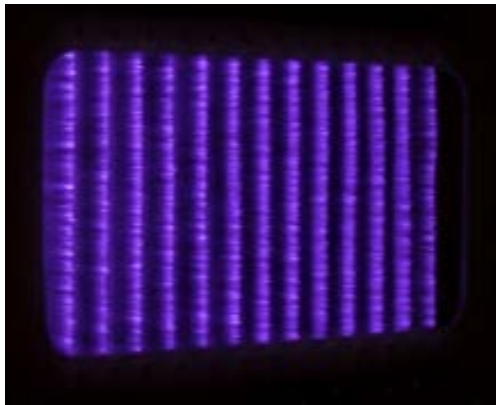
HOCl degrades RhB and could oxidize various non-PFAS compounds in brine.



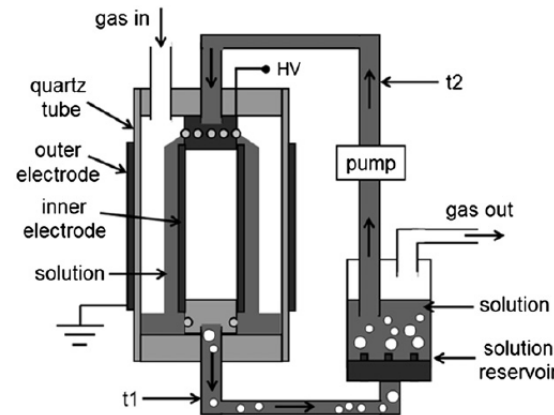
Influence of solution pH on Rh B removal.
Conductivity is fixed at 45 mS/cm

Non-surfactants

- 100+ reactors available to compare without clear design guidelines.
- For the most effective reactors plasma generated in a gas phase is contacting a thin film of liquid.



Corona above water



DBD with falling liquid film

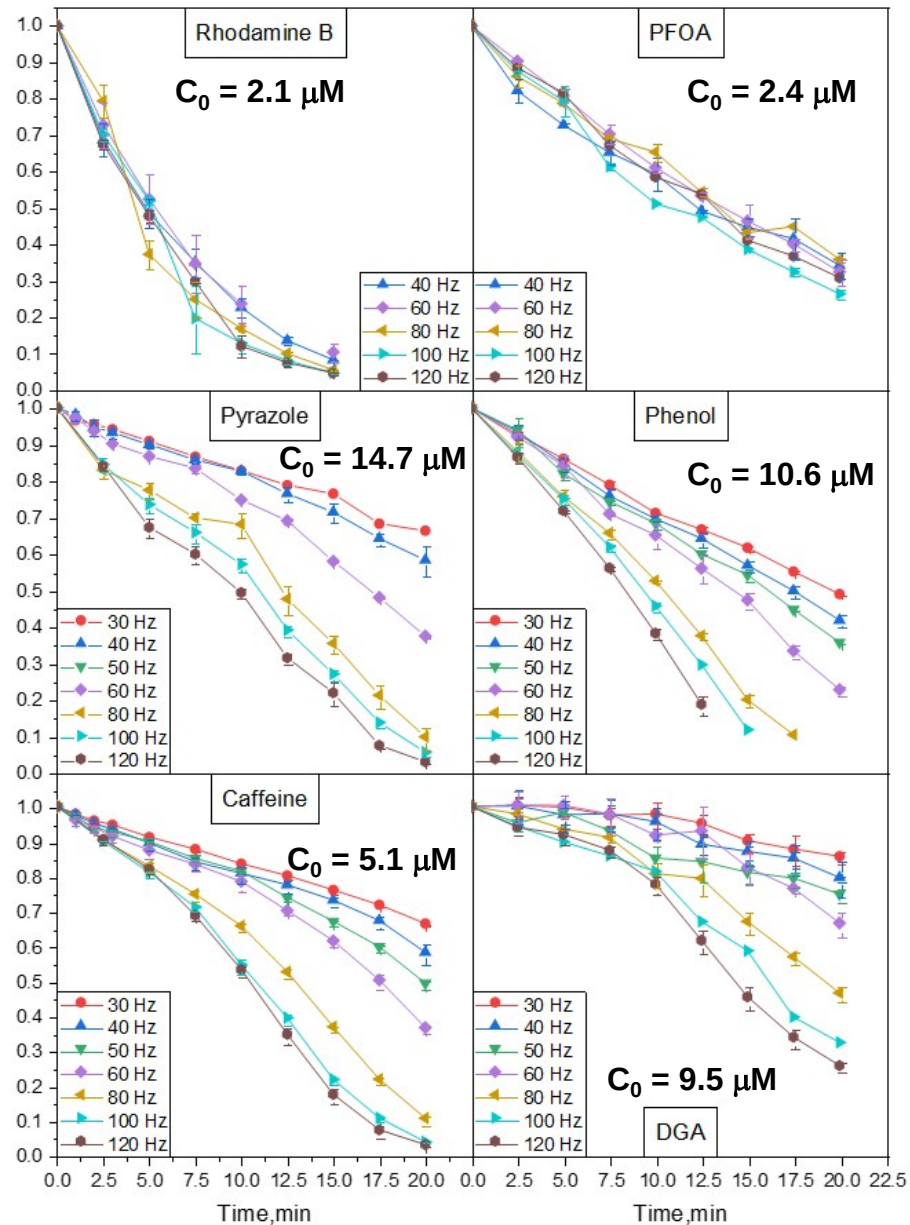
- **Design points to consider:**
 - (1) Ozone chemistry decoupled from OH radical chemistry
 - (2) Reasonable treatment volumes
 - (3) Environmentally relevant ($\sim\mu\text{g/L}$) concentrations of mixtures of compounds

The importance of a compound's initial concentration in its removal

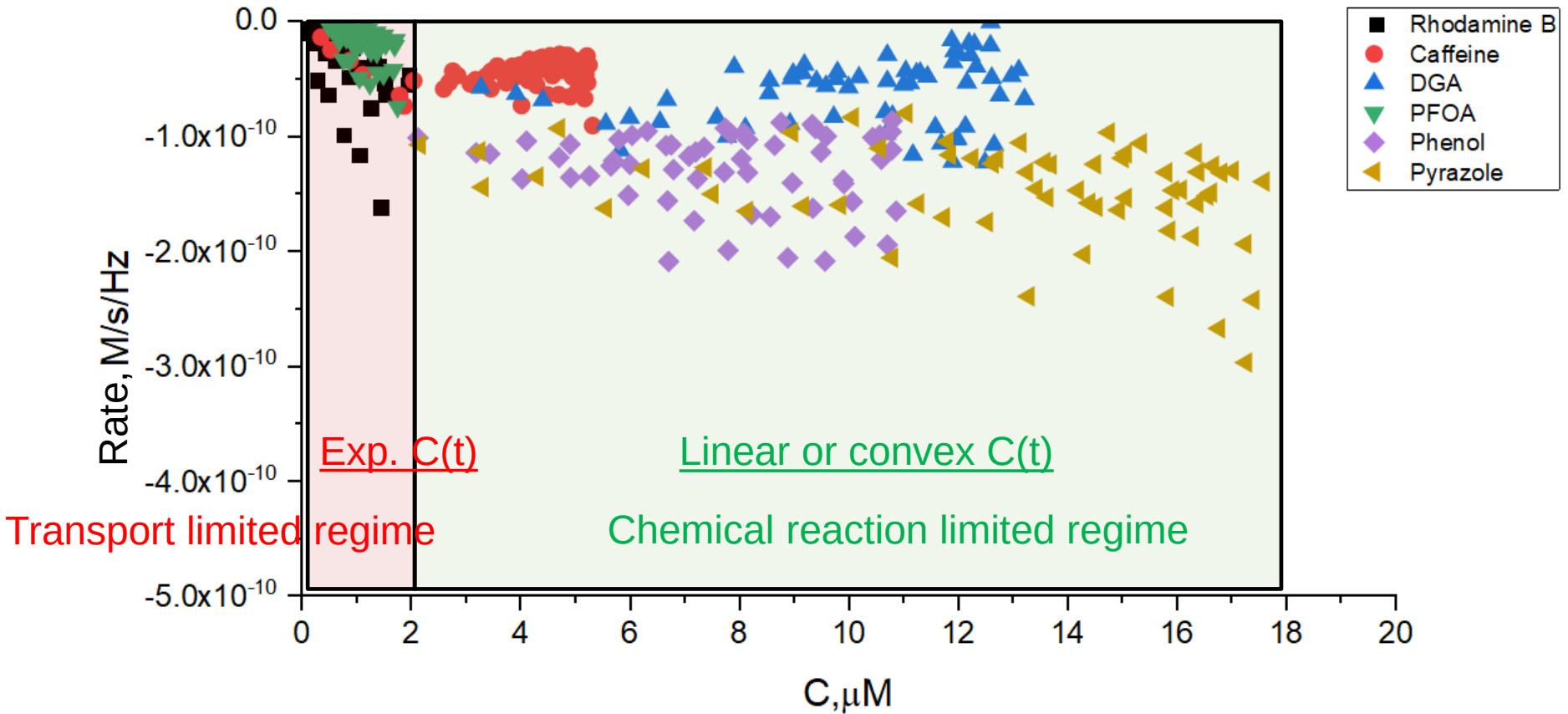


**Rail-plate electrode configuration
(no external mixing)**

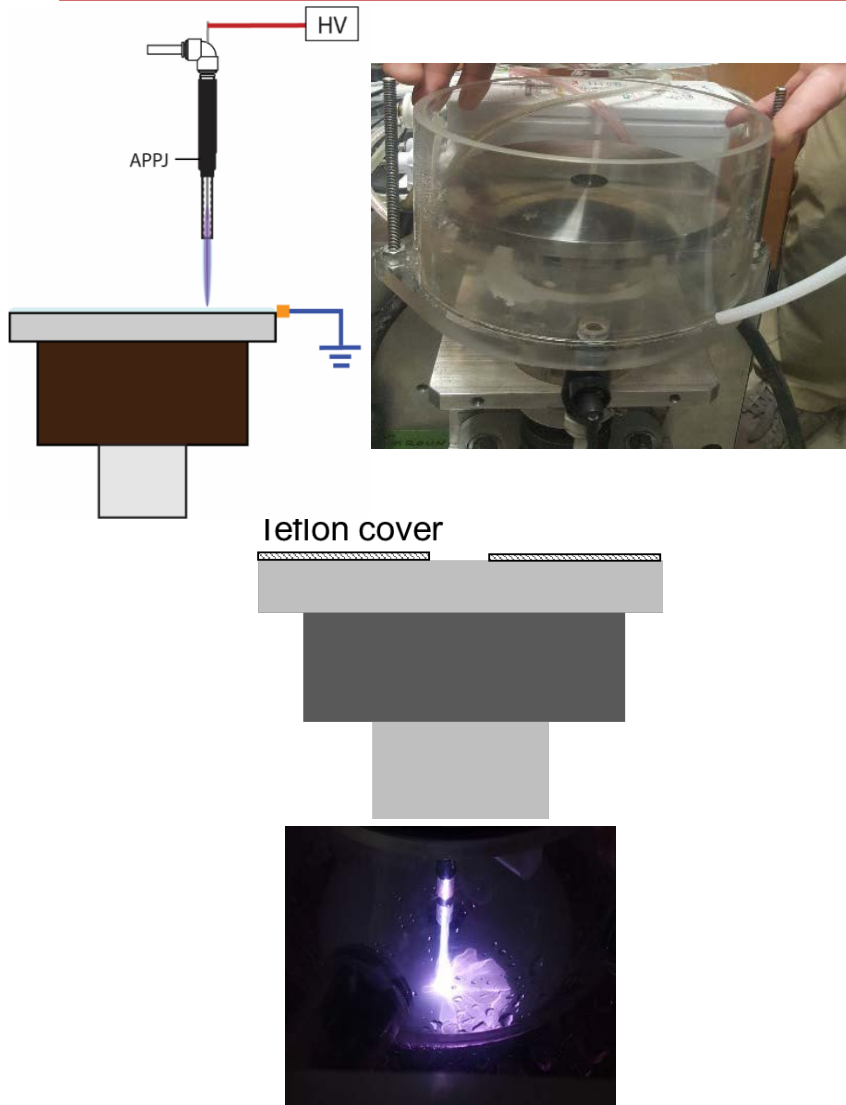
Degradation profiles of six compounds as a function of discharge frequency



Bulk liquid concentration controls the removal regime

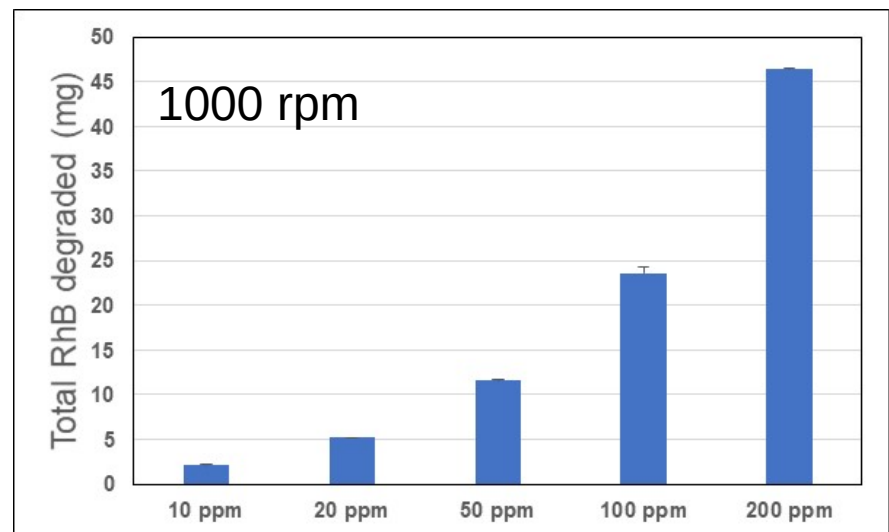
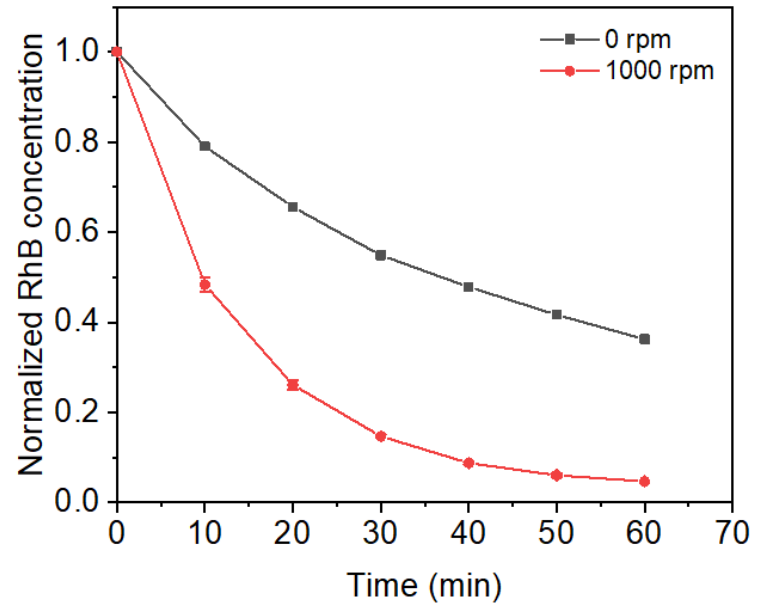


Removal of rhodamine B in a plasma spinning disc reactor



Letlon cover

Treatment volume 500 mL



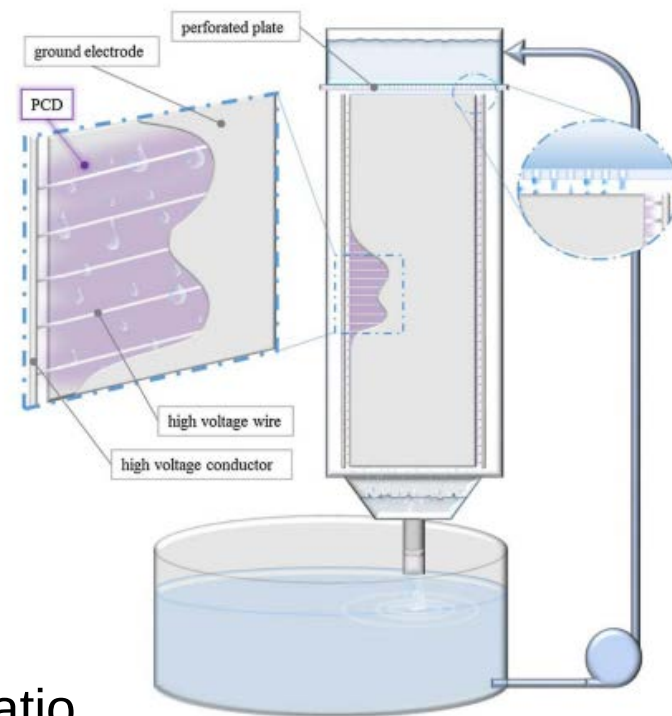
Plasma process (non-PFAS) scaleup

We have promising bench-scale plasma reactors so let's start scaling up!

- 50 L batch hospital effluent treatment
- 27 pharmaceuticals ($\sim 1149 \mu\text{g/L}$)
- 59 % removal (treatment times not reported)
- Ozone plays a role in the degradation

Technological challenges:

- (1) Ensuring high area-to-volume treatment ratio
- (2) Generation of large volume plasma
- (3) Power supply scaleup



Pilot scale reactor for pharmaceuticals treatment

Requirements and Recommendations

Reactor design depends on the water characteristics:

- surfactants vs. non-surfactants
- total organic carbon
- solution electrical conductivity

Realistic throughput:

- up to 100 gpm for direct treatment
- up to 20 gpm for concentrate treatment (likely near-future adoption)
 - *Membrane*
 - *Ion exchange*
 - *Adsorption/desorption*

Hypothetical target: Develop a 1 gal 1,4 dioxane treatment system

Dyes should be avoided as they exhibit surfactant-like properties

Performance goal: Rapid removal (minutes timeframe for direct treatment)

Energy considerations not important initially

Requirements and Recommendations

Performance criteria to consider:

- Environmentally relevant concentrations with and without co-contaminants : $\sim\mu\text{g/L}$ in groundwater or mg/L post-concentration

Starting concentrations influence overall kinetics (transport vs. species limited regime)

- Surface-to-volume ratio

Start with a thin liquid film or a spray (practicality?)

Filamentary vs. diffuse plasma

- Utilize plasma-generated H_2O_2 to form additional OH in the bulk liquid (?)

>10,000 mg/L of H_2O_2 is required to oxidize organic mater in the groundwater

- Ozone chemistry decoupled from OH radical chemistry
- Air (nitrates!) vs. oxygen vs. argon
- Iron and solid catalysts should be avoided

Summary

- The utilization efficacy of plasma-generated species depends on the proximity of the compound(s) treated to the plasma-liquid interface and the plasma area.
- The process is a competitive AOP for the treatment of a range of compounds and a superior technique for the removal of long-chain PFAS from various aqueous matrices.
- Addition of CTAB facilitates the transport of short-chain PFAS to the plasma liquid interface and enables their removal although chloride ions may interfere with the binding process.
- Chlorine chemistry (HOCl) may significantly contribute to the oxidation of bulk liquid constituents.
- Applications: water reuse (e.g., recycling of wastewater treatment plant effluents) and point source treatment (e.g., industrial and hospital effluents).
- Post-concentration step treatment (plasma treatment train) is the most realistic near-future application of the technology.

Acknowledgments

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